

THE CITY OF KINGSVILLE LANDFILL  
TCEQ PERMIT MSW 235-C

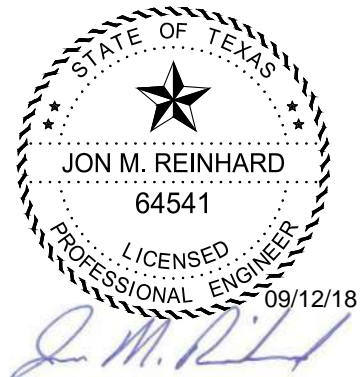
**PERMIT AMENDMENT APPLICATION**

**Volume 4 of 6**



CITY OF KINGSVILLE, TEXAS

September 2018  
Revision 0



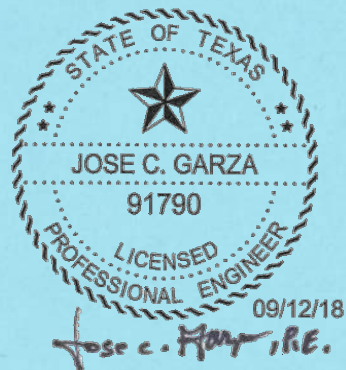
Prepared by



HANSON PROJECT NO. 16L0438-0003

**CITY OF KINGSVILLE LANDFILL**  
**PART III**  
**ATTACHMENT 5**  
**ALTERNATIVE LINER AND OVERLINER**  
**POINT OF COMPLIANCE DEMONSTRATIONS**

**ATTACHMENT 5**  
**ALTERNATIVE LINER AND OVERLINER DESIGN AND POINT OF  
COMPLIANCE DEMONSTRATIONS**



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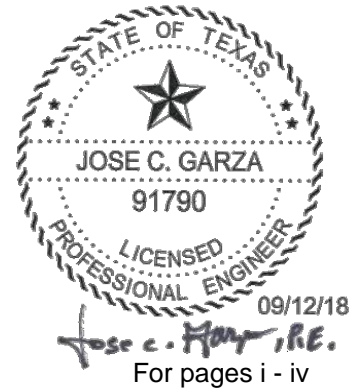
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# 1 INTRODUCTION

## 1.1 Purpose and Scope

This attachment is submitted to allow the use of a geosynthetic clay liner (GCL) as an alternative to the Subtitle D two-foot thick soil liner component of the liner system and demonstrate that the proposed alternative liner and overliner will meet the point of compliance (POC) requirements specified in Title 30 Texas Administrative Code (TAC) §330.331 (a).

This Alternate Liner Design Demonstration (ALD) was performed in accordance with the procedures presented in the *Texas Water Commission Alternate Liner Design Handbook, A Performance Standard As Authorized by 31 Texas Administrative Code (TAC) §330.202 (Version 1, August 1993)*, using the Hydrologic Evaluation of Landfill Performance (HELP) and Mutimed Exposure Assessment (MULTIMED) computer models. This is achieved by demonstrating that the predicted concentrations of selected leachate chemical constituents do not exceed maximum contaminant levels (as listed in Table 1 in §330.331(a)(1)) in the uppermost aquifer at the POC. The concentration of various constituents at the POC is determined by calculating a dilution attenuation factor (DAF), which is determined by the following equation.

$$DAF = \frac{C_o, \text{ Initial Constituent Concentration of Leachate Within the Landfill}}{C_p, \text{ Constituent Concentration at the POC}}$$

The DAF represents the factor by which the constituent concentration is expected to decrease between the landfill and the POC. When the constituent's concentration in leachate is divided by the model predicted DAF, the resulting concentration must be less than the allowable maximum contaminant levels (MCLs) in groundwater for the chemical parameters listed in Table 1 included in Title 30 TAC §330.331(a)(1).

The scope of this attachment includes both an alternative liner for future sectors and the proposed alternative liner and overliner for the pre-Subtitle D areas.

## 1.2 Proposed Alternative Liner

The layout of the proposed alternative liner is shown in Appendix A-Point of Compliance Figures, A.1 Permit Amendment Application MSW-235C Landfill Completion Site Plan. The proposed alternative liner system consists of a 60-mil high density polyethylene (HDPE) geomembrane placed over a GCL overlain by a geocomposite leachate collection



layer covered with a 2-foot-thick layer of protective soil cover. The components of the proposed alternative liner are shown in Appendix B.1 HELP Model/MULTIMED Model-Summary of Cases 1-8 for both interim and closed conditions. Details of the alternate liner are in Appendix D.1 and Appendix D.2.

### **1.3 Proposed Overliner System**

The layout of the proposed overliner system is shown in Appendix A Point of Compliance Figures, A.1 Permit Amendment Application MSW-235C Landfill Completion Site Plan. The proposed alternative overliner system consists of a 60-mil high density polyethylene (HDPE) geomembrane placed over GCL overlain by a geocomposite leachate collection layer covered with a 2-foot thick layer of protective soil cover. The overliner will be placed over pre-Subtitle D areas to separate the existing waste and the vertical expansion area. The overliner system areas include Sectors 8A and 8B. The components of the proposed overliner system are shown in Appendix B.11 Help Model/MULTIMED Model-Summary of Cases 1OL-8OL for both interim and closed conditions. Details of the overliner system are in Appendix D.3 and Appendix D.4.

### **1.4 Site Geology and Hydrogeology**

A geologic and hydrogeologic site exploration program was conducted for the proposed City of Kingsville Landfill. Details of these investigations are included in Attachment 4 Geology Report.

## **2 ALTERNATE LINER DEMONSTRATION METHODS**

### **2.1 HELP Model**

The HELP Model Version 3.07 was used to estimate the amount of leachate generated by the landfill and the percolation through the proposed alternative liner system and overliner system. The HELP model is a water-balance model developed by the U.S. Army Corps of Engineers Waterways Experiment Station for the Environmental Protection Agency (EPA). The model uses climate, soil, and landfill design data to perform a solution technique that accounts for the effects of surface storage, run-off, infiltration, percolation, soil moisture storage, evapotranspiration, and lateral drainage.

### **2.2 MULTIMED MODEL**

The MULTIMED Model Version 1.01 was used to assess contaminant fate and transport between the landfill base and the Point of Compliance (POC). MULTIMED was developed by the Athens Environmental Research Laboratory for the EPA. MULTIMED estimates the capacity of the hydrogeologic system modeled to dilute and attenuate contaminate concentrations. The model can be used to simulate fate and transport processes in both unsaturated and saturated subsurface environments. In this application, only the saturated environment was modeled to provide a conservative analysis.

### **2.3 LANDFILL CONFIGURATIONS**

Sixteen HELP Model simulations were completed to estimate percolation rates through the alternate liner and overliner system. Both interim and closed landfill conditions were modeled in accordance with the Texas Water Commission Alternate Liner Design Handbook. The landfill configurations modeled for the alternative liner are summarized in Appendix B.1. HELP Model/MULTIMED Model-Summary of Cases 1-8 and in Appendix B.2 HELP Model Case Summary. The landfill configurations modeled for the overliner system are summarized in Appendix B.11 HELP Model/MULTIMED Model-Summary of Cases 1OL-8OL and B.12 HELP Model Case Summary. The resulting percolation rate for each HELP Model simulation was then used to estimate the DAF using MULTIMED for each of the 16 cases. MULTIMED model analysis is in Appendix C. Calculations of the DAF are in Appendix D. The locations used for the POC demonstrations were chosen to represent the shortest distance to the POC. The analysis locations were selected to model the scenario at the toe of the landfill, midway up the slope, at the slope transition, and peak in order to consider the effect of the waste column thickness on the calculated DAF. Point of Compliance Figures are in Appendix A. DAFs were also computed at the four locations for each landfill configuration to show a direct relationship with the distance from the POC to the analysis point. Leachate Data is in Appendix E. MULTIMED Model output is in Appendix F. Aquifer Specific Data, geology, and hydrogeology are in

Appendices C.7.1 through C.7.11. The upper clay (light olive green clay) is ubiquitous under the site with a minimum proven thickness of 38 feet thick, the Chicot Aquifer is approximately 220 feet below ground surface, and the Evangeline Aquifer is approximately 500 feet below ground surface. The light olive green clay layer serves as aquiclude between the uppermost aquifer below the landfill site and the Chicot aquifer. To provide a conservative assumption given the bottom of the landfill and the groundwater, the percolation through the alternate liner and overliner system was assumed to be conveyed directly to the upper strata and therefore travel time, dilution, and attenuation are not accounted for in this analysis for upper soils.

## **2.4 SLOPE STABILITY ANALYSIS**

The alternative liner and overliner system were analyzed for slope stability by performing two dimensional, effective stress slope stability analyses for the final, closed geometry, using the computer program SLIDE. The slope stability calculations are presented in Part III Attachment 4, Appendix 2-Section 7 WASTE MASS STABILITY and Appendix F: Graphical Representation of Mass Stability Analyses Results.

### **3 MODEL INPUT PARAMETERS**

Detailed HELP and MULTIMED information is presented in Appendices A through F. HELP Model input parameters and results are summarized in Appendices B.1, B.2, B.11, and B.12 for both the analysis of the alternative liner (interim and closed conditions) and overliner system (interim and closed conditions). In general, conservative assumptions were made in determining the percolation rate and dilution attenuation factor (DAF). A list of major assumptions used in the MULTIMED demonstrations are presented in Table 3-1. The table also compares the actual site conditions to the assumptions used for modeling. The criteria used to develop the percolation rate for each landfill case were selected to maximize the percolation rate. As discussed in Section 2.3, a major conservative assumption is not accounting for the approximately 38 feet of low permeability light olive green clay separating the bottom of the landfill and the uppermost groundwater zone. The estimated percolation through the alternative liner and overliner system is modeled to be conveyed directly to the strata below the bottom of the landfill at each evaluation section location; and the water table is assumed to be at the bottom of the liner as a conservative approach. If less conservative assumptions were used, the DAF calculated using MULTIMED for each landfill case would be significantly larger.

The MULTIMED model input parameters are detailed in Appendix C. By making the assumptions listed in Table 3-1, a single MULTIMED simulation accounts for all 24 constituents identified by the EPA as requiring landfill design protection criteria. The required minimum DAFs for the 24 EPA constituents are given in Table 2-Leachate Evaluation, page 24 of the *Texas Water Commission Alternate Liner Design Handbook*; the same table of constituents listed in Table 1 in Title 30 TAC §330.331(a)(1). The largest DAF listed in the table is 260. Therefore, if MULTIMED results in a DAF higher than 260 for a generic chemical that is conservatively modeled with no carbon absorption, no biodegradation, and no decay, it is concluded that the proposed alternative liner and overliner system design is acceptable. The actual DAF for a specific chemical would be higher than the result calculated by MULTIMED under these circumstances since actual physical processes of absorption, biodegradation, and decay would act to reduce chemical concentrations at the POC to less than those predicted by MULTIMED. The model result is then expressed in terms of the DAF, which is defined as the ratio of the input concentration to the concentration at the POC. MULTIMED can be used to find the DAF by using an input concentration of 1.0 mg/L. The DAF is the reciprocal of the resulting concentration of POC. The POCs for this demonstration are in Appendix F.

**Table 3-1**  
**Major Assumption Used to Determine MULTIMED Model Input Parameters**

Input Parameters	Assumption	Actual Site Conditions
Model Source Type	Steady state	Assumed amount of leachate percolation is released continuously. This is a very conservative assumption.
Biodegradation	No biodegradation	Biodegradation is active in hydrogeologic environments
Chemical Decay	No chemical decay	Chemical decay will occur with most contaminants in hydrogeologic environments

## 4 POINT OF COMPLIANCE DEMONSTRATION RESULTS

The HELP and MULTIMED models were used to evaluate the proposed design of the alternative liner and overliner system by estimating constituent concentrations at the POC for the landfill cases discussed in Section 2.3. The percolation rates obtained from the HELP Model cases included in Appendix C.3 and Appendix C.4 were used as input for the MULTIMED model to determine the DAF. Conservatively, the constituent concentrations at the base of the landfill liner and at the POC were used to calculate the DAF.

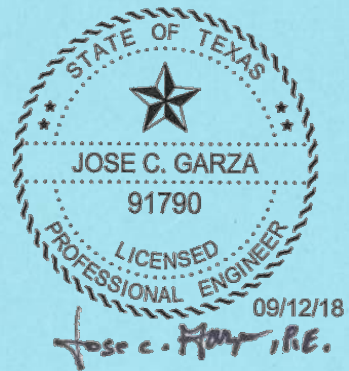
A summary of the calculated DAF is presented below and in Appendix D.

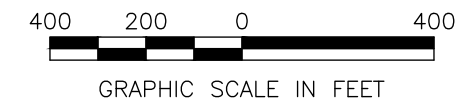
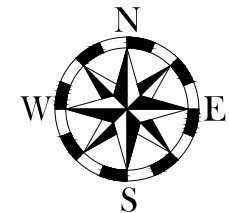
Location	Interim Case DAF	Closed Case DAF
Alternative Liner Location 1	33,979	85,106
Alternative Liner Location 2	57,471	201,288
Alternative Liner Location 3	80,645	282,566
Alternative Liner Location 4	286,533	1,003,814

Location	Interim Case DAF	Closed Case DAF
Overliner Location 1	18,797	65,833
Overliner Location 2	77,640	232,450
Overliner Location 3	158,253	473,934
Overliner Location 4	615,385	1,842,639

The results demonstrate that the proposed alternative liner design and overliner design meets or exceeds the requirements of Title 30 TAC §330.331(a)(1). The DAF calculated by the use of HELP and MULTIMED are well in excess of the 260 minimum criterion. The actual DAFs are expected to be substantially higher than the DAFs predicted by this modeling demonstration because the model input was conservatively estimated as discussed in previous sections of this report.

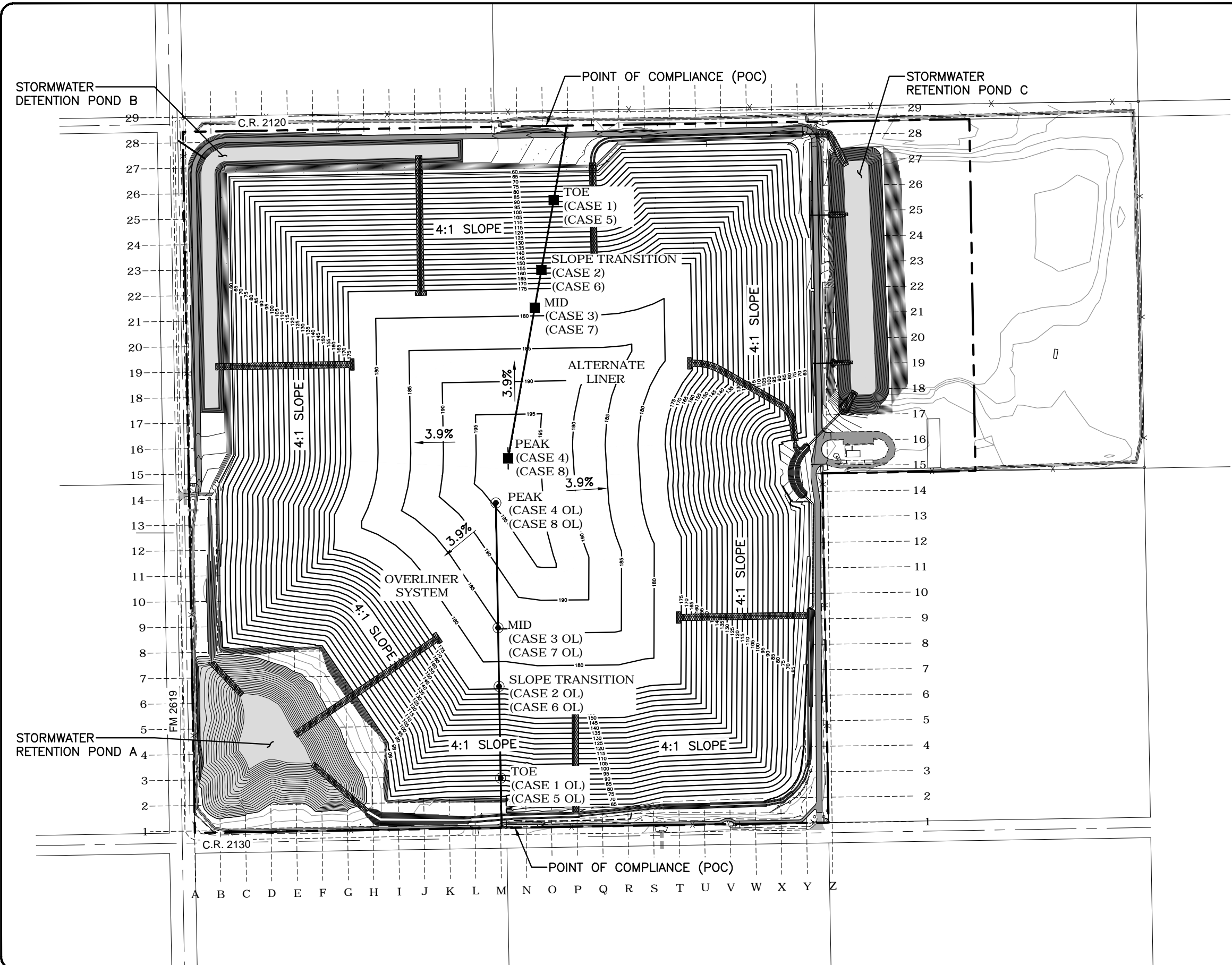
APPENDIX A  
POINT OF COMPLIANCE FIGURES





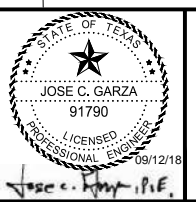
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- — EXISTING ROAD
- — — — PERMIT BOUNDARY LIMITS
- 200 — FINAL COVER CONTOURS
- — — — PROPOSED ROAD
- ▬ PROPOSED STORMWATER LETDOWN STRUCTURE
- PROPOSED STORMWATER PONDS
- PROPOSED ALTERNATE LINER
- PROPOSED OVERLINER SYSTEM



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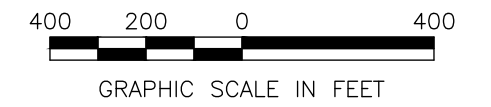
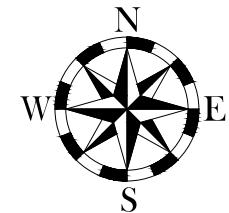
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**PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL COMPLETION SITE PLAN  
 CITY OF KINGSVILLE LANDFILL**  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

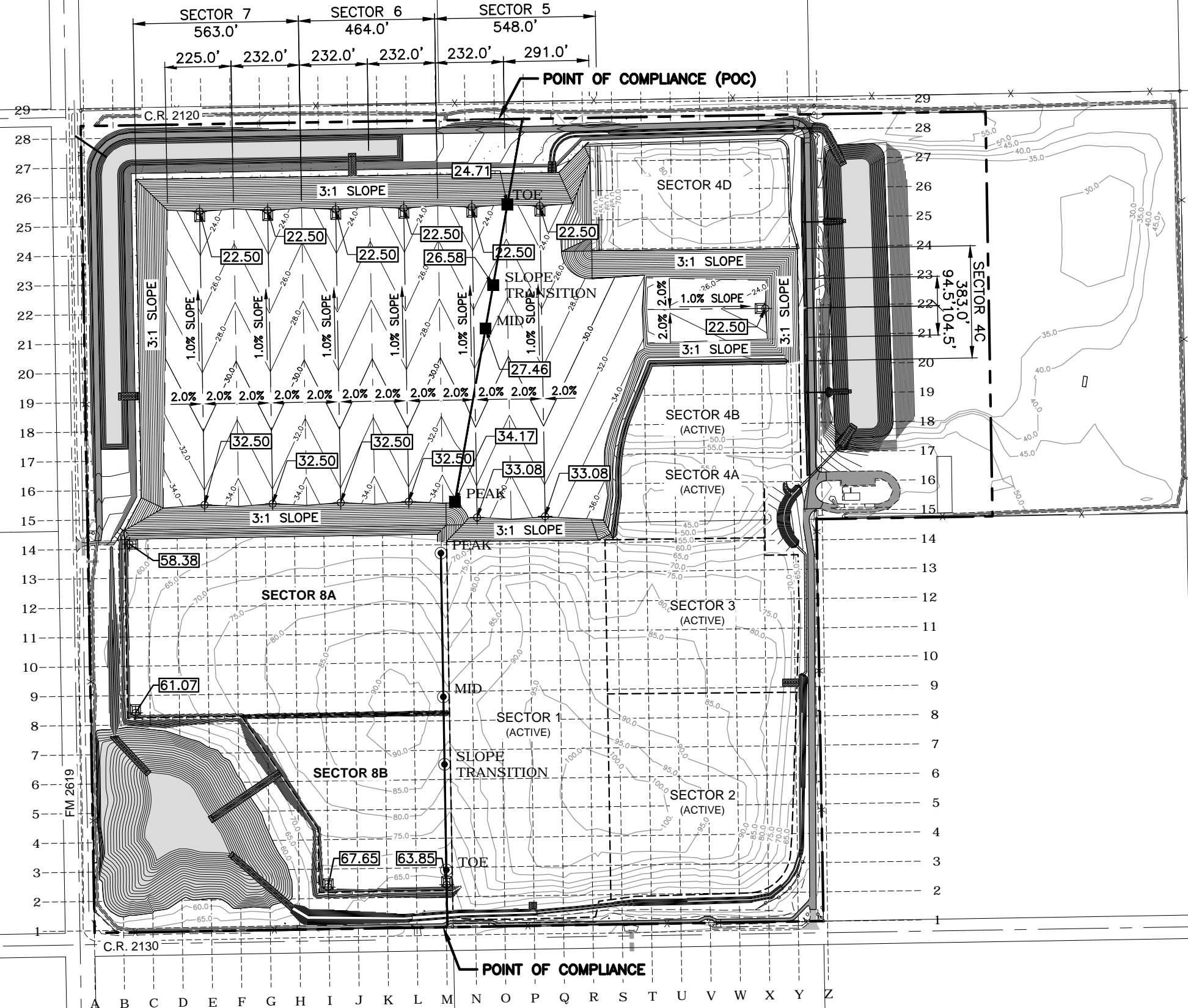
**FIGURE:  
 III.5-A.1**





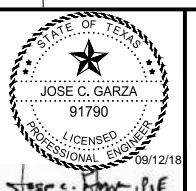
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- — PERMIT BOUNDARY LIMITS
- 24.0 — BASE OF EXCAVATION CONTOURS
- 22.50 BASE OF EXCAVATION ELEVATION
- — PROPOSED ROAD
- — PROPOSED STORMWATER LETDOWN STRUCTURE
- — PROPOSED STORMWATER PONDS
- PROPOSED ALTERNATIVE LINER
- PROPOSED OVERLINER



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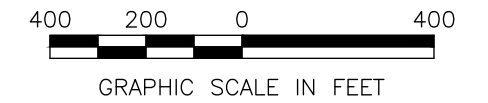
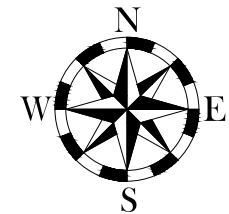
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PART III, ATTACHMENT 5, APPENDIX A  
**LANDFILL COMPLETION  
 EXCAVATION PLAN**  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

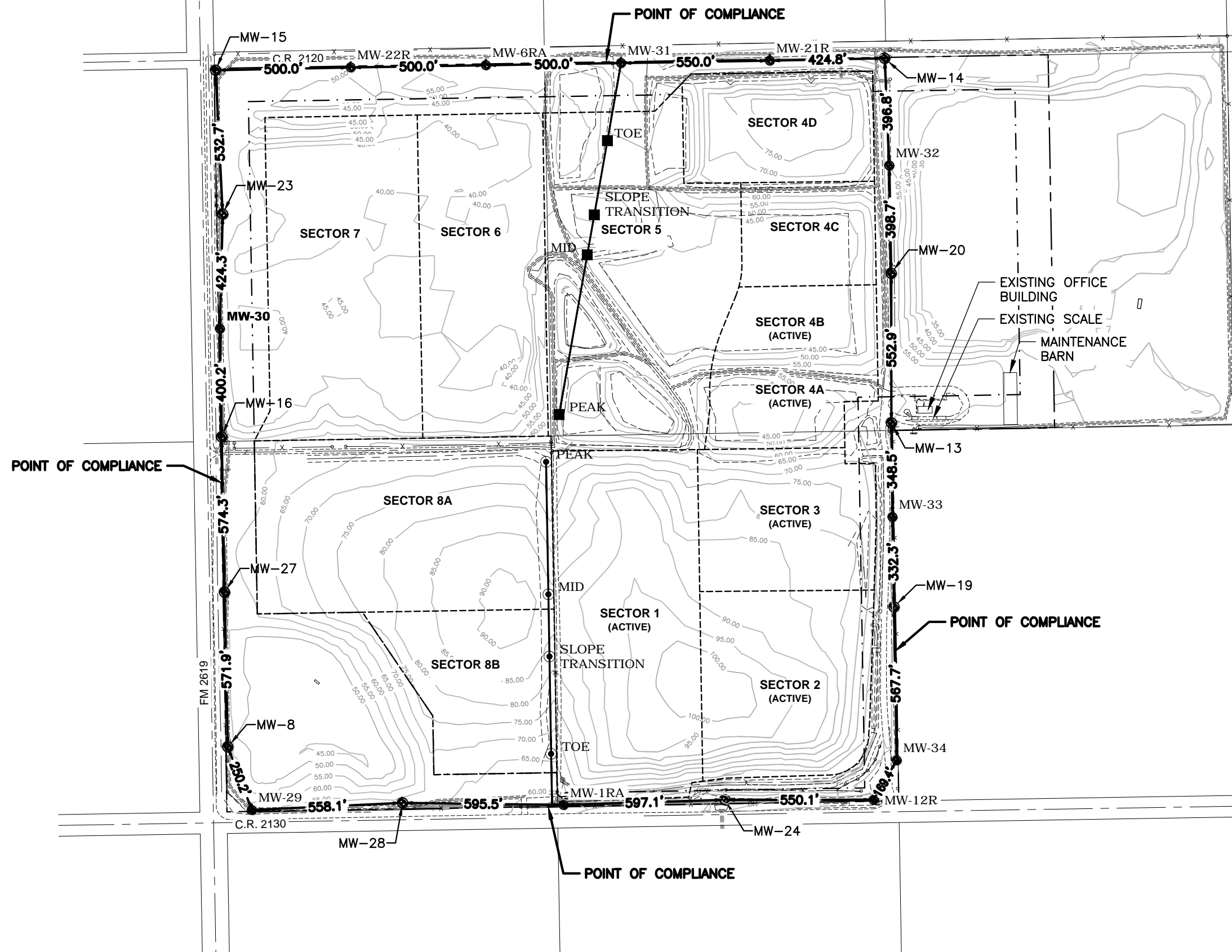
**FIGURE:  
 III.5-A.2**



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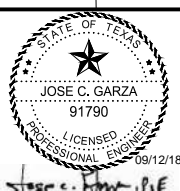
- MW-20 MONITOR WELL LOCATION
- x — EXISTING FENCE
- 65.00 — EXISTING SURFACE CONTOUR (2015)
- - - - SECTOR OUTLINE
- - - - PERMIT BOUNDARY (175.89 ACRES)
- - - - BUFFER ZONE
- 400.2' — POINT OF COMPLIANCE
- PROPOSED ALTERNATIVE LINER
- PROPOSED OVERLINER

SITE COORDINATES		
MONITOR WELL LOCATIONS		
MW	Northing	Easting
MW-8	17051473.78	1203673.74
MW-13	17052672.16	1206127.95
MW-14	17054020.04	1206103.02
MW-15	17053976.10	1203628.61
MW-16	17052619.76	1203651.21
MW-19	17051991.35	1206137.50
MW-20	17053225.01	1206127.20
MW-23	17053444.05	1203654.88
MW-24	17051277.99	1205512.42
MW-27	17052045.52	1203661.75
MW-28	17051266.46	1204320.24
MW-1RA	17051258.70	1204915.66
MW-32	17053623.64	1206120.29
MW-6RA	17053994.38	1204628.44
MW-12R	17051277.38	1206062.51
MW-21R	17054011.48	1205678.30
MW-22R	17053986.24	1204128.51
MW-29	17051239.92	1203762.81
MW-30	17053019.90	1203644.60
MW-31	17054002.53	1205128.38
MW-33	17052323.65	1206132.04
MW-34	17051423.79	1206147.64



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Date	09/12/2018
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DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

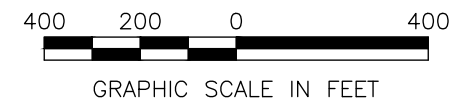
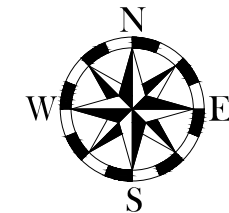


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PART III, ATTACHMENT 5, APPENDIX A  
LANDFILL POINT OF COMPLIANCE LOCATIONS  
CITY OF KINGSVILLE LANDFILL  
MSW PERMIT No. 235-C  
KINGSVILLE, TEXAS  
KLEBERG COUNTY, TEXAS

FIGURE:  
III.5-A.3



**HYDRAULIC GRADIENT**

$$i = \frac{34 - 31.50}{800}$$

$$i = 3.125 \times 10^{-3}$$

$$i = 0.003125$$

**HYDRAULIC GRADIENT**

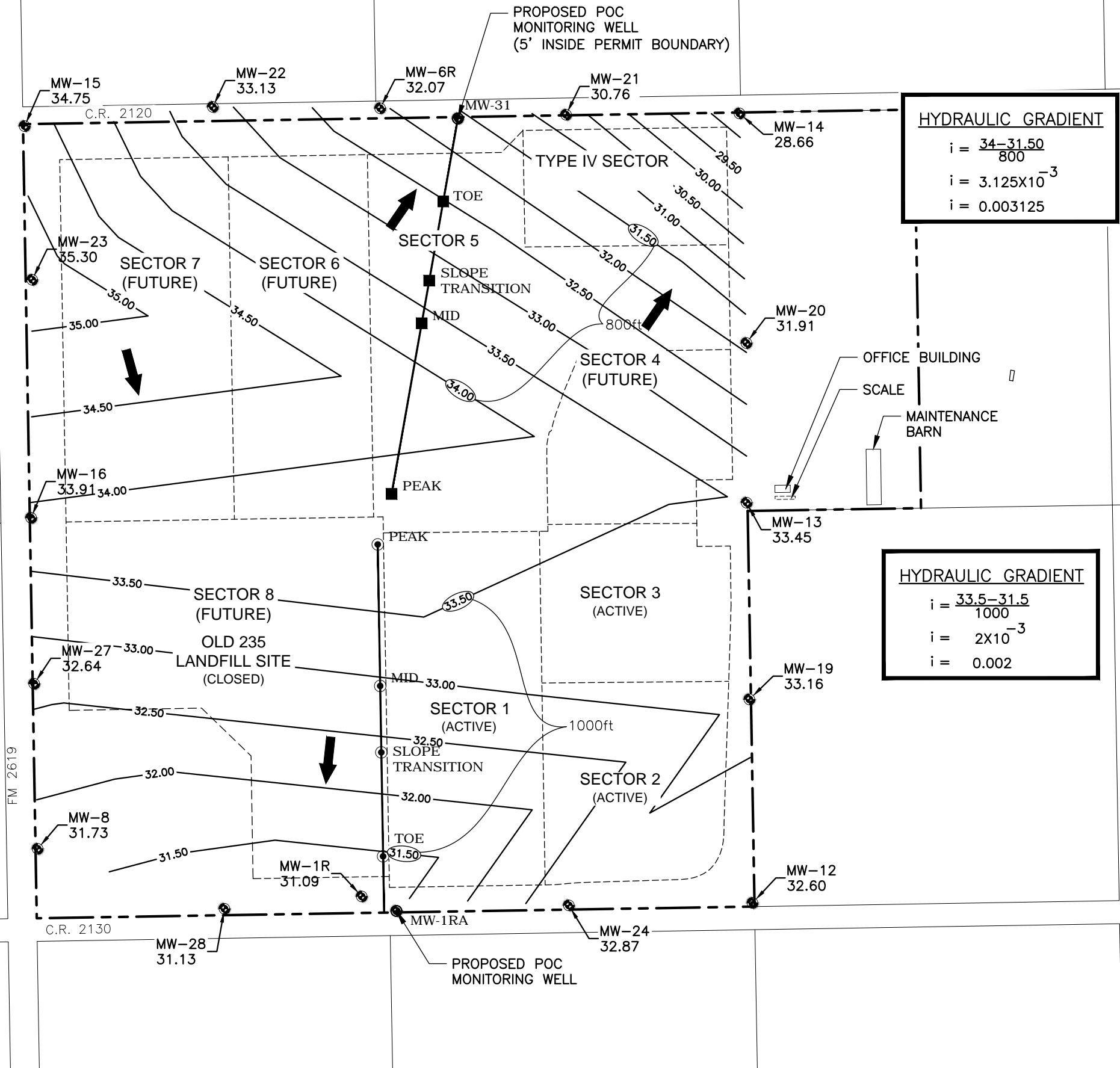
$$i = \frac{33.5 - 31.5}{1000}$$

$$i = 2 \times 10^{-3}$$

$$i = 0.002$$

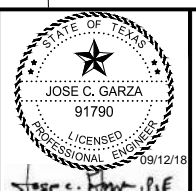
- LEGEND:**
- MW-20 31.91
  - 32.00
  - 
  - 
  - 
  - 
  - 
  -

**NOTE:**  
 THIS DRAWING WAS ORIGINALLY SEALED BY SCOT E. COLLINS, P.G., LICENSE No. 10398 ON 02/09/2016 (EXHIBIT 2 GROUNDWATER CONTOUR MAP (JANUARY 2016) CITY OF KINGSVILLE LANDFILL.



SEP 12, 2018 5:41 PM TORRE01809 I:\16JOBS\16L0438\8514-CITY OF KINGSVILLE\8514-03-CAD-PART-1\8514-03-MULTIMED-GROUNDWATER CONTOUR MAP.DWG

NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



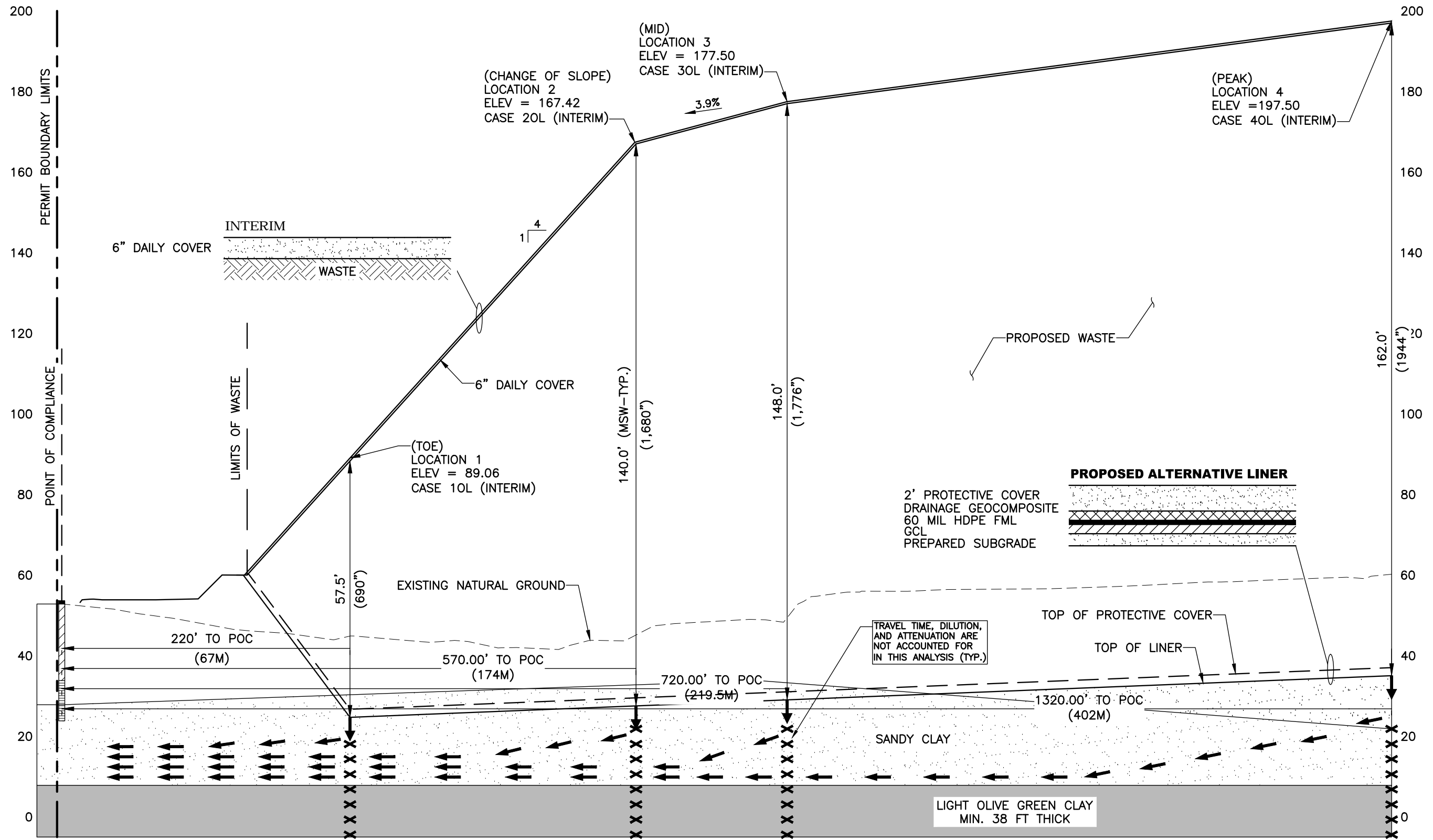
Hanson No.	16L0438
Filename	
Scale	AS SHOWN
Date	09/12/2018
LAYOUT	DT 09/12/2018
DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

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**PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL GROUNDWATER CONTOUR  
 MAP/HYDRAULIC GRADIENT  
 CITY OF KINGSVILLE LANDFILL**  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:  
 III.5-A.4**



**ALTERNATIVE LINER DEMONSTRATION – INTERIM LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE ALTERNATIVE LINER.
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

**MULTIMED INFORMATION**

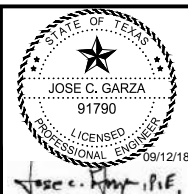
AVERAGE AQUIFER THICKNESS = 32.81FT (10M)  
 HYDRAULIC CONDUCTIVITY =  $4.12 \times 10^{-4}$  CM/SEC OR  
 130 M/YR  
 HYDRAULIC GRADIENT =  $i = 0.003125$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

SEP 11, 2018 2:47 PM TORRE01809 I:\16JOBS\16L0438\8514-CITY OF KINGSVILLE\8514-03\CAD-PART-III\8514-03-MULTIMED-SECTIONS.DWG

NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



Hanson No.	16L0438
Filename	
Scale	AS SHOWN
Date	09/12/2018
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DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

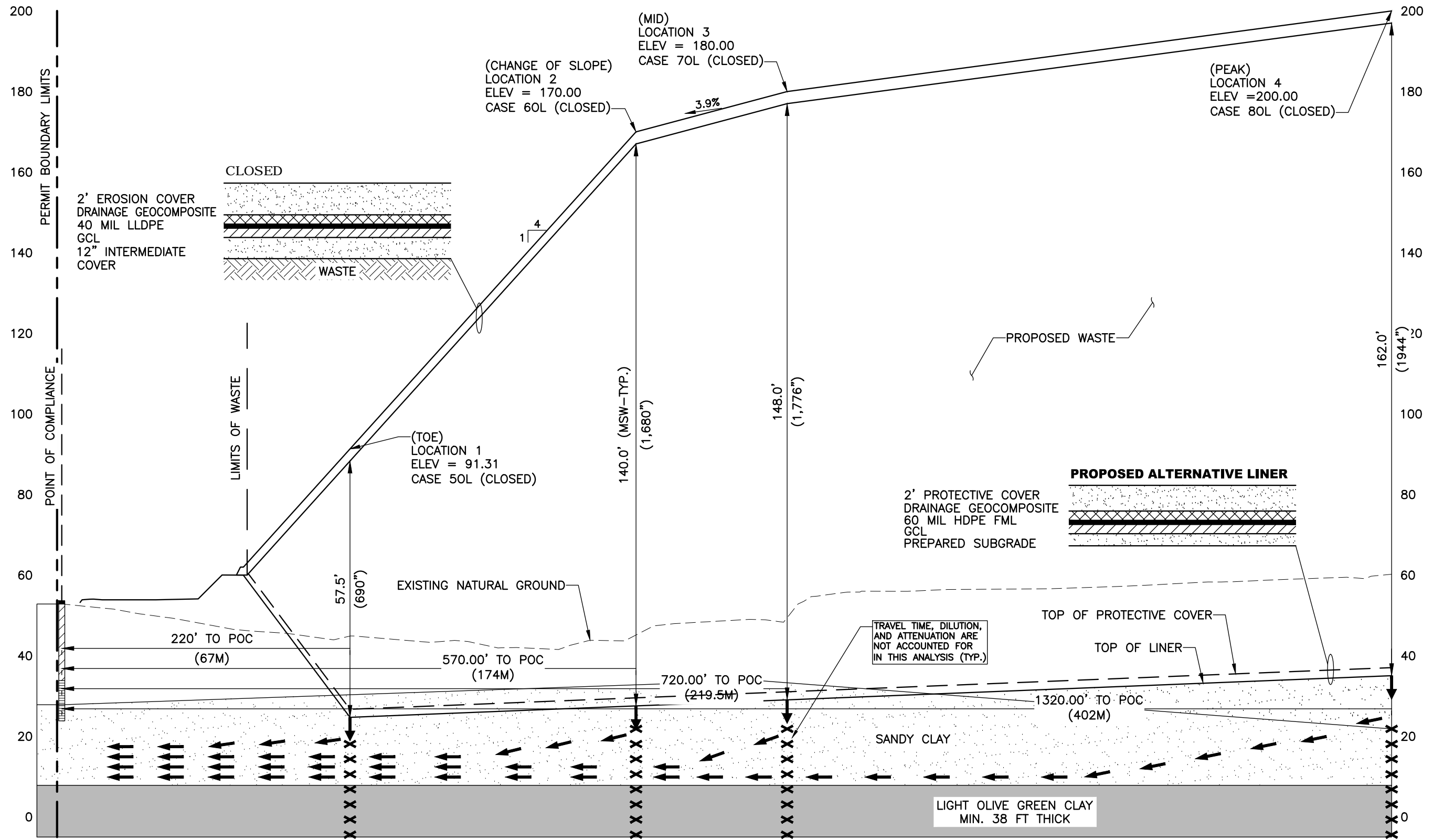


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PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL TYPICAL PROFILE-INTERIM  
 LANDFILL WITH ALTERNATIVE LINER  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

FIGURE:  
 III.5-A.5



**ALTERNATIVE LINER DEMONSTRATION - CLOSED LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE ALTERNATIVE LINER.
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

**MULTIMED INFORMATION**

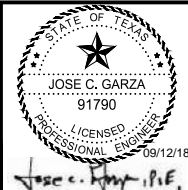
AVERAGE AQUIFER THICKNESS = 32.81FT (10M)  
 HYDRAULIC CONDUCTIVITY =  $4.12 \times 10^{-4}$  CM/SEC OR  
 130 M/YR  
 HYDRAULIC GRADIENT =  $i = 0.003125$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

SEP 11, 2018 2:48 PM TORREDO1809 I:\16JOBS\1610438\8514-CITY OF KINGSVILLE\8514-03\CAD-PART-III\8514-03-MULTIMED-SECTIONS.DWG

NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



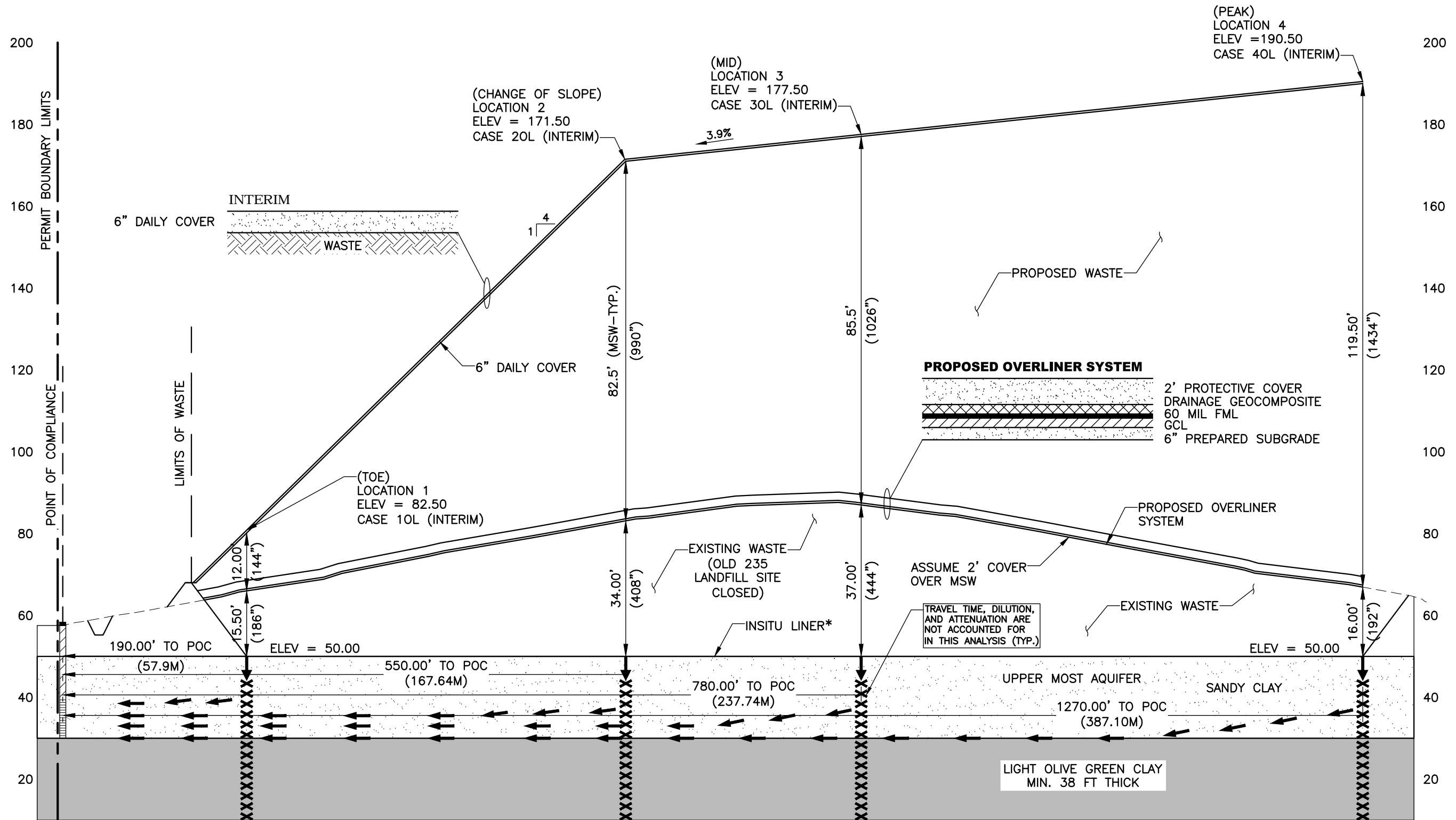
Hanson No.	1610438
Filename	
Scale	AS SHOWN
Date	09/12/2018
LAYOUT	DT 09/12/2018
DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

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PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL TYPICAL PROFILE-CLOSED  
 LANDFILL WITH ALTERNATIVE LINER  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:  
 III.5-A.6**



**\*OVERLINER DEMONSTRATION - INTERIM LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE INSITU LINER (ASSUMED EQUAL TO PERCOLATION THROUGH OVERLINER).
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

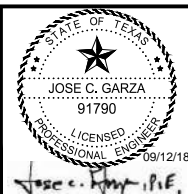
MULTIMED INFORMATION	
AVERAGE AQUIFER THICKNESS =	32.81FT (10M)
HYDRAULIC CONDUCTIVITY =	$4.12 \times 10^{-4}$ CM/SEC
HYDRAULIC GRADIENT = $i =$	0.002

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

SEP 11, 2018 2:51 PM TORRED1809 I:\16JOBS\1610438\8514-CITY OF KINGSVILLE\8514-03-CAD-PART-III\MULTIMED-SECTIONS.DWG

NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



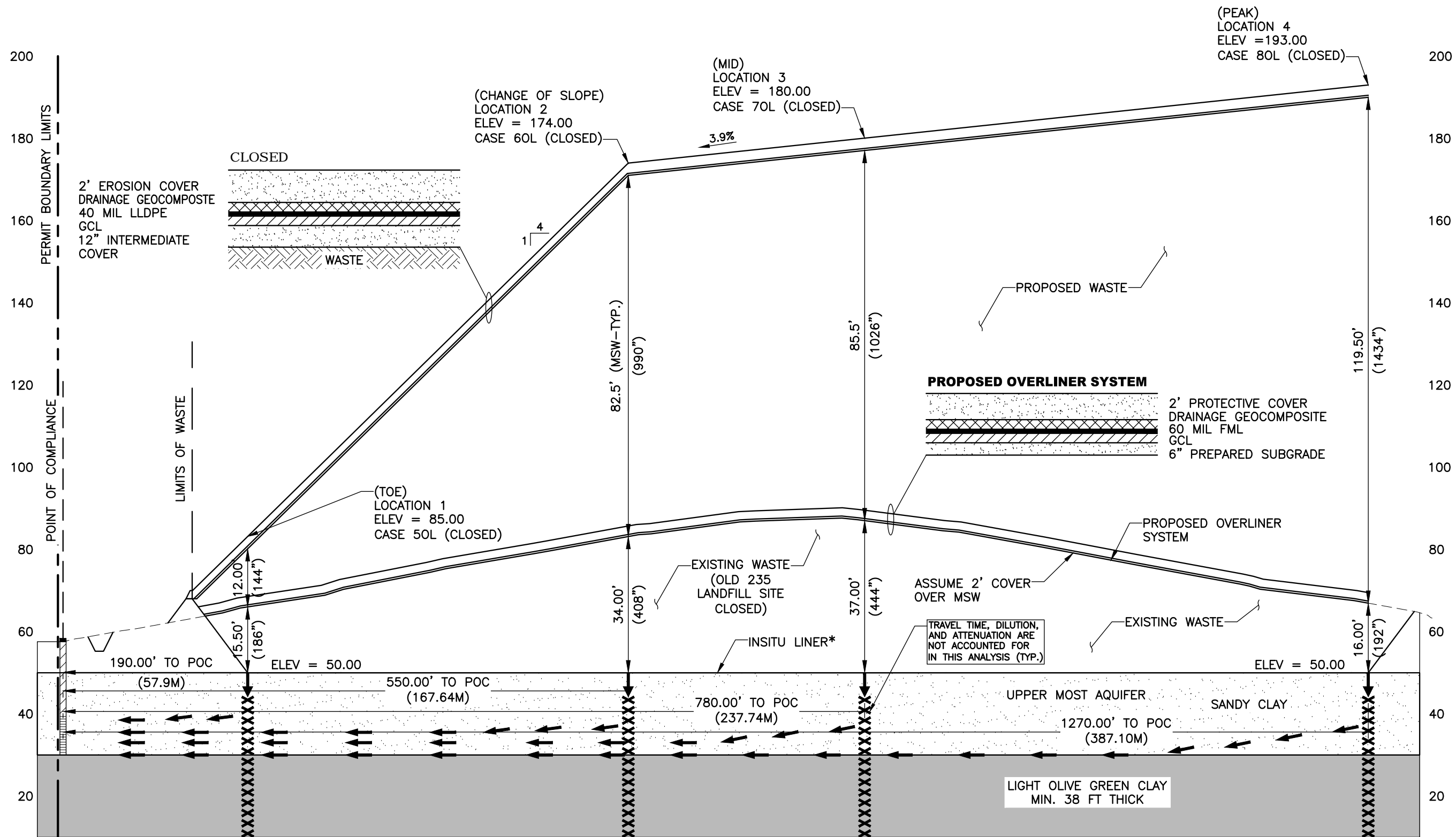
Hanson No.	1610438
Filename	
Scale	AS SHOWN
Date	09/12/2018
LAYOUT	DT 09/12/2018
DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

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PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL TYPICAL PROFILE-INTERIM  
 LANDFILL WITH ALTERNATIVE AND OVERLINER  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:**  
**III.5-A.7**



**\*OVERLINER DEMONSTRATION - CLOSED LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE INSITU LINER (ASSUMED EQUAL TO PERCOLATION THROUGH OVERLINER).
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

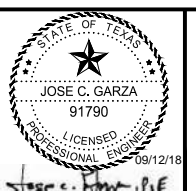
MULTIMED INFORMATION	
AVERAGE AQUIFER THICKNESS =	32.81FT (10M)
HYDRAULIC CONDUCTIVITY =	$4.12 \times 10^{-4}$ CM/SEC
HYDRAULIC GRADIENT =	$i = 0.002$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

SEP 11, 2018 2:51 PM TORRED1809 I:\16JOBS\1610438\8514-CITY OF KINGSVILLE\8514-03-CAD-PART-III\MULTIMED-SECTIONS.DWG

NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



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Filename	
Scale	AS SHOWN
Date	09/12/2018
LAYOUT	DT 09/12/2018
DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

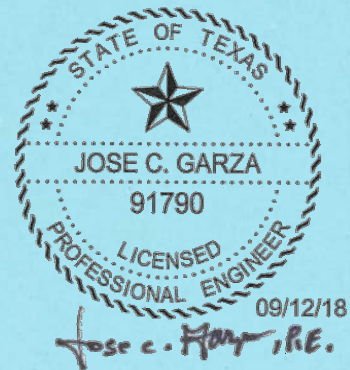


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PART III, ATTACHMENT 5, APPENDIX A  
 LANDFILL TYPICAL PROFILE-CLOSED  
 LANDFILL WITH ALTERNATIVE AND OVERLINER  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

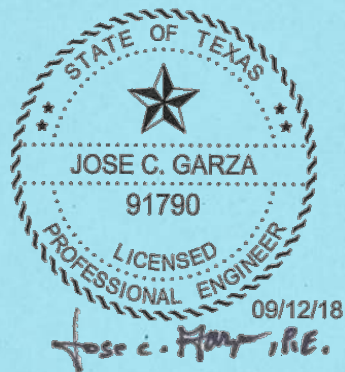
**FIGURE:  
 III.5-A.8**

APPENDIX B  
HELP MODEL ANALYSIS ALTERNATIVE LINER





APPENDIX B.1  
HELP MODEL/MULTIMED MODEL-SUMMARY OF CASES 1-8



Project No. 8514-3 Permit Amendment

Description: HELP Model/MULTIMED Model-Summary of Cases 1-8

Date: 3/01/17

By: JCG

**Case 1-Interim Landfill (Location 1)**- An open landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 57.5 feet of waste with 250 foot drain length at 2%, and 6 inches of daily soil cover.

**Case 2-Interim Landfill (Location 2)**- An open landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 140 feet of waste with 500 foot drain length at 2%, and 6 inches of daily soil cover.

**Case 3-Interim Landfill (Location 3)**- An open landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 148 feet of waste with 500 foot drain length at 2%, and 6 inches of daily soil cover.

**Case 4-Interim Landfill (Location 4)**- An open landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 162 feet of waste with 500 foot drain length at 2%, and 6 inches of daily soil cover.

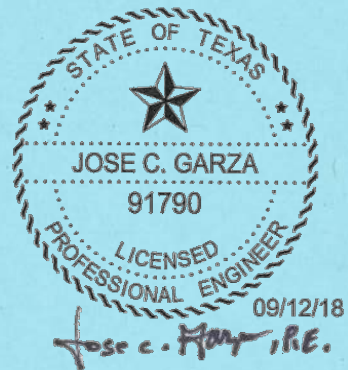
**Case 5-Closed Landfill (Location 1)** - A closed landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 57.5 feet of waste with 250 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case 6-Closed Landfill (Location 2)**- A closed landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 140 feet of waste with 500 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case 7-Closed Landfill (Location 3)**- A closed landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 12 inch protective soil layer (Protective Cover), 148 feet of waste with 500 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case 8-Closed Landfill (Location 4)**- A closed landfill with a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 162 feet of waste with 500 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

APPENDIX B.2  
HELP MODEL CASE SUMMARY

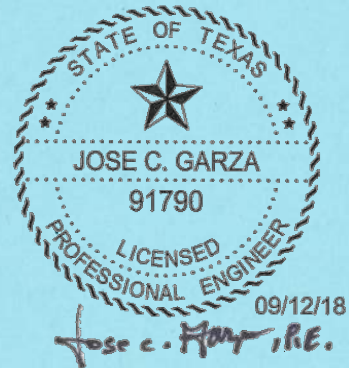


HELP MODEL CASE SUMMARY

Case Alternative Liner	Average Precipitation (IN/YR)	Average Runoff (IN/YR)	Average Evapotranspiration (IN/YR)	Average Percolation Through Liner (CF/YR)	Peak Percolation Through Liner (CF/DAY)	*Peak Percolation Through Liner (M/YR)
<b>Interim Landfill HELP Information</b>						
Location 1 • 57.5 feet of waste (Case 1)						
20 yr	25.74	2.391	21.632	0.004	0.000050	1.28E-07
Location 2 • 140 feet of waste (Case 2)						
20 yr	25.74	2.135	21.716	0.004	0.00007	1.79E-07
Location 3 • 148 feet of waste (Case 3)						
20 yr	25.74	2.197	21.691	0.004	0.00007	1.79E-07
Location 4 • 162 feet of waste (Case 4)						
20 yr	25.74	1.907	21.787	0.005	0.00007	1.79E-07
<b>Closed Landfill HELP Information</b>						
Location 1 • 57.5 feet of waste (Case 5)						
30 yr	27.20	1.880	21.749	0.001	0.00002	5.11E-08
Location 2 • 140 feet of waste (Case 6)						
30 yr	27.20	1.680	21.481	0.004	0.00002	5.11E-08
Location 3 • 148 feet of waste (Case 7)						
30 yr	27.20	1.711	21.470	0.004	0.00002	5.11E-08
Location 4 • 162 feet of waste (Case 8)						
30 yr	27.20	1.533	21.495	0.004	0.00002	5.11E-08

\* Determined Using Peak Daily Percolation/Leakage Rate Through GCL and Converted to (M/YR)  
 Example: ((.00005 FT<sup>3</sup>/Day-Acre)x(1 Acre/43,560 FT<sup>2</sup>)/(1 Meter/3.28 FT)) x (365 Days/1 YR)= 1.28 x 10<sup>-7</sup> M/YR

APPENDIX B.3  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 1-  
LOCATION 1



CASE120Y.OUT

↑  
\*\*\*\*\*  
\*\*\*\*\*  
\*\*  
\*\*  
\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
\*\*  
\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE1.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE120Y.OUT

TIME: 16:43 DATE: 3/13/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 1 (Location 1)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2393 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 690.00 INCHES  
Page 1

FOR PERMIT PURPOSES ONLY

CASE120Y.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2905 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3244 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0152 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

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CASE120Y.OUT

WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 FAIR STAND OF GRASS, A SURFACE SLOPE OF 25.%  
 AND A SLOPE LENGTH OF 100. FEET.

SCS RUNOFF CURVE NUMBER = 89.50  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.124 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 209.820 INCHES  
 TOTAL INITIAL WATER = 209.820 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)



FOR PERMIT PURPOSES ONLY

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	CASE120Y.OUT MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
<b>RUNOFF</b>						
TOTALS	0.015 0.380	0.067 0.193	0.006 0.784	0.104 0.181	0.281 0.073	0.288 0.020
STD. DEVIATIONS	0.043 0.817	0.081 0.198	0.009 0.914	0.237 0.274	0.504 0.212	0.348 0.070
<b>EVAPOTRANSPIRATION</b>						
TOTALS	0.939 2.037	2.086 1.875	1.297 3.620	1.241 2.256	1.988 1.089	2.114 1.091
STD. DEVIATIONS	0.543 1.606	0.911 1.312	0.701 1.225	0.915 1.220	1.322 0.757	1.388 0.583
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 4</b>						
TOTALS	0.0660 0.1446	0.0208 0.1781	0.0717 0.1018	0.0580 0.4110	0.0362 0.4038	0.0534 0.1914
STD. DEVIATIONS	0.0860 0.2593	0.0317 0.3508	0.1423 0.2000	0.1051 0.5937	0.0619 0.7436	0.1057 0.3248
<b>PERCOLATION/LEAKAGE THROUGH LAYER 6</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

FOR PERMIT PURPOSES ONLY

CASE120Y.OUT

DAILY AVERAGE HEAD ON TOP OF LAYER 5

-----						
AVERAGES	0.0005	0.0002	0.0005	0.0004	0.0003	0.0004
	0.0010	0.0013	0.0007	0.0029	0.0030	0.0014
STD. DEVIATIONS	0.0006	0.0002	0.0010	0.0008	0.0004	0.0008
	0.0018	0.0025	0.0015	0.0042	0.0055	0.0023

\*\*\*\*\*

\*\*\*\*\*

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

-----				
	INCHES		CU. FEET	PERCENT
-----				
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.391	( 1.2854)	8679.79	9.288
EVAPOTRANSPIRATION	21.632	( 3.6809)	78522.88	84.028
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.73689	( 1.43677)	6304.902	6.74690
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.001	( 0.001)		
CHANGE IN WATER STORAGE	-0.016	( 0.5277)	-58.66	-0.063

\*\*\*\*\*

↑

\*\*\*\*\*

PEAK DAILY VALUES FOR YEARS 1 THROUGH 20

-----		
	(INCHES)	(CU. FT.)
-----		
PRECIPITATION	5.07	18404.102
RUNOFF	2.138	7761.3745
DRAINAGE COLLECTED FROM LAYER 4	0.16595	602.40332
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00005
AVERAGE HEAD ON TOP OF LAYER 5	0.037	
MAXIMUM HEAD ON TOP OF LAYER 5	0.072	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	2.4 FEET	
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3879

CASE120Y.OUT

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

\*\*\*\*\*

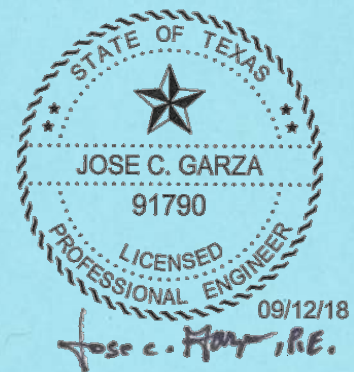
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FINAL WATER STORAGE AT END OF YEAR 20

LAYER	(INCHES)	(VOL/VOL)
1	1.4211	0.2369
2	200.1899	0.2901
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
SNOW WATER	0.000	

\*\*\*\*\*  
 \*\*\*\*\*

**APPENDIX B.4**  
**HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 2-**  
**LOCATION 2**



CASE220Y.OUT

```
*****
*****
**
**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE          **
**          HELP MODEL VERSION 3.07 (1 NOVEMBER 1997)              **
**          DEVELOPED BY ENVIRONMENTAL LABORATORY                  **
**          USAE WATERWAYS EXPERIMENT STATION                    **
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY       **
**
**
*****
*****
```

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE2.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE220Y.OUT

TIME: 16:53 DATE: 3/13/2017

```
*****
*****
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 2 (LOCATION 2)
*****
*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2391 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 1680.00 INCHES  
Page 1

FOR PERMIT PURPOSES ONLY

CASE220Y.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2914 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3245 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0205 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE220Y.OUT

WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #13 WITH A FAIR STAND OF GRASS, A SURFACE SLOPE OF 25.% AND A SLOPE LENGTH OF 350. FEET.

SCS RUNOFF CURVE NUMBER = 88.80  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.124 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 498.905 INCHES  
 TOTAL INITIAL WATER = 498.905 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

FOR PERMIT PURPOSES ONLY

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	CASE220Y.OUT MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
<b>RUNOFF</b>						
TOTALS	0.012 0.350	0.055 0.170	0.003 0.716	0.092 0.149	0.254 0.066	0.252 0.016
STD. DEVIATIONS	0.037 0.770	0.071 0.181	0.006 0.864	0.216 0.234	0.479 0.199	0.315 0.057
<b>EVAPOTRANSPIRATION</b>						
TOTALS	0.932 2.048	2.093 1.899	1.304 3.628	1.251 2.264	1.993 1.098	2.128 1.076
STD. DEVIATIONS	0.540 1.634	0.899 1.319	0.714 1.222	0.930 1.208	1.317 0.786	1.382 0.592
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 4</b>						
TOTALS	0.0714 0.1629	0.0325 0.1994	0.0735 0.1144	0.0598 0.4250	0.0433 0.4282	0.0680 0.2290
STD. DEVIATIONS	0.0918 0.3040	0.0521 0.4252	0.1373 0.2386	0.1034 0.5913	0.0700 0.7365	0.1461 0.4175
<b>PERCOLATION/LEAKAGE THROUGH LAYER 6</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)



FOR PERMIT PURPOSES ONLY

CASE220Y.OUT

DAILY AVERAGE HEAD ON TOP OF LAYER 5

-----						
AVERAGES	0.0010	0.0005	0.0010	0.0009	0.0006	0.0010
	0.0023	0.0028	0.0017	0.0060	0.0063	0.0033
STD. DEVIATIONS	0.0013	0.0008	0.0020	0.0015	0.0010	0.0021
	0.0043	0.0061	0.0035	0.0084	0.0108	0.0059

\*\*\*\*\*

\*\*\*\*\*

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

-----				
	INCHES		CU. FEET	PERCENT
	-----		-----	-----
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.135	( 1.1936)	7751.57	8.295
EVAPOTRANSPIRATION	21.716	( 3.6903)	78829.24	84.355
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.90751	( 1.54789)	6924.269	7.40968
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.002	( 0.002)		
CHANGE IN WATER STORAGE	-0.015	( 0.5511)	-56.19	-0.060

\*\*\*\*\*

\*\*\*\*\*

PEAK DAILY VALUES FOR YEARS 1 THROUGH 20

-----		
	(INCHES)	(CU. FT.)
	-----	-----
PRECIPITATION	5.07	18404.102
RUNOFF	2.088	7578.4883
DRAINAGE COLLECTED FROM LAYER 4	0.16062	583.03455
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00007
AVERAGE HEAD ON TOP OF LAYER 5	0.071	
MAXIMUM HEAD ON TOP OF LAYER 5	0.141	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	1.7 FEET	
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3901

CASE220Y.OUT

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

\*\*\*\*\*

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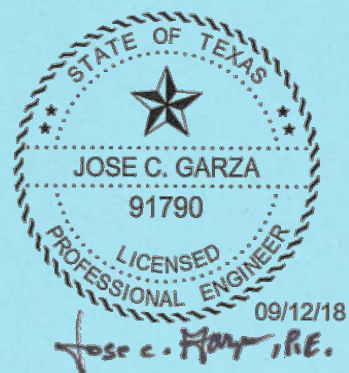
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FINAL WATER STORAGE AT END OF YEAR 20

LAYER	(INCHES)	(VOL/VOL)
1	1.4393	0.2399
2	489.2699	0.2912
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
SNOW WATER	0.000	

\*\*\*\*\*

**APPENDIX B.5**  
**HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 3-**  
**LOCATION 3**



CASE320Y.OUT

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\*\*\*\*\*  
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\*\*  
\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
\*\*  
\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE3.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE320Y.OUT

TIME: 9:42 DATE: 3/ 3/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 3 (LOCATION 3)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2391 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 1776.00 INCHES  
Page 1

FOR PERMIT PURPOSES ONLY

CASE320Y.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2914 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3245 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0205 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE320Y.OUT

WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #13 WITH A FAIR STAND OF GRASS, A SURFACE SLOPE OF 12.% AND A SLOPE LENGTH OF 200. FEET.

SCS RUNOFF CURVE NUMBER = 89.00  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.124 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 526.937 INCHES  
 TOTAL INITIAL WATER = 526.937 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

FOR PERMIT PURPOSES ONLY

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	CASE320Y.OUT MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
<b>RUNOFF</b>						
TOTALS	0.013 0.358	0.058 0.176	0.004 0.733	0.095 0.155	0.261 0.067	0.260 0.017
STD. DEVIATIONS	0.038 0.783	0.074 0.186	0.007 0.879	0.221 0.241	0.486 0.202	0.324 0.058
<b>EVAPOTRANSPIRATION</b>						
TOTALS	0.931 2.045	2.093 1.896	1.302 3.629	1.250 2.258	1.993 1.099	2.121 1.074
STD. DEVIATIONS	0.537 1.629	0.898 1.315	0.710 1.227	0.928 1.202	1.312 0.786	1.384 0.593
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 4</b>						
TOTALS	0.0691 0.1587	0.0357 0.1953	0.0747 0.1104	0.0581 0.4160	0.0416 0.4200	0.0640 0.2277
STD. DEVIATIONS	0.0916 0.2950	0.0544 0.4190	0.1437 0.2386	0.1048 0.5831	0.0687 0.7316	0.1397 0.4157
<b>PERCOLATION/LEAKAGE THROUGH LAYER 6</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

FOR PERMIT PURPOSES ONLY

CASE320Y.OUT

DAILY AVERAGE HEAD ON TOP OF LAYER 5

AVERAGES	0.0010	0.0006	0.0011	0.0009	0.0006	0.0009
	0.0023	0.0028	0.0016	0.0059	0.0062	0.0032
STD. DEVIATIONS	0.0013	0.0009	0.0020	0.0015	0.0010	0.0021
	0.0042	0.0060	0.0035	0.0083	0.0108	0.0059

\*\*\*\*\*

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

	INCHES		CU. FEET	PERCENT
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.197	( 1.2161)	7975.32	8.534
EVAPOTRANSPIRATION	21.691	( 3.6830)	78736.87	84.257
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.87134	( 1.53436)	6792.955	7.26917
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.002	( 0.002)		
CHANGE IN WATER STORAGE	-0.015	( 0.5521)	-56.24	-0.060

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 20

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.106	7646.4312
DRAINAGE COLLECTED FROM LAYER 4	0.16174	587.13318
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00007
AVERAGE HEAD ON TOP OF LAYER 5	0.071	
MAXIMUM HEAD ON TOP OF LAYER 5	0.142	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	2.9 FEET	
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3893



CASE320Y.OUT

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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↑

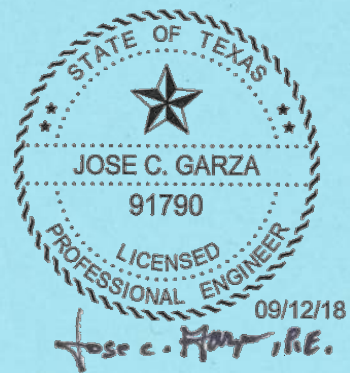
\*\*\*\*\*

FINAL WATER STORAGE AT END OF YEAR 20

LAYER	(INCHES)	(VOL/VOL)
1	1.4394	0.2399
2	517.3019	0.2913
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
SNOW WATER	0.000	

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APPENDIX B.6  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 4-  
LOCATION 4



FOR PERMIT PURPOSES ONLY

CASE420Y.OUT

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\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
\*\*  
\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEY20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE4.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE420Y.OUT

TIME: 17: 0 DATE: 3/13/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 4 (LOCATION 4)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 1944.00 INCHES

CASE420Y.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2914 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3246 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0206 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE420Y.OUT

WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 FAIR STAND OF GRASS, A SURFACE SLOPE OF 4%  
 AND A SLOPE LENGTH OF 600. FEET.

SCS RUNOFF CURVE NUMBER = 88.00  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 1.920 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 575.790 INCHES  
 TOTAL INITIAL WATER = 575.790 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

FOR PERMIT PURPOSES ONLY

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	CASE420Y.OUT MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
<b>RUNOFF</b>						
TOTALS	0.010 0.322	0.044 0.145	0.002 0.650	0.080 0.131	0.229 0.058	0.222 0.013
STD. DEVIATIONS	0.032 0.721	0.059 0.160	0.004 0.809	0.198 0.208	0.452 0.182	0.284 0.047
<b>EVAPOTRANSPIRATION</b>						
TOTALS	0.926 2.063	2.091 1.908	1.307 3.649	1.259 2.262	2.002 1.101	2.140 1.080
STD. DEVIATIONS	0.553 1.651	0.908 1.324	0.722 1.215	0.938 1.209	1.315 0.795	1.392 0.582
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 4</b>						
TOTALS	0.0726 0.1774	0.0392 0.2168	0.0796 0.1255	0.0589 0.4497	0.0482 0.4595	0.0756 0.2524
STD. DEVIATIONS	0.0955 0.3182	0.0557 0.4582	0.1545 0.2771	0.1063 0.6082	0.0799 0.7549	0.1563 0.4589
<b>PERCOLATION/LEAKAGE THROUGH LAYER 6</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

FOR PERMIT PURPOSES ONLY

CASE420Y.OUT

DAILY AVERAGE HEAD ON TOP OF LAYER 5

AVERAGES	0.0010	0.0006	0.0011	0.0009	0.0007	0.0011
	0.0025	0.0031	0.0018	0.0064	0.0068	0.0036
STD. DEVIATIONS	0.0014	0.0009	0.0022	0.0016	0.0011	0.0023
	0.0045	0.0065	0.0041	0.0087	0.0111	0.0065

\*\*\*\*\*

\*\*\*\*\*

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

	INCHES		CU. FEET	PERCENT
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	1.907	( 1.1083)	6921.00	7.406
EVAPOTRANSPIRATION	21.787	( 3.6980)	79085.98	84.630
LATERAL DRAINAGE COLLECTED FROM LAYER 4	2.05535	( 1.61442)	7460.923	7.98396
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000	( 0.00000)	0.005	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.002	( 0.002)		
CHANGE IN WATER STORAGE	-0.005	( 0.5759)	-18.99	-0.020

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 20

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.016	7318.0361
DRAINAGE COLLECTED FROM LAYER 4	0.16131	585.57281
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00007
AVERAGE HEAD ON TOP OF LAYER 5	0.071	
MAXIMUM HEAD ON TOP OF LAYER 5	0.142	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	1.4 FEET	
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3947

CASE420Y.OUT

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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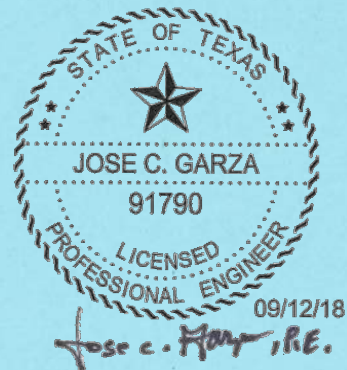
FINAL WATER STORAGE AT END OF YEAR 20

LAYER	(INCHES)	(VOL/VOL)
1	1.4410	0.2402
2	566.3580	0.2913
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
SNOW WATER	0.000	

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APPENDIX B.7  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 5-  
LOCATION 1



CASE530Y.OUT

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\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
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\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE5.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE530Y.OUT

TIME: 8:21 DATE: 3/14/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 5 (LOCATION 1)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2719 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES

CASE530Y.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 18

THICKNESS = 690.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL

CASE530Y.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE530Y.OUT  
 EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 25.0%  
 AND A SLOPE LENGTH OF 100. FEET.

SCS RUNOFF CURVE NUMBER = 85.60  
 FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.674 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 219.926 INCHES  
 TOTAL INITIAL WATER = 219.926 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 3.50  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
-----	-----	-----	-----	-----	-----

FOR PERMIT PURPOSES ONLY

56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

CASE530Y.OUT

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
<b>RUNOFF</b>						
TOTALS	0.007 0.342	0.022 0.218	0.005 0.608	0.051 0.191	0.188 0.067	0.174 0.007
STD. DEVIATIONS	0.022 0.789	0.041 0.366	0.026 0.822	0.171 0.318	0.500 0.265	0.243 0.028
<b>EVAPOTRANSPIRATION</b>						
TOTALS	1.093 1.754	1.768 2.186	1.331 3.474	1.252 2.435	1.966 1.312	2.071 1.107
STD. DEVIATIONS	0.665 1.256	0.864 1.504	0.621 1.237	0.803 1.136	1.191 0.899	1.228 0.681
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 2</b>						
TOTALS	0.0698 0.3318	0.2237 0.3490	0.1155 0.8839	0.0457 0.7081	0.1805 0.2403	0.3327 0.0780
STD. DEVIATIONS	0.1315 0.5455	0.2604 0.5857	0.1270 0.9977	0.1234 0.7204	0.2785 0.3203	0.4691 0.1153
<b>PERCOLATION/LEAKAGE THROUGH LAYER 4</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 8</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

FOR PERMIT PURPOSES ONLY

CASE530Y.OUT						
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
PERCOLATION/LEAKAGE THROUGH LAYER 10						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 3						
AVERAGES	0.0005	0.0017	0.0008	0.0003	0.0013	0.0139
	0.0206	0.0177	0.1061	0.0240	0.0018	0.0006
STD. DEVIATIONS	0.0009	0.0020	0.0009	0.0009	0.0020	0.0415
	0.1028	0.0537	0.2641	0.0529	0.0024	0.0008

DAILY AVERAGE HEAD ON TOP OF LAYER 9						
AVERAGES	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES		CU. FEET	PERCENT
PRECIPITATION	27.20	( 5.704)	98722.7	100.00
RUNOFF	1.880	( 1.2157)	6825.49	6.914
EVAPOTRANSPIRATION	21.749	( 3.7373)	78947.65	79.969
LATERAL DRAINAGE COLLECTED FROM LAYER 2	3.55912	( 1.91851)	12919.604	13.08676
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00001	( 0.00001)	0.023	0.00002
AVERAGE HEAD ON TOP OF LAYER 3	0.016	( 0.026)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00001	( 0.00001)	0.022	0.00002
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000	( 0.00000)	0.001	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000	( 0.000)		
CHANGE IN WATER STORAGE	0.008	( 0.4489)	29.91	0.030

FOR PERMIT PURPOSES ONLY

CASE530Y.OUT

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PEAK DAILY VALUES FOR YEARS	1 THROUGH 30	
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.1035
DRAINAGE COLLECTED FROM LAYER 2	0.91251	3312.41650
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000012	0.04380
AVERAGE HEAD ON TOP OF LAYER 3	14.568	
MAXIMUM HEAD ON TOP OF LAYER 3	18.997	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	87.9 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.00001	0.03665
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.000	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4285
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2210

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 30		
LAYER	(INCHES)	(VOL/VOL)
1	6.7730	0.2822

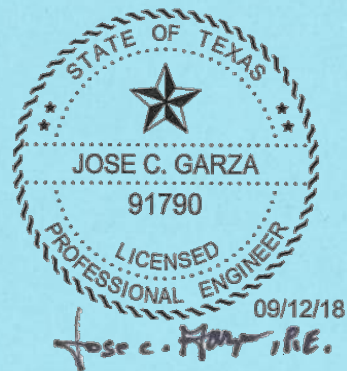


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CASE530Y.OUT		
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	201.4800	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
SNOW WATER	0.000	

\*\*\*\*\*  
\*\*\*\*\*

APPENDIX B.8  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 6-  
LOCATION 2



CASE630Y.OUT

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\*\*\*\*\*  
\*\* \*\*  
\*\* \*\*  
\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
\*\* \*\*  
\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE6.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE630Y.OUT

TIME: 8:29 DATE: 3/14/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 6 (LOCATION 2)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2754 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES  
Page 1

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CASE630Y.OUT  
 POROSITY = 0.8500 VOL/VOL  
 FIELD CAPACITY = 0.0100 VOL/VOL  
 WILTING POINT = 0.0050 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
 SLOPE = 2.00 PERCENT  
 DRAINAGE LENGTH = 500.0 FEET

LAYER 3  
 -----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
 MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
 POROSITY = 0.0000 VOL/VOL  
 FIELD CAPACITY = 0.0000 VOL/VOL  
 WILTING POINT = 0.0000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
 FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
 FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
 FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
 -----

TYPE 3 - BARRIER SOIL LINER  
 MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
 POROSITY = 0.7500 VOL/VOL  
 FIELD CAPACITY = 0.7470 VOL/VOL  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS = 1680.00 INCHES  
 POROSITY = 0.6710 VOL/VOL  
 FIELD CAPACITY = 0.2920 VOL/VOL

CASE630Y.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

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CASE630Y.OUT  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 25.0%  
 AND A SLOPE LENGTH OF 350. FEET.

SCS RUNOFF CURVE NUMBER = 84.60  
 FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.757 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 509.089 INCHES  
 TOTAL INITIAL WATER = 509.089 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 3.50  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
-----	-----	-----	-----	-----	-----

FOR PERMIT PURPOSES ONLY

				CASE630Y.OUT	
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
<b>RUNOFF</b>						
TOTALS	0.005 0.325	0.016 0.191	0.004 0.568	0.047 0.161	0.169 0.044	0.145 0.004
STD. DEVIATIONS	0.016 0.770	0.032 0.339	0.020 0.843	0.171 0.294	0.495 0.176	0.206 0.018
<b>EVAPOTRANSPIRATION</b>						
TOTALS	1.081 1.728	1.760 2.139	1.314 3.444	1.251 2.384	1.928 1.304	2.038 1.109
STD. DEVIATIONS	0.675 1.204	0.902 1.461	0.615 1.229	0.801 1.106	1.168 0.896	1.210 0.689
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 2</b>						
TOTALS	0.0809 0.3796	0.2406 0.4275	0.1121 0.9447	0.0567 0.7920	0.2251 0.2900	0.3948 0.0857
STD. DEVIATIONS	0.1435 0.6067	0.2996 0.6486	0.1230 0.9618	0.1528 0.8406	0.3265 0.4048	0.5469 0.1200
<b>PERCOLATION/LEAKAGE THROUGH LAYER 4</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 8</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

FOR PERMIT PURPOSES ONLY

CASE630Y.OUT						
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
PERCOLATION/LEAKAGE THROUGH LAYER 10						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
-----

DAILY AVERAGE HEAD ON TOP OF LAYER 3						
AVERAGES	0.0012	0.0038	0.0016	0.0008	0.0104	0.0589
	0.0681	0.0899	0.3548	0.1774	0.0241	0.0012
STD. DEVIATIONS	0.0020	0.0047	0.0017	0.0022	0.0324	0.1912
	0.2573	0.2432	0.7287	0.4575	0.1013	0.0017

DAILY AVERAGE HEAD ON TOP OF LAYER 9						
AVERAGES	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES		CU. FEET	PERCENT
PRECIPITATION	27.20	( 5.704)	98722.7	100.00
RUNOFF	1.680	( 1.1902)	6099.48	6.178
EVAPOTRANSPIRATION	21.481	( 3.7202)	77976.52	78.985
LATERAL DRAINAGE COLLECTED FROM LAYER 2	4.02954	( 2.05403)	14627.235	14.81649
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00002	( 0.00003)	0.077	0.00008
AVERAGE HEAD ON TOP OF LAYER 3	0.066	( 0.096)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00002	( 0.00003)	0.073	0.00007
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000	( 0.000)		
CHANGE IN WATER STORAGE	0.005	( 0.4311)	19.37	0.020



FOR PERMIT PURPOSES ONLY

CASE630Y.OUT

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	30
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.0957
DRAINAGE COLLECTED FROM LAYER 2	0.45365	1646.75024
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000023	0.08305
AVERAGE HEAD ON TOP OF LAYER 3	22.812	
MAXIMUM HEAD ON TOP OF LAYER 3	31.119	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	158.8 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.00002	0.07910
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.000	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4300
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2210

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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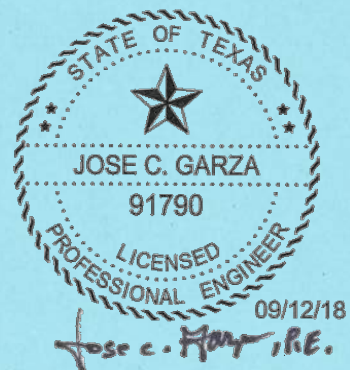
FINAL WATER STORAGE AT END OF YEAR 30		
LAYER	(INCHES)	(VOL/VOL)
1	6.7691	0.2820

FOR PERMIT PURPOSES ONLY

CASE630Y.OUT		
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	490.5600	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
SNOW WATER	0.000	

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\*\*\*\*\*

APPENDIX B.9  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 7-  
LOCATION 3



CASE730Y.OUT

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\*\* \*\*  
\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
\*\* \*\*  
\*\*\*\*\*  
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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE7.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE730Y.OUT

TIME: 10:27 DATE: 3/ 3/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 7 (LOCATION 3)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2734 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES  
Page 1

CASE730Y.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18

THICKNESS = 1776.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL

CASE730Y.OUT

WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
 -----

TYPE 2 - LATERAL DRAINAGE LAYER  
 MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
 POROSITY = 0.8500 VOL/VOL  
 FIELD CAPACITY = 0.0100 VOL/VOL  
 WILTING POINT = 0.0050 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
 SLOPE = 2.00 PERCENT  
 DRAINAGE LENGTH = 500.0 FEET

LAYER 9  
 -----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
 MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
 POROSITY = 0.0000 VOL/VOL  
 FIELD CAPACITY = 0.0000 VOL/VOL  
 WILTING POINT = 0.0000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
 FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
 FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
 FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
 -----

TYPE 3 - BARRIER SOIL LINER  
 MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
 POROSITY = 0.7500 VOL/VOL  
 FIELD CAPACITY = 0.7470 VOL/VOL  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE730Y.OUT  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #13 WITH A GOOD STAND OF GRASS, A SURFACE SLOPE OF 12.2% AND A SLOPE LENGTH OF 200. FEET.

SCS RUNOFF CURVE NUMBER = 84.80  
 FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.709 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 537.073 INCHES  
 TOTAL INITIAL WATER = 537.073 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 3.50  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
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FOR PERMIT PURPOSES ONLY

				CASE730Y.OUT		
56.30	59.30	65.90	73.00	78.10	82.70	
84.90	85.00	81.50	74.00	65.00	59.10	

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
<b>RUNOFF</b>						
TOTALS	0.005 0.327	0.017 0.197	0.004 0.576	0.048 0.165	0.172 0.045	0.150 0.004
STD. DEVIATIONS	0.017 0.771	0.034 0.344	0.021 0.849	0.172 0.296	0.495 0.177	0.212 0.019
<b>EVAPOTRANSPIRATION</b>						
TOTALS	1.078 1.733	1.759 2.138	1.312 3.441	1.250 2.378	1.927 1.302	2.039 1.114
STD. DEVIATIONS	0.678 1.208	0.893 1.465	0.613 1.222	0.800 1.103	1.166 0.899	1.215 0.690
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 2</b>						
TOTALS	0.0770 0.3734	0.2413 0.4229	0.1130 0.9423	0.0569 0.7940	0.2266 0.2864	0.3893 0.0853
STD. DEVIATIONS	0.1384 0.6049	0.3007 0.6418	0.1237 0.9643	0.1480 0.8378	0.3277 0.4003	0.5341 0.1205
<b>PERCOLATION/LEAKAGE THROUGH LAYER 4</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 8</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000



FOR PERMIT PURPOSES ONLY

CASE730Y.OUT						
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
PERCOLATION/LEAKAGE THROUGH LAYER 10						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 3						
-----						
AVERAGES	0.0011	0.0038	0.0016	0.0008	0.0105	0.0584
	0.0675	0.0853	0.3606	0.1844	0.0215	0.0012
STD. DEVIATIONS	0.0020	0.0047	0.0018	0.0022	0.0325	0.1892
	0.2555	0.2308	0.7392	0.4599	0.0994	0.0017

DAILY AVERAGE HEAD ON TOP OF LAYER 9						
-----						
AVERAGES	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES		CU. FEET	PERCENT
	-----		-----	-----
PRECIPITATION	27.20	( 5.704)	98722.7	100.00
RUNOFF	1.711	( 1.1947)	6210.31	6.291
EVAPOTRANSPIRATION	21.470	( 3.7084)	77936.37	78.945
LATERAL DRAINAGE COLLECTED FROM LAYER 2	4.00840	( 2.03256)	14550.508	14.73877
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00002	( 0.00003)	0.078	0.00008
AVERAGE HEAD ON TOP OF LAYER 3	0.066	( 0.097)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00002	( 0.00003)	0.073	0.00007
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000	( 0.000)		
CHANGE IN WATER STORAGE	0.007	( 0.4345)	25.43	0.026

FOR PERMIT PURPOSES ONLY

CASE730Y.OUT

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	30
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.0957
DRAINAGE COLLECTED FROM LAYER 2	0.45365	1646.75073
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000023	0.08307
AVERAGE HEAD ON TOP OF LAYER 3	22.816	
MAXIMUM HEAD ON TOP OF LAYER 3	31.124	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	158.8 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.00002	0.07912
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.000	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4300
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2210

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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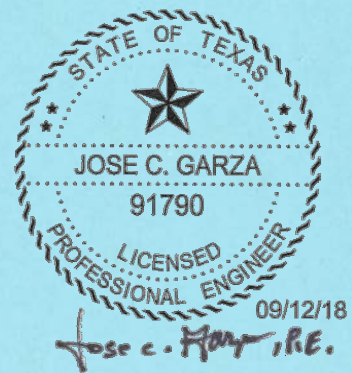
FINAL WATER STORAGE AT END OF YEAR 30		
LAYER	(INCHES)	(VOL/VOL)
1	6.7714	0.2821

FOR PERMIT PURPOSES ONLY

CASE730Y.OUT		
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	518.5920	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
SNOW WATER	0.000	

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APPENDIX B.10  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 8-  
LOCATION 4



CASE830Y.OUT

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\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE8.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE830Y.OUT

TIME: 8:39 DATE: 3/14/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE 8 (LOCATION 4)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2733 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES  
Page 1

CASE830Y.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 18

THICKNESS = 1944.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL

CASE830Y.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 500.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

FOR PERMIT PURPOSES ONLY

CASE830Y.OUT  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #13 WITH A GOOD STAND OF GRASS, A SURFACE SLOPE OF 4.4% AND A SLOPE LENGTH OF 600. FEET.

SCS RUNOFF CURVE NUMBER = 83.40  
 FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.708 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 586.128 INCHES  
 TOTAL INITIAL WATER = 586.128 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 3.50  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR KINGSVILLE TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
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FOR PERMIT PURPOSES ONLY

				CASE830Y.OUT		
56.30	59.30	65.90	73.00	78.10	82.70	
84.90	85.00	81.50	74.00	65.00	59.10	

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

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AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
<b>RUNOFF</b>						
TOTALS	0.003 0.320	0.011 0.167	0.003 0.536	0.043 0.138	0.154 0.039	0.117 0.002
STD. DEVIATIONS	0.012 0.765	0.024 0.317	0.015 0.853	0.167 0.285	0.494 0.166	0.168 0.012
<b>EVAPOTRANSPIRATION</b>						
TOTALS	1.075 1.740	1.755 2.149	1.316 3.445	1.246 2.375	1.943 1.304	2.036 1.111
STD. DEVIATIONS	0.680 1.225	0.890 1.476	0.616 1.225	0.799 1.098	1.174 0.904	1.212 0.695
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 2</b>						
TOTALS	0.0871 0.3740	0.2477 0.4325	0.1143 0.9802	0.0601 0.8286	0.2280 0.2979	0.4259 0.0849
STD. DEVIATIONS	0.1585 0.6004	0.3090 0.6575	0.1186 0.9888	0.1609 0.8731	0.3250 0.4168	0.5887 0.1196
<b>PERCOLATION/LEAKAGE THROUGH LAYER 4</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
<b>LATERAL DRAINAGE COLLECTED FROM LAYER 8</b>						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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CASE830Y.OUT  
0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 10

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
-----

DAILY AVERAGE HEAD ON TOP OF LAYER 3

AVERAGES	0.0012	0.0039	0.0016	0.0009	0.0104	0.0748
	0.0679	0.0824	0.3707	0.2120	0.0248	0.0012
STD. DEVIATIONS	0.0023	0.0048	0.0017	0.0024	0.0323	0.2328
	0.2719	0.2347	0.7766	0.4906	0.1168	0.0017

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES		CU. FEET	PERCENT
PRECIPITATION	27.20	( 5.704)	98722.7	100.00
RUNOFF	1.533	( 1.1930)	5565.96	5.638
EVAPOTRANSPIRATION	21.495	( 3.7381)	78026.06	79.036
LATERAL DRAINAGE COLLECTED FROM LAYER 2	4.16123	( 2.10988)	15105.281	15.30072
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00002	( 0.00003)	0.083	0.00008
AVERAGE HEAD ON TOP OF LAYER 3	0.071	( 0.104)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00002	( 0.00003)	0.079	0.00008
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000	( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000	( 0.000)		
CHANGE IN WATER STORAGE	0.007	( 0.4342)	25.30	0.026

CASE830Y.OUT

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	30
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.0947
DRAINAGE COLLECTED FROM LAYER 2	0.45365	1646.74548
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000023	0.08285
AVERAGE HEAD ON TOP OF LAYER 3	22.774	
MAXIMUM HEAD ON TOP OF LAYER 3	31.078	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	158.7 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.00002	0.07933
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.000	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4300
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2210

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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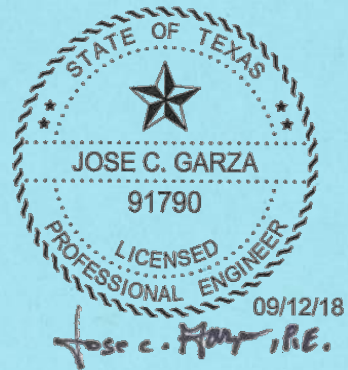
FINAL WATER STORAGE AT END OF YEAR 30		
LAYER	(INCHES)	(VOL/VOL)
1	6.7694	0.2821

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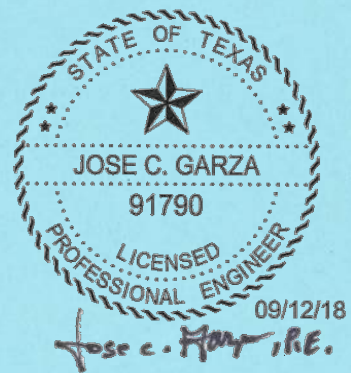
CASE830Y.OUT		
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	567.6481	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
SNOW WATER	0.000	

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HELP MODEL ANALYSIS ALTERNATIVE LINER AND OVERLINER



APPENDIX B.11  
HELP MODEL/MULTIMED MODEL-SUMMARY OF CASES 10L-80L



FOR PERMIT PURPOSES ONLY

Project No. 8514-3 Permit Amendment

Description: HELP Model/MULTIMED Model-Summary of Cases 10L-80L

Date: 3/07/17

By: JCG

**Case10L-Interim Landfill (Location 1)**- An open landfill with 15.5 feet of insitu pre-Subtitle D waste and liner, 30 inches of cover, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 12 feet of waste with 400 foot drain length at 2%, and 6 inches of daily soil cover.

**Case20L-Interim Landfill (Location 2)**- An open landfill with 34 feet of insitu pre-Subtitle waste and liner, 30 inches of cover, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 82.5 feet of waste with 400 foot drain length at 2%, and 6 inches of daily soil cover.

**Case 30L-Interim Landfill (Location 3)**- An open landfill with 37 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 85.5 feet of waste with 400 foot drain length at 2%, and 6 inches of daily soil cover.

**Case40L-Interim Landfill (Location 4)**- An open landfill with 16 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 119.5 feet of waste with 400 foot drain length at 2%, and 6 inches of daily soil cover.

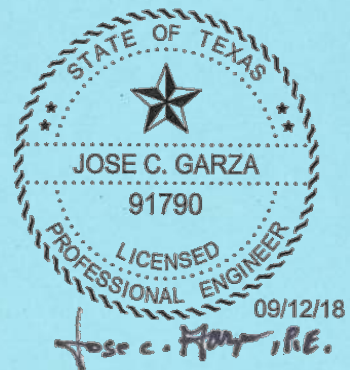
**Case50L-Closed Landfill (Location 1)** - A closed landfill with 15.5 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 12 feet of waste with 400 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case60L-Closed Landfill (Location 2)**- A closed landfill with 34 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 82.5 feet of waste with 400 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case70L-Closed Landfill (Location 3)**- A closed landfill with 37 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 12 inch protective soil layer (Protective Cover), 85.5 feet of waste with 400 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

**Case80L-Closed Landfill (Location 4)**- A closed landfill with 16 feet of insitu pre-Subtitle D waste and liner, a Geosynthetic Clay Liner (GCL), a 60 mil HDPE Flexible Membrane Liner (FML), a Geocomposite drainage layer (Geonet), a 24 inch protective soil layer (Protective Cover), 119.5 feet of waste with 400 foot drain length at 2%, and 12 inches of intermediate cover, a GCL, a 40 mil LLDPE membrane, a Geocomposite drainage layer, and 24 inch erosion cover.

APPENDIX B.12  
HELP MODEL CASE SUMMARY



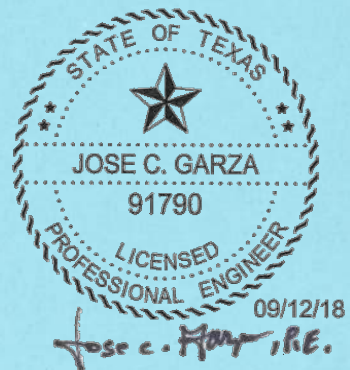


HELP MODEL CASE SUMMARY

Case Alternative Liner/Overliner	Average Precipitation (IN/YR)	Average Runoff (IN/YR)	Average Evapotranspiration (IN/YR)	Average Percolation Through Liner (CF/YR)	Peak Percolation Through Liner (CF/DAY)	*Peak Percolation Through Liner (M/YR)
<b>Interim Landfill HELP Information</b>						
Location 1 (Case 10L) • 12 feet of waste above liner • 15.5 feet of waste below liner						
20 yr	25.74	2.364	21.601	0.004	0.00007	1.79E-07
Location 2 (Case 20L) • 82.5 feet of waste above liner • 34 feet of waste below liner						
20 yr	25.74	2.135	21.716	0.004	0.00006	1.53E-07
Location 3 (Case 30L) • 85.5 feet of waste above liner • 37 feet of waste below liner						
20 yr	25.74	2.043	21.741	0.004	0.00006	1.53E-07
Location 4 (Case 40L) • 119.5 feet of waste above liner • 16 feet of waste below liner						
20 yr	25.74	1.907	21.787	0.004	0.00006	1.53E-07
<b>Closed Landfill HELP Information</b>						
Location 1 (Case 50L) • 12 feet of waste above liner • 15.5 feet of waste below liner						
30 yr	27.20	1.880	21.749	0.001	0.00002	5.11E-08
Location 2 (Case 60L) • 82.5 feet of waste above liner • 34 feet of waste below liner						
30 yr	27.20	1.723	21.785	0.002	0.00002	5.11E-08
Location 3 (Case 70L) • 85.5 feet of waste above liner • 37 feet of waste below liner						
30 yr	27.20	1.657	21.773	0.002	0.00002	5.11E-08
Location 4 (Case 80L) • 119.5 feet of waste above liner • 16 feet of waste below liner						
30 yr	27.20	1.562	21.805	0.002	0.00002	5.11E-08

\* Determined Using Peak Daily Percolation/Leakage Rate Through GCL and Converted to (M/YR)  
 Example: ((.00007 FT<sup>3</sup>/Day-Acre)x(1 Acre/43,560 FT<sup>2</sup>)/(1 Meter/3.28 FT)) x (365 Days/1 YR)= 1.79 x 10<sup>-7</sup> M/YR

APPENDIX B.13  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 10L-  
LOCATION 1



FOR PERMIT PURPOSES ONLY

CASE10L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVE20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE10L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE10L.OUT

TIME: 14:36 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE10L (LOCATION 1)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 144.00 INCHES  
Page 1

CASE10L.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2837 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3242 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0181 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 400.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

CASE10L.OUT  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 7  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 30.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 8  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS = 186.00 INCHES  
 POROSITY = 0.6710 VOL/VOL  
 FIELD CAPACITY = 0.2920 VOL/VOL  
 WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 FAIR STAND OF GRASS, A SURFACE SLOPE OF 25.%  
 AND A SLOPE LENGTH OF 100. FEET.

SCS RUNOFF CURVE NUMBER = 89.50  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 1.886 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 114.065 INCHES  
 TOTAL INITIAL WATER = 114.065 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

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CASE10L.OUT  
 STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
RUNOFF						
TOTALS	0.015 0.377	0.067 0.192	0.006 0.779	0.103 0.173	0.278 0.073	0.282 0.019
STD. DEVIATIONS	0.042	0.081	0.009	0.233	0.504	0.344

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	0.815	0.200	0.918	CASE10L .OUT 0.257	0.214	0.065
EVAPOTRANSPIRATION						
TOTALS	0.927 2.038	2.081 1.886	1.305 3.610	1.245 2.255	1.981 1.096	2.108 1.069
STD. DEVIATIONS	0.558 1.630	0.899 1.312	0.714 1.219	0.924 1.213	1.308 0.780	1.378 0.585
LATERAL DRAINAGE COLLECTED FROM LAYER 4						
TOTALS	0.0557 0.1701	0.0293 0.1696	0.0663 0.1118	0.0567 0.5501	0.0409 0.3280	0.0574 0.1472
STD. DEVIATIONS	0.0736 0.2914	0.0491 0.3491	0.1278 0.2088	0.1001 0.8668	0.0685 0.5012	0.1269 0.2297
PERCOLATION/LEAKAGE THROUGH LAYER 6						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
PERCOLATION/LEAKAGE THROUGH LAYER 8						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

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 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
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DAILY AVERAGE HEAD ON TOP OF LAYER 5						
	0.0006	0.0004	0.0008	0.0007	0.0005	0.0007
AVERAGES	0.0019	0.0019	0.0013	0.0063	0.0039	0.0017
STD. DEVIATIONS	0.0008 0.0033	0.0006 0.0040	0.0015 0.0025	0.0012 0.0099	0.0008 0.0059	0.0015 0.0026

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20

	INCHES		CU. FEET	PERCENT
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.364	( 1.2831)	8580.98	9.183
EVAPOTRANSPIRATION	21.601	( 3.6817)	78409.91	83.907
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.78305	( 1.49648)	6472.482	6.92623

FOR PERMIT PURPOSES ONLY

		CASE10L.OUT		
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000 ( 0.00000)	0.004	0.00000	
AVERAGE HEAD ON TOP OF LAYER 5	0.002 ( 0.001)			
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.00000 ( 0.00000)	0.000	0.00000	
CHANGE IN WATER STORAGE	-0.004 ( 0.5412)	-14.46	-0.015	

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	20
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.156	7827.0879
DRAINAGE COLLECTED FROM LAYER 4	0.19851	720.60400
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00007
AVERAGE HEAD ON TOP OF LAYER 5	0.070	
MAXIMUM HEAD ON TOP OF LAYER 5	0.139	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	4.2 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.000000	0.00000
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3865
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 20		
LAYER	(INCHES)	(VOL/VOL)
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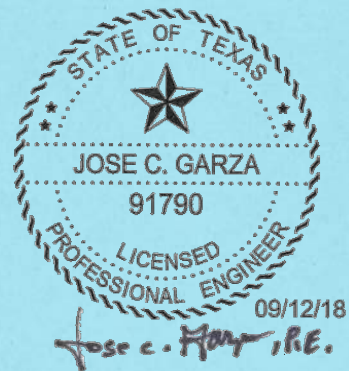


FOR PERMIT PURPOSES ONLY

		CASE10L.OUT
1	1.4228	0.2371
2	40.7579	0.2830
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
7	9.6289	0.3210
8	54.2892	0.2919
SNOW WATER	0.000	

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APPENDIX B.14  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 20L-  
LOCATION 2



CASE20L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE20L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE20L.OUT

TIME: 14:43 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE20L (LOCATION 2)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2391 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 990.00 INCHES  
Page 1

CASE20L.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2909 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3245 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0184 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 400.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

CASE20L.OUT  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

LAYER 7  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 30.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS = 408.00 INCHES  
 POROSITY = 0.6710 VOL/VOL  
 FIELD CAPACITY = 0.2920 VOL/VOL  
 WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 FAIR STAND OF GRASS, A SURFACE SLOPE OF 25.%  
 AND A SLOPE LENGTH OF 356. FEET.

SCS RUNOFF CURVE NUMBER = 88.80  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.124 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 426.166 INCHES  
 TOTAL INITIAL WATER = 426.166 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

FOR PERMIT PURPOSES ONLY

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CASE20L.OUT
STATION LATITUDE      = 27.77 DEGREES
MAXIMUM LEAF AREA INDEX = 2.00
START OF GROWING SEASON (JULIAN DATE) = 0
END OF GROWING SEASON (JULIAN DATE) = 367
EVAPORATIVE ZONE DEPTH = 12.0 INCHES
AVERAGE ANNUAL WIND SPEED = 12.00 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %
    
```

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
RUNOFF						
TOTALS	0.012 0.350	0.055 0.170	0.003 0.716	0.092 0.149	0.254 0.066	0.252 0.016
STD. DEVIATIONS	0.037	0.071	0.006	0.216	0.479	0.315

FOR PERMIT PURPOSES ONLY

	CASE20L.OUT					
	0.770	0.181	0.864	0.234	0.199	0.057
-----						
EVAPOTRANSPIRATION						
-----						
TOTALS	0.932	2.093	1.304	1.251	1.993	2.128
	2.048	1.899	3.628	2.264	1.098	1.076
STD. DEVIATIONS	0.540	0.899	0.714	0.930	1.317	1.382
	1.634	1.319	1.222	1.208	0.786	0.592
-----						
LATERAL DRAINAGE COLLECTED FROM LAYER 4						
-----						
TOTALS	0.0702	0.0321	0.0735	0.0597	0.0436	0.0677
	0.1643	0.1983	0.1143	0.4356	0.4270	0.2210
STD. DEVIATIONS	0.0901	0.0515	0.1376	0.1032	0.0709	0.1448
	0.3053	0.4238	0.2389	0.6078	0.7392	0.3968
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 6						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 8						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 5						
-----						
AVERAGES	0.0008	0.0004	0.0008	0.0007	0.0005	0.0008
	0.0019	0.0023	0.0013	0.0050	0.0050	0.0025
STD. DEVIATIONS	0.0010	0.0006	0.0016	0.0012	0.0008	0.0017
	0.0035	0.0048	0.0028	0.0069	0.0087	0.0045

-----  
 AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20  
 -----

	INCHES		CU. FEET	PERCENT
	-----		-----	-----
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.135	( 1.1936)	7751.57	8.295
EVAPOTRANSPIRATION	21.716	( 3.6903)	78829.24	84.355
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.90747	( 1.55045)	6924.125	7.40953

FOR PERMIT PURPOSES ONLY

	CASE20L.OUT			
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000 ( 0.00000)	0.004	0.00000	
AVERAGE HEAD ON TOP OF LAYER 5	0.002 ( 0.001)			
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.00000 ( 0.00000)	0.000	0.00000	
CHANGE IN WATER STORAGE	-0.015 ( 0.5500)	-56.04	-0.060	

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	20
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.088	7578.4883
DRAINAGE COLLECTED FROM LAYER 4	0.16451	597.18555
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00006
AVERAGE HEAD ON TOP OF LAYER 5	0.058	
MAXIMUM HEAD ON TOP OF LAYER 5	0.116	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	1.8 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.000000	0.00000
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3901
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR	20	
LAYER	(INCHES)	(VOL/VOL)

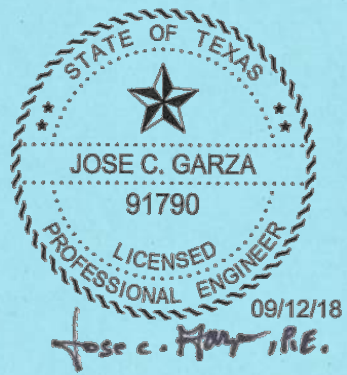


FOR PERMIT PURPOSES ONLY

		CASE20L.OUT
1	1.4393	0.2399
2	287.7899	0.2907
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
7	9.6295	0.3210
8	119.1126	0.2919
SNOW WATER	0.000	

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APPENDIX B.15  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 30L-  
LOCATION 3



FOR PERMIT PURPOSES ONLY

CASE30L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE30L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE30L.OUT

TIME: 14:51 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE30L (LOCATION 3)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 1026.00 INCHES  
Page 1

CASE30L.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2909 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3246 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0184 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 400.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

CASE30L.OUT  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 7  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 30.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 8  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS = 444.00 INCHES  
 POROSITY = 0.6710 VOL/VOL  
 FIELD CAPACITY = 0.2920 VOL/VOL  
 WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 FAIR STAND OF GRASS, A SURFACE SLOPE OF 3.0%  
 AND A SLOPE LENGTH OF 220. FEET.

SCS RUNOFF CURVE NUMBER = 88.50  
 FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 1.920 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 446.987 INCHES  
 TOTAL INITIAL WATER = 446.987 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

FOR PERMIT PURPOSES ONLY

CASE30L.OUT  
 STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.15	2.02	1.05	1.42	2.41	2.71
	2.43	2.37	5.38	2.30	1.33	1.18
STD. DEVIATIONS	0.63	1.18	0.55	1.20	1.88	2.04
	2.55	1.63	3.12	1.75	1.17	0.85
RUNOFF						
TOTALS	0.011	0.050	0.003	0.087	0.244	0.240
	0.339	0.160	0.690	0.141	0.062	0.015
STD. DEVIATIONS	0.035	0.066	0.005	0.209	0.469	0.303

FOR PERMIT PURPOSES ONLY

				CASE30L.OUT		
	0.752	0.173	0.842	0.224	0.191	0.052
-----						
EVAPOTRANSPIRATION						
-----						
TOTALS	0.923	2.100	1.303	1.256	1.998	2.129
	2.050	1.905	3.640	2.259	1.105	1.073
STD. DEVIATIONS	0.556	0.908	0.712	0.934	1.314	1.388
	1.630	1.324	1.226	1.208	0.790	0.591
-----						
LATERAL DRAINAGE COLLECTED FROM LAYER 4						
-----						
TOTALS	0.0699	0.0385	0.0689	0.0590	0.0458	0.0682
	0.1735	0.2086	0.1176	0.4423	0.4385	0.2333
STD. DEVIATIONS	0.0925	0.0574	0.1339	0.1045	0.0746	0.1486
	0.3121	0.4439	0.2479	0.6142	0.7449	0.4210
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 6						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 8						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

-----						
DAILY AVERAGE HEAD ON TOP OF LAYER 5						
-----						
AVERAGES	0.0008	0.0005	0.0008	0.0007	0.0005	0.0008
	0.0020	0.0024	0.0014	0.0050	0.0052	0.0027
STD. DEVIATIONS	0.0011	0.0007	0.0015	0.0012	0.0008	0.0017
	0.0036	0.0051	0.0029	0.0070	0.0088	0.0048

-----  
 AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20  
 -----

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	2.043	( 1.1566)	7417.81	7.938
EVAPOTRANSPIRATION	21.741	( 3.6990)	78919.84	84.452
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.96422	( 1.58077)	7130.124	7.62997

FOR PERMIT PURPOSES ONLY

		CASE30L.0UT	
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000 ( 0.00000)	0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.002 ( 0.002)		
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.00000 ( 0.00000)	0.000	0.00000
CHANGE IN WATER STORAGE	-0.005 ( 0.5491)	-18.84	-0.020

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PEAK DAILY VALUES FOR YEARS	1 THROUGH 20	
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.060	7476.7285
DRAINAGE COLLECTED FROM LAYER 4	0.16176	587.17737
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00006
AVERAGE HEAD ON TOP OF LAYER 5	0.057	
MAXIMUM HEAD ON TOP OF LAYER 5	0.113	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	2.4 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.000000	0.00000
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3913
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 20		
LAYER	(INCHES)	(VOL/VOL)
-----	-----	-----

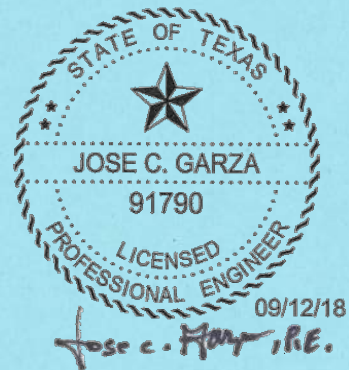


FOR PERMIT PURPOSES ONLY

		CASE30L.OUT
1	1.4410	0.2402
2	298.3019	0.2907
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
7	9.6295	0.3210
8	129.6245	0.2919
SNOW WATER	0.000	

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APPENDIX B.16  
HELP OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 40L-  
LOCATION 4



FOR PERMIT PURPOSES ONLY

CASE40L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR20Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE20Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO20Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV20Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE40L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE40L.OUT

TIME: 14:29 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE40L (LOCATION 4)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 6.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 1434.00 INCHES

CASE40L.OUT  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2912 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 3  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3246 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 4  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0185 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 400.0 FEET

LAYER 5  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 6  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL

CASE40L.OUT  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 30.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18

THICKNESS = 192.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
FAIR STAND OF GRASS, A SURFACE SLOPE OF 3.0%  
AND A SLOPE LENGTH OF 500. FEET.

SCS RUNOFF CURVE NUMBER = 88.00  
FRACTION OF AREA ALLOWING RUNOFF = 80.0 PERCENT  
AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
INITIAL WATER IN EVAPORATIVE ZONE = 1.920 INCHES  
UPPER LIMIT OF EVAPORATIVE STORAGE = 6.606 INCHES  
LOWER LIMIT OF EVAPORATIVE STORAGE = 1.788 INCHES  
INITIAL SNOW WATER = 0.000 INCHES  
INITIAL WATER IN LAYER MATERIALS = 492.539 INCHES  
TOTAL INITIAL WATER = 492.539 INCHES  
TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
CORPUS CHRISTI TEXAS

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CASE40L.OUT  
 STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 2.00  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 20

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.15 2.43	2.02 2.37	1.05 5.38	1.42 2.30	2.41 1.33	2.71 1.18
STD. DEVIATIONS	0.63 2.55	1.18 1.63	0.55 3.12	1.20 1.75	1.88 1.17	2.04 0.85
RUNOFF						
TOTALS	0.010 0.322	0.044 0.145	0.002 0.650	0.080 0.131	0.229 0.058	0.222 0.013
STD. DEVIATIONS	0.032	0.059	0.004	0.198	0.452	0.284

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	CASE40L.OUT					
	0.721	0.160	0.809	0.208	0.182	0.047
-----						
EVAPOTRANSPIRATION						
-----						
TOTALS	0.926	2.091	1.307	1.259	2.002	2.140
	2.063	1.908	3.649	2.262	1.101	1.080
STD. DEVIATIONS	0.553	0.908	0.722	0.938	1.315	1.392
	1.651	1.324	1.215	1.209	0.795	0.582
-----						
LATERAL DRAINAGE COLLECTED FROM LAYER 4						
-----						
TOTALS	0.0720	0.0389	0.0796	0.0588	0.0484	0.0755
	0.1785	0.2158	0.1255	0.4555	0.4591	0.2478
STD. DEVIATIONS	0.0945	0.0552	0.1549	0.1061	0.0808	0.1552
	0.3193	0.4566	0.2773	0.6167	0.7573	0.4462
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 6						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
-----						
PERCOLATION/LEAKAGE THROUGH LAYER 8						
-----						
TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 5						
-----						
AVERAGES	0.0008	0.0005	0.0009	0.0007	0.0006	0.0009
	0.0020	0.0025	0.0015	0.0052	0.0054	0.0028
STD. DEVIATIONS	0.0011	0.0007	0.0018	0.0012	0.0009	0.0018
	0.0036	0.0052	0.0033	0.0070	0.0089	0.0051

-----  
 AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 20  
 -----

	INCHES		CU. FEET	PERCENT
	-----		-----	-----
PRECIPITATION	25.74	( 5.706)	93448.9	100.00
RUNOFF	1.907	( 1.1083)	6921.00	7.406
EVAPOTRANSPIRATION	21.787	( 3.6980)	79085.98	84.630
LATERAL DRAINAGE COLLECTED FROM LAYER 4	2.05532	( 1.61590)	7460.818	7.98385

FOR PERMIT PURPOSES ONLY

			CASE40L.OUT	
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.00000 ( 0.00000)		0.004	0.00000
AVERAGE HEAD ON TOP OF LAYER 5	0.002 ( 0.002)			
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.00000 ( 0.00000)		0.000	0.00000
CHANGE IN WATER STORAGE	-0.005 ( 0.5751)		-18.88	-0.020

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PEAK DAILY VALUES FOR YEARS	1 THROUGH	20
	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.016	7318.0361
DRAINAGE COLLECTED FROM LAYER 4	0.16526	599.88171
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00006
AVERAGE HEAD ON TOP OF LAYER 5	0.058	
MAXIMUM HEAD ON TOP OF LAYER 5	0.115	
LOCATION OF MAXIMUM HEAD IN LAYER 4 (DISTANCE FROM DRAIN)	4.6 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 8	0.000000	0.00000
SNOW WATER	0.00	0.0000
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3947
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1490

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 20		
	(INCHES)	(VOL/VOL)
LAYER		

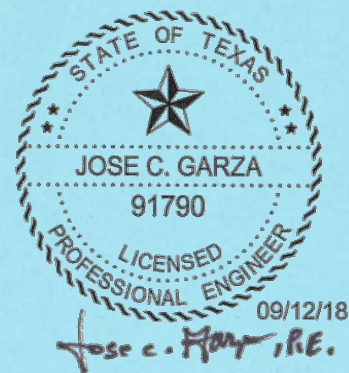


FOR PERMIT PURPOSES ONLY

		CASE40L.OUT
1	1.4410	0.2402
2	417.4379	0.2911
3	7.7040	0.3210
4	0.0020	0.0100
5	0.0000	0.0000
6	0.1800	0.7500
7	9.6289	0.3210
8	56.0412	0.2919
SNOW WATER	0.000	

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APPENDIX B.17  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 50L-  
LOCATION 1



CASE50L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE50L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE50L.OUT

TIME: 16: 7 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE50L (LOCATION 1)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2719 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES  
Page 1

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CASE50L.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18

THICKNESS = 144.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL

CASE5OL.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

CASE50L.OUT  
EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

LAYER 11  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 30.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 12  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 186.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
GOOD STAND OF GRASS, A SURFACE SLOPE OF 25.0%  
AND A SLOPE LENGTH OF 100. FEET.

SCS RUNOFF CURVE NUMBER = 85.60  
FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
INITIAL WATER IN EVAPORATIVE ZONE = 2.674 INCHES  
UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
INITIAL SNOW WATER = 0.000 INCHES  
INITIAL WATER IN LAYER MATERIALS = 124.412 INCHES  
TOTAL INITIAL WATER = 124.412 INCHES  
TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
MAXIMUM LEAF AREA INDEX = 3.50

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CASE50L.OUT

START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
<b>RUNOFF</b>						
TOTALS	0.007 0.342	0.022 0.218	0.005 0.608	0.051 0.191	0.188 0.067	0.174 0.007
STD. DEVIATIONS	0.022 0.789	0.041 0.366	0.026 0.822	0.171 0.318	0.500 0.265	0.243 0.028

FOR PERMIT PURPOSES ONLY

CASE50L.OUT

EVAPOTRANSPIRATION

TOTALS	1.093 1.754	1.768 2.186	1.331 3.474	1.252 2.435	1.966 1.312	2.071 1.107
STD. DEVIATIONS	0.665 1.256	0.864 1.504	0.621 1.237	0.803 1.136	1.191 0.899	1.228 0.681

LATERAL DRAINAGE COLLECTED FROM LAYER 2

TOTALS	0.0698 0.3318	0.2237 0.3490	0.1155 0.8839	0.0457 0.7081	0.1805 0.2403	0.3327 0.0780
STD. DEVIATIONS	0.1315 0.5455	0.2604 0.5857	0.1270 0.9977	0.1234 0.7204	0.2785 0.3203	0.4691 0.1153

PERCOLATION/LEAKAGE THROUGH LAYER 4

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 10

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 12

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 3

AVERAGES	0.0005 0.0206	0.0017 0.0177	0.0008 0.1061	0.0003 0.0240	0.0013 0.0018	0.0139 0.0006
STD. DEVIATIONS	0.0009 0.1028	0.0020 0.0537	0.0009 0.2641	0.0009 0.0529	0.0020 0.0024	0.0415 0.0008

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
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	CASE50L.OUT					
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

\*\*\*\*\*

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES	CU. FEET	PERCENT
PRECIPITATION	27.20 ( 5.704)	98722.7	100.00
RUNOFF	1.880 ( 1.2157)	6825.49	6.914
EVAPOTRANSPIRATION	21.749 ( 3.7373)	78947.65	79.969
LATERAL DRAINAGE COLLECTED FROM LAYER 2	3.55912 ( 1.91851)	12919.604	13.08676
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00001 ( 0.00001)	0.023	0.00002
AVERAGE HEAD ON TOP OF LAYER 3	0.016 ( 0.026)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00001 ( 0.00001)	0.022	0.00002
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000 ( 0.00000)	0.001	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000 ( 0.000)		
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.00000 ( 0.00000)	0.000	0.00000
CHANGE IN WATER STORAGE	0.008 ( 0.4489)	29.91	0.030

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 30

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.1035
DRAINAGE COLLECTED FROM LAYER 2	0.91251	3312.41650
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000012	0.04380
AVERAGE HEAD ON TOP OF LAYER 3	14.568	
MAXIMUM HEAD ON TOP OF LAYER 3	18.997	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	87.9 FEET	

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CASE50L.OUT		
DRAINAGE COLLECTED FROM LAYER 8	0.00001	0.03665
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.000	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.000000	0.00000
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.4285	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.2210	

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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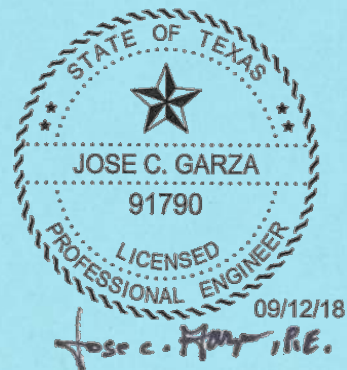
FINAL WATER STORAGE AT END OF YEAR 30

LAYER	(INCHES)	(VOL/VOL)
1	6.7730	0.2822
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	42.0480	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
11	9.6289	0.3210
12	54.2892	0.2919
SNOW WATER	0.000	

CASE50L.OUT

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APPENDIX B.18  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 60L-  
LOCATION 2



CASE60L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE60L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE60L.OUT

TIME: 16:16 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE60L (LOCATION 2)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2722 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES

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CASE60L.OUT

POROSITY	=	0.8500	VOL/VOL
FIELD CAPACITY	=	0.0100	VOL/VOL
WILTING POINT	=	0.0050	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0100	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	10.0000000000	CM/SEC
SLOPE	=	2.00	PERCENT
DRAINAGE LENGTH	=	250.0	FEET

LAYER 3  
 -----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
 MATERIAL TEXTURE NUMBER 36

THICKNESS	=	0.04	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.399999993000E-12	CM/SEC
FML PINHOLE DENSITY	=	1.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	2.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	3	- GOOD

LAYER 4  
 -----

TYPE 3 - BARRIER SOIL LINER  
 MATERIAL TEXTURE NUMBER 17

THICKNESS	=	0.24	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.300000003000E-08	CM/SEC

LAYER 5  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS	=	12.00	INCHES
POROSITY	=	0.4300	VOL/VOL
FIELD CAPACITY	=	0.3210	VOL/VOL
WILTING POINT	=	0.2210	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.3210	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.330000003000E-04	CM/SEC

LAYER 6  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS	=	990.00	INCHES
POROSITY	=	0.6710	VOL/VOL
FIELD CAPACITY	=	0.2920	VOL/VOL

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CASE60L.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

CASE60L.OUT  
EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

LAYER 11  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 30.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 12  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 408.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
GOOD STAND OF GRASS, A SURFACE SLOPE OF 25.0%  
AND A SLOPE LENGTH OF 356. FEET.

SCS RUNOFF CURVE NUMBER = 84.60  
FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
INITIAL WATER IN EVAPORATIVE ZONE = 2.681 INCHES  
UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
INITIAL SNOW WATER = 0.000 INCHES  
INITIAL WATER IN LAYER MATERIALS = 436.275 INCHES  
TOTAL INITIAL WATER = 436.275 INCHES  
TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
MAXIMUM LEAF AREA INDEX = 3.50



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CASE60L.OUT  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.37 2.36	1.81 2.86	1.19 5.39	1.40 2.99	2.51 1.49	2.59 1.25
STD. DEVIATIONS	0.81 2.23	1.21 2.36	0.57 2.96	1.05 1.90	1.80 1.16	1.82 0.84
RUNOFF						
TOTALS	0.005 0.327	0.016 0.193	0.004 0.573	0.047 0.168	0.171 0.066	0.149 0.005
STD. DEVIATIONS	0.018 0.772	0.033 0.343	0.020 0.823	0.170 0.315	0.498 0.283	0.215 0.021

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CASE60L.OUT

EVAPOTRANSPIRATION

TOTALS	1.096	1.761	1.331	1.252	1.971	2.085
	1.756	2.192	3.492	2.429	1.316	1.104
STD. DEVIATIONS	0.662	0.861	0.620	0.803	1.183	1.235
	1.251	1.505	1.239	1.134	0.905	0.683

LATERAL DRAINAGE COLLECTED FROM LAYER 2

TOTALS	0.0775	0.2338	0.1173	0.0485	0.1907	0.3438
	0.3452	0.3639	0.9017	0.7403	0.2420	0.0762
STD. DEVIATIONS	0.1419	0.2767	0.1258	0.1298	0.2881	0.4853
	0.5558	0.6168	1.0007	0.7614	0.3121	0.1053

PERCOLATION/LEAKAGE THROUGH LAYER 4

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 10

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 12

TOTALS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 3

AVERAGES	0.0006	0.0018	0.0008	0.0004	0.0014	0.0163
	0.0205	0.0202	0.1047	0.0279	0.0018	0.0005
STD. DEVIATIONS	0.0010	0.0022	0.0009	0.0010	0.0021	0.0561
	0.1017	0.0598	0.2561	0.0609	0.0023	0.0007

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

FOR PERMIT PURPOSES ONLY

CASE60L.OUT

STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES		CU. FEET		PERCENT
PRECIPITATION	27.20	( 5.704)	98722.7		100.00
RUNOFF	1.723	( 1.2076)	6253.77		6.335
EVAPOTRANSPIRATION	21.785	( 3.7320)	79078.27		80.101
LATERAL DRAINAGE COLLECTED FROM LAYER 2	3.68090	( 1.95906)	13361.677		13.53456
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00001	( 0.00001)	0.024		0.00002
AVERAGE HEAD ON TOP OF LAYER 3	0.016	( 0.026)			
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00001	( 0.00001)	0.023		0.00002
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000	( 0.00000)	0.002		0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000	( 0.000)			
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.00000	( 0.00000)	0.000		0.00000
CHANGE IN WATER STORAGE	0.008	( 0.4598)	28.94		0.029

\*\*\*\*\*

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 30

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.1035
DRAINAGE COLLECTED FROM LAYER 2	0.91340	3315.63574
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000012	0.04489
AVERAGE HEAD ON TOP OF LAYER 3	14.828	
MAXIMUM HEAD ON TOP OF LAYER 3	19.279	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	88.6 FEET	

FOR PERMIT PURPOSES ONLY

CASE60L.OUT

DRAINAGE COLLECTED FROM LAYER 8	0.00001	0.03755
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.006	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.000000	0.00000
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.4270	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.2210	

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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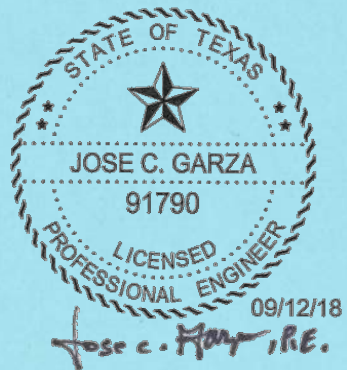
FINAL WATER STORAGE AT END OF YEAR 30

LAYER	(INCHES)	(VOL/VOL)
1	6.7725	0.2822
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	289.0800	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
11	9.6295	0.3210
12	119.1125	0.2919
SNOW WATER	0.000	

CASE60L.OUT

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APPENDIX B.19  
HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 70L-  
LOCATION 3



FOR PERMIT PURPOSES ONLY

CASE70L.OUT

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PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE70L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE70L.OUT

TIME: 16:25 DATE: 3/ 6/2017

\*\*\*\*\*  
TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE70L (LOCATION 3)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2758 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20  
THICKNESS = 0.20 INCHES  
Page 1

FOR PERMIT PURPOSES ONLY

CASE70L.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18

THICKNESS = 1026.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL



CASE70L.OUT  
 WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
 -----

TYPE 2 - LATERAL DRAINAGE LAYER  
 MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
 POROSITY = 0.8500 VOL/VOL  
 FIELD CAPACITY = 0.0100 VOL/VOL  
 WILTING POINT = 0.0050 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
 SLOPE = 2.00 PERCENT  
 DRAINAGE LENGTH = 250.0 FEET

LAYER 9  
 -----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
 MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
 POROSITY = 0.0000 VOL/VOL  
 FIELD CAPACITY = 0.0000 VOL/VOL  
 WILTING POINT = 0.0000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.199999996000E-12 CM/SEC  
 FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
 FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
 FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
 -----

TYPE 3 - BARRIER SOIL LINER  
 MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
 POROSITY = 0.7500 VOL/VOL  
 FIELD CAPACITY = 0.7470 VOL/VOL  
 WILTING POINT = 0.4000 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

CASE70L.OUT  
 EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 11  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 13

THICKNESS = 30.00 INCHES  
 POROSITY = 0.4300 VOL/VOL  
 FIELD CAPACITY = 0.3210 VOL/VOL  
 WILTING POINT = 0.2210 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 12  
 -----

TYPE 1 - VERTICAL PERCOLATION LAYER  
 MATERIAL TEXTURE NUMBER 18

THICKNESS = 444.00 INCHES  
 POROSITY = 0.6710 VOL/VOL  
 FIELD CAPACITY = 0.2920 VOL/VOL  
 WILTING POINT = 0.0770 VOL/VOL  
 INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
 EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
 -----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
 SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3.0%  
 AND A SLOPE LENGTH OF 220. FEET.

SCS RUNOFF CURVE NUMBER = 84.10  
 FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
 AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 INITIAL WATER IN EVAPORATIVE ZONE = 2.768 INCHES  
 UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
 LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
 INITIAL SNOW WATER = 0.000 INCHES  
 INITIAL WATER IN LAYER MATERIALS = 457.386 INCHES  
 TOTAL INITIAL WATER = 457.386 INCHES  
 TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
 -----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
 CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
 MAXIMUM LEAF AREA INDEX = 3.50

FOR PERMIT PURPOSES ONLY

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CASE70L.OUT
START OF GROWING SEASON (JULIAN DATE) = 0
END OF GROWING SEASON (JULIAN DATE) = 367
EVAPORATIVE ZONE DEPTH = 12.0 INCHES
AVERAGE ANNUAL WIND SPEED = 12.00 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %
    
```

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	1.37	1.81	1.19	1.40	2.51	2.59
	2.36	2.86	5.39	2.99	1.49	1.25
STD. DEVIATIONS	0.81	1.21	0.57	1.05	1.80	1.82
	2.23	2.36	2.96	1.90	1.16	0.84
RUNOFF						
TOTALS	0.004	0.013	0.003	0.044	0.164	0.137
	0.325	0.178	0.562	0.159	0.064	0.004
STD. DEVIATIONS	0.016	0.029	0.018	0.166	0.498	0.200
	0.770	0.331	0.824	0.315	0.281	0.018

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CASE70L.OUT

EVAPOTRANSPIRATION

TOTALS	1.095 1.754	1.769 2.181	1.332 3.481	1.252 2.435	1.978 1.313	2.082 1.102
STD. DEVIATIONS	0.663 1.244	0.860 1.501	0.624 1.235	0.803 1.138	1.187 0.902	1.231 0.681

LATERAL DRAINAGE COLLECTED FROM LAYER 2

TOTALS	0.0767 0.3548	0.2331 0.3828	0.1179 0.9254	0.0493 0.7490	0.1925 0.2449	0.3537 0.0806
STD. DEVIATIONS	0.1439 0.5774	0.2713 0.6301	0.1269 1.0117	0.1333 0.7734	0.2928 0.3251	0.4967 0.1272

PERCOLATION/LEAKAGE THROUGH LAYER 4

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 10

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 12

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

-----  
 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)  
 -----

DAILY AVERAGE HEAD ON TOP OF LAYER 3

AVERAGES	0.0005 0.0223	0.0018 0.0241	0.0008 0.1085	0.0004 0.0318	0.0014 0.0018	0.0186 0.0006
STD. DEVIATIONS	0.0010 0.1021	0.0021 0.0699	0.0009 0.2572	0.0010 0.0681	0.0021 0.0024	0.0627 0.0009

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
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FOR PERMIT PURPOSES ONLY

	CASE70L.OUT					
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES	CU. FEET	PERCENT
PRECIPITATION	27.20 ( 5.704)	98722.7	100.00
RUNOFF	1.657 ( 1.2106)	6015.83	6.094
EVAPOTRANSPIRATION	21.773 ( 3.7354)	79036.62	80.059
LATERAL DRAINAGE COLLECTED FROM LAYER 2	3.76085 ( 1.98336)	13651.874	13.82851
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00001 ( 0.00001)	0.025	0.00003
AVERAGE HEAD ON TOP OF LAYER 3	0.018 ( 0.026)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00001 ( 0.00001)	0.024	0.00002
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000 ( 0.00000)	0.002	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000 ( 0.000)		
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.00000 ( 0.00000)	0.000	0.00000
CHANGE IN WATER STORAGE	0.005 ( 0.4439)	18.34	0.019

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 30

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.1035
DRAINAGE COLLECTED FROM LAYER 2	0.91351	3316.05835
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000012	0.04505
AVERAGE HEAD ON TOP OF LAYER 3	14.866	
MAXIMUM HEAD ON TOP OF LAYER 3	19.319	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	88.7 FEET	

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CASE70L.OUT

DRAINAGE COLLECTED FROM LAYER 8	0.00001	0.03769
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.006	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.000000	0.00000
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.4264	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.2210	

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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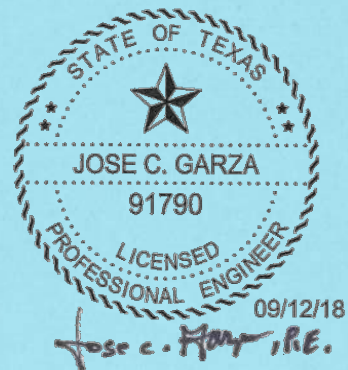
FINAL WATER STORAGE AT END OF YEAR 30

LAYER	(INCHES)	(VOL/VOL)
1	6.7715	0.2821
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	299.5920	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
11	9.6295	0.3210
12	129.6245	0.2919
SNOW WATER	0.000	

CASE70L.OUT

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**APPENDIX B.20**  
**HELP OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 80L-**  
**LOCATION 4**





FOR PERMIT PURPOSES ONLY

CASE80L.OUT

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\*\* HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE \*\*  
\*\* HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) \*\*  
\*\* DEVELOPED BY ENVIRONMENTAL LABORATORY \*\*  
\*\* USAE WATERWAYS EXPERIMENT STATION \*\*  
\*\* FOR USEPA RISK REDUCTION ENGINEERING LABORATORY \*\*  
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\*\*\*\*\*  
\*\*\*\*\*

PRECIPITATION DATA FILE: C:\HELP3\MDATA\KGVPR30Y.D4  
TEMPERATURE DATA FILE: C:\HELP3\MDATA\KGVTE30Y.D7  
SOLAR RADIATION DATA FILE: C:\HELP3\MDATA\KGVSO30Y.D13  
EVAPOTRANSPIRATION DATA: C:\HELP3\MDATA\KGVVEV30Y.D11  
SOIL AND DESIGN DATA FILE: C:\HELP3\MDATA\CASE80L.D10  
OUTPUT DATA FILE: C:\HELP3\MDATA\CASE80L.OUT

TIME: 16:36 DATE: 3/ 6/2017

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TITLE: CITY OF KINGSVILLE SOLID WASTE LANDFILL-CASE80L (LOCATION 4)  
\*\*\*\*\*

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE  
COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2757 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC  
NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 4.63  
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
Page 1

CASE80L.OUT  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 3  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 36

THICKNESS = 0.04 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.399999993000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 4  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.300000003000E-08 CM/SEC

LAYER 5  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 12.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.330000003000E-04 CM/SEC

LAYER 6  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18

THICKNESS = 1434.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL

CASE80L.OUT  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2920 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

LAYER 7  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13

THICKNESS = 24.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 8  
-----

TYPE 2 - LATERAL DRAINAGE LAYER  
MATERIAL TEXTURE NUMBER 20

THICKNESS = 0.20 INCHES  
POROSITY = 0.8500 VOL/VOL  
FIELD CAPACITY = 0.0100 VOL/VOL  
WILTING POINT = 0.0050 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0100 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 10.0000000000 CM/SEC  
SLOPE = 2.00 PERCENT  
DRAINAGE LENGTH = 250.0 FEET

LAYER 9  
-----

TYPE 4 - FLEXIBLE MEMBRANE LINER  
MATERIAL TEXTURE NUMBER 35

THICKNESS = 0.06 INCHES  
POROSITY = 0.0000 VOL/VOL  
FIELD CAPACITY = 0.0000 VOL/VOL  
WILTING POINT = 0.0000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.0000 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.19999996000E-12 CM/SEC  
FML PINHOLE DENSITY = 1.00 HOLES/ACRE  
FML INSTALLATION DEFECTS = 2.00 HOLES/ACRE  
FML PLACEMENT QUALITY = 3 - GOOD

LAYER 10  
-----

TYPE 3 - BARRIER SOIL LINER  
MATERIAL TEXTURE NUMBER 17

THICKNESS = 0.24 INCHES  
POROSITY = 0.7500 VOL/VOL  
FIELD CAPACITY = 0.7470 VOL/VOL  
WILTING POINT = 0.4000 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.7500 VOL/VOL

CASE80L.OUT  
EFFECTIVE SAT. HYD. COND. = 0.30000003000E-08 CM/SEC

LAYER 11  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 13  
THICKNESS = 30.00 INCHES  
POROSITY = 0.4300 VOL/VOL  
FIELD CAPACITY = 0.3210 VOL/VOL  
WILTING POINT = 0.2210 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.3210 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.33000003000E-04 CM/SEC

LAYER 12  
-----

TYPE 1 - VERTICAL PERCOLATION LAYER  
MATERIAL TEXTURE NUMBER 18  
THICKNESS = 192.00 INCHES  
POROSITY = 0.6710 VOL/VOL  
FIELD CAPACITY = 0.2920 VOL/VOL  
WILTING POINT = 0.0770 VOL/VOL  
INITIAL SOIL WATER CONTENT = 0.2919 VOL/VOL  
EFFECTIVE SAT. HYD. COND. = 0.10000005000E-02 CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA  
-----

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT  
SOIL DATA BASE USING SOIL TEXTURE #13 WITH A  
GOOD STAND OF GRASS, A SURFACE SLOPE OF 3.0%  
AND A SLOPE LENGTH OF 500. FEET.

SCS RUNOFF CURVE NUMBER = 83.40  
FRACTION OF AREA ALLOWING RUNOFF = 100.0 PERCENT  
AREA PROJECTED ON HORIZONTAL PLANE = 1.000 ACRES  
EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
INITIAL WATER IN EVAPORATIVE ZONE = 2.765 INCHES  
UPPER LIMIT OF EVAPORATIVE STORAGE = 5.160 INCHES  
LOWER LIMIT OF EVAPORATIVE STORAGE = 2.652 INCHES  
INITIAL SNOW WATER = 0.000 INCHES  
INITIAL WATER IN LAYER MATERIALS = 502.935 INCHES  
TOTAL INITIAL WATER = 502.935 INCHES  
TOTAL SUBSURFACE INFLOW = 0.00 INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA  
-----

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM  
CORPUS CHRISTI TEXAS

STATION LATITUDE = 27.77 DEGREES  
MAXIMUM LEAF AREA INDEX = 3.50

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CASE80L.OUT  
 START OF GROWING SEASON (JULIAN DATE) = 0  
 END OF GROWING SEASON (JULIAN DATE) = 367  
 EVAPORATIVE ZONE DEPTH = 12.0 INCHES  
 AVERAGE ANNUAL WIND SPEED = 12.00 MPH  
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 78.00 %  
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 76.00 %  
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 76.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
1.63	1.69	1.20	1.57	3.29	3.12
2.26	2.78	5.31	2.92	1.61	1.17

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
56.30	59.30	65.90	73.00	78.10	82.70
84.90	85.00	81.50	74.00	65.00	59.10

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING  
 COEFFICIENTS FOR CORPUS CHRISTI TEXAS  
 AND STATION LATITUDE = 27.77 DEGREES

\*\*\*\*\*

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 30

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
<b>PRECIPITATION</b>						
TOTALS	1.37	1.81	1.19	1.40	2.51	2.59
	2.36	2.86	5.39	2.99	1.49	1.25
STD. DEVIATIONS	0.81	1.21	0.57	1.05	1.80	1.82
	2.23	2.36	2.96	1.90	1.16	0.84
<b>RUNOFF</b>						
TOTALS	0.003	0.010	0.003	0.042	0.156	0.122
	0.316	0.163	0.535	0.147	0.061	0.003
STD. DEVIATIONS	0.013	0.024	0.015	0.164	0.497	0.184
	0.758	0.318	0.809	0.320	0.279	0.014

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CASE80L.OUT

EVAPOTRANSPIRATION

TOTALS	1.098 1.756	1.771 2.189	1.335 3.487	1.250 2.438	1.982 1.317	2.083 1.099
STD. DEVIATIONS	0.661 1.255	0.863 1.518	0.626 1.230	0.802 1.138	1.189 0.905	1.239 0.685

LATERAL DRAINAGE COLLECTED FROM LAYER 2

TOTALS	0.0759 0.3641	0.2321 0.3858	0.1168 0.9507	0.0532 0.7510	0.1955 0.2525	0.3680 0.0787
STD. DEVIATIONS	0.1410 0.5970	0.2677 0.6265	0.1258 1.0470	0.1423 0.7857	0.2933 0.3241	0.5138 0.1151

PERCOLATION/LEAKAGE THROUGH LAYER 4

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 10

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

PERCOLATION/LEAKAGE THROUGH LAYER 12

TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 3

AVERAGES	0.0005 0.0273	0.0018 0.0201	0.0008 0.1213	0.0004 0.0321	0.0014 0.0019	0.0187 0.0006
STD. DEVIATIONS	0.0010 0.1291	0.0021 0.0571	0.0009 0.2670	0.0010 0.0798	0.0021 0.0024	0.0583 0.0008

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
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STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 30

	INCHES	CU. FEET	PERCENT
PRECIPITATION	27.20 ( 5.704)	98722.7	100.00
RUNOFF	1.562 ( 1.2013)	5669.92	5.743
EVAPOTRANSPIRATION	21.805 ( 3.7516)	79151.28	80.175
LATERAL DRAINAGE COLLECTED FROM LAYER 2	3.82437 ( 2.05115)	13882.466	14.06208
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.00001 ( 0.00001)	0.027	0.00003
AVERAGE HEAD ON TOP OF LAYER 3	0.019 ( 0.029)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.00001 ( 0.00001)	0.025	0.00003
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.00000 ( 0.00000)	0.002	0.00000
AVERAGE HEAD ON TOP OF LAYER 9	0.000 ( 0.000)		
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.00000 ( 0.00000)	0.000	0.00000
CHANGE IN WATER STORAGE	0.005 ( 0.4494)	19.00	0.019

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PEAK DAILY VALUES FOR YEARS 1 THROUGH 30

	(INCHES)	(CU. FT.)
PRECIPITATION	5.07	18404.102
RUNOFF	2.585	9382.1035
DRAINAGE COLLECTED FROM LAYER 2	0.91331	3315.29883
PERCOLATION/LEAKAGE THROUGH LAYER 4	0.000012	0.04488
AVERAGE HEAD ON TOP OF LAYER 3	14.828	
MAXIMUM HEAD ON TOP OF LAYER 3	19.277	
LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN)	88.6 FEET	

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CASE80L.OUT		
DRAINAGE COLLECTED FROM LAYER 8	0.00001	0.03850
PERCOLATION/LEAKAGE THROUGH LAYER 10	0.000000	0.00002
AVERAGE HEAD ON TOP OF LAYER 9	0.000	
MAXIMUM HEAD ON TOP OF LAYER 9	0.006	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
PERCOLATION/LEAKAGE THROUGH LAYER 12	0.000000	0.00000
SNOW WATER	0.02	73.7433
MAXIMUM VEG. SOIL WATER (VOL/VOL)	0.4265	
MINIMUM VEG. SOIL WATER (VOL/VOL)	0.2210	

\*\*\* Maximum heads are computed using McEnroe's equations. \*\*\*

Reference: Maximum Saturated Depth over Landfill Liner  
 by Bruce M. McEnroe, University of Kansas  
 ASCE Journal of Environmental Engineering  
 Vol. 119, No. 2, March 1993, pp. 262-270.

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FINAL WATER STORAGE AT END OF YEAR 30

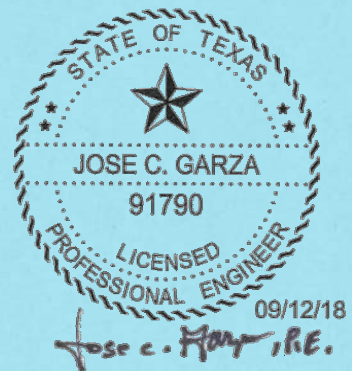
LAYER	(INCHES)	(VOL/VOL)
1	6.7738	0.2822
2	0.0020	0.0100
3	0.0000	0.0000
4	0.1800	0.7500
5	3.8520	0.3210
6	418.7280	0.2920
7	7.7040	0.3210
8	0.0020	0.0100
9	0.0000	0.0000
10	0.1800	0.7500
11	9.6289	0.3210
12	56.0412	0.2919
SNOW WATER	0.000	



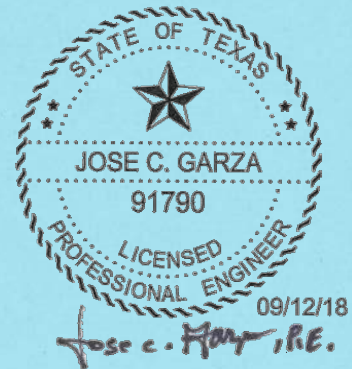
CASE80L.OUT

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APPENDIX C  
MULTIMED MODEL ANALYSIS



APPENDIX C.1  
CONTENTS



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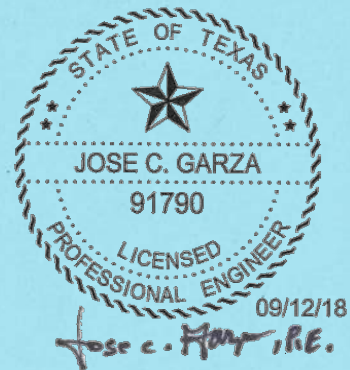
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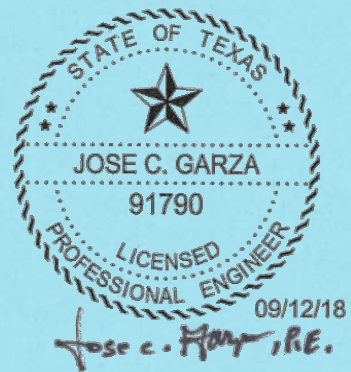
APPENDIX C.2  
MULTIMED CHEMICAL-SPECIFIC DATA



**MULTIMED CHEMICAL - SPECIFIC DATA**

Variable Name	Units	Value	Comments
Solid phase decay coefficient	1/yr	0	decay not used
Dissolved phase decay coefficient	1/yr	0	decay not used
Chemical decay coefficient	1/yr	0	decay not used
Acid catalyst hydrolysis constant	1/m-yr	0	hydrolysis not used
Neutral hydrolysis rate constant	1/yr	0	hydrolysis not used
Base catalyst hydrolysis constant	1/m-yr	0	hydrolysis not used
Reference temperature	degrees C	20	not used in model since decay not used
Normalized distribution coefficient	ml/g	0	0 because simulation is steady state, with no chemical decay
Distribution coefficient	ml/g		derived by MULTIMED from normalized distribution coefficient
Biodegradation coefficient	1/yr	0	biodegradation not allowed by TCEQ

APPENDIX C.3  
MULTIMED SOURCE-SPECIFIC DATA



**MULTIMED SOURCE - SPECIFIC DATA**

Variable Name	Units	Value	Comments
Infiltration rate	m/yr	varies	See table below.
Area of waste disposal unit	m <sup>2</sup>	485,623	120 acres
Spread of contaminant source	m	0	Derived by MULTIMED
Recharge rate	m/yr	0.0368	Five percent of average annual precipitation (1.45 inches/yr)
Initial concentration at landfill (C <sub>0</sub> )	mg/L	1.0	Set at 1.0 to find DAF
Length scale of facility	m		Derived by MULTIMED
Width scale of facility	m		Derived by MULTIMED

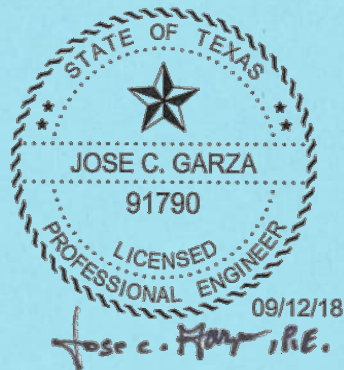
Case	Infiltration Rate (m/yr)	Comments
Interim cases with Alternative Liner		
• 57.5 feet of waste (Case 1) 20 yr	*1.28 x 10 <sup>-7</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 140 feet of waste (Case 2) 20 yr	1.79 x 10 <sup>-7</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 148 feet of waste (Case 3) 20 yr	1.79 x 10 <sup>-7</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 162 feet of waste (Case 4) 20 yr	1.79 x 10 <sup>-7</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
Closed cases with Alternative Liner		
• 57.5 feet of waste (Case 5) 30 yr	5.11 x 10 <sup>-8</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 140 feet of waste (Case 6) 30 yr	5.11 x 10 <sup>-8</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 148 feet of waste (Case 7) 30 yr	5.11 x 10 <sup>-8</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2
• 162 feet of waste (Case 8) 30 yr	5.11 x 10 <sup>-8</sup>	Calculated using peak daily percolation/leakage rate through GCL. See Appx. B.2

\* Determined Using Peak Daily Percolation/Leakage Rate Through GCL and Converted to (M/YR)

Example: ((.00005 FT<sup>3</sup>/Day-Acre)x(1 Acre/43,560 FT<sup>2</sup>)/(1 Meter/3.28 FT)) x (365 Days/1 YR)= 1.28 x 10<sup>-7</sup> M/YR



**APPENDIX C.4**  
**MULTIMED SOURCE-SPECIFIC DATA-OVERLINER DEMONSTRATION**



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**MULTIMED SOURCE - SPECIFIC DATA**

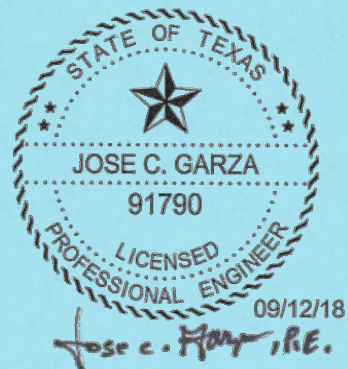
**Overliner Demonstration**

Variable Name	Units	Value	Comments
Infiltration rate	m/yr	varies	See table below.
Area of waste disposal unit	m <sup>2</sup>	485,623	120 acres
Spread of contaminant source	m	0	Derived by MULTIMED
Recharge rate	m/yr	0.0368	Five percent of average annual precipitation (1.45 inches/yr)
Initial concentration at landfill (C <sub>0</sub> )	mg/L	1.0	Set at 1.0 to find DAF
Length scale of facility	m		Derived by MULTIMED
Width scale of facility	m		Derived by MULTIMED

Case	Infiltration Rate (m/yr)	Comments
<b>Interim Cases with Overliner</b>		
Location 1 (Case 1OL) • 12 feet of waste above liner • 15.5 feet of waste below liner 20 yr	$*1.79 \times 10^{-7}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 2 (Case 2OL) • 82.5 feet of waste above liner • 34 feet of waste below liner 20 yr	$1.53 \times 10^{-7}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 3 (Case 3OL) • 85.5 feet of waste above liner • 37 feet of waste above liner 20 yr	$1.53 \times 10^{-7}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 4 (Case 4OL) • 119.5 feet of waste above liner • 16 feet of waste above liner 20 yr	$1.53 \times 10^{-7}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
<b>Closed cases with Overliner</b>		
Location 1 (Case 5OL) • 12 feet of waste above liner • 15.5 feet of waste below liner 30 yr	$5.11 \times 10^{-8}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 2 (Case 6OL) • 82.5 feet of waste above liner • 34 feet of waste below liner 30 yr	$5.11 \times 10^{-8}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 3 (Case 7OL) • 85.5 feet of waste above liner • 37 feet of waste below liner 30 yr	$5.11 \times 10^{-8}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12
Location 4 (Case 8OL) • 119.5 feet of waste above liner • 16 feet of waste below liner 30 yr	$5.11 \times 10^{-8}$	Calculated using peak daily percolation/ leakage rate through GCL. See Appx. B.12

\* Determined Using Peak Daily Percolation/Leakage Rate Through GCL and Converted to (M/YR)  
 Example:  $((.00007 \text{ FT}^3/\text{Day-Acre}) \times (1 \text{ Acre}/43,560 \text{ FT}^2)) / (1 \text{ Meter}/3.28 \text{ FT}) \times (365 \text{ Days}/1 \text{ YR}) = 1.79 \times 10^{-7} \text{ M/YR}$

APPENDIX C.5  
UNSATURATED ZONE DATA

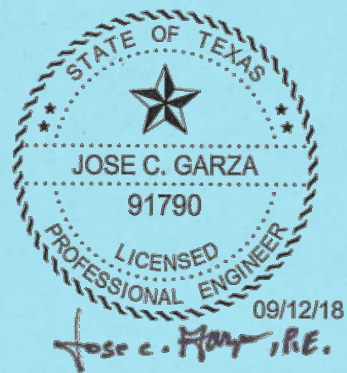


**MULTIMED UNSATURATED ZONE DATA**

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Note that the unsaturated zone was not modeled as part of this point of compliance demonstration. The attenuating effects of the unsaturated zone were conservatively disregarded.

**APPENDIX C.6**  
**MULTIMED AQUIFER-SPECIFIC DATA**



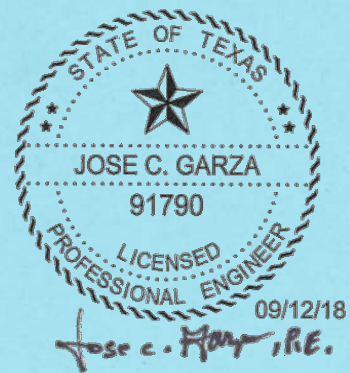
**MULTIMED AQUIFER - SPECIFIC DATA**

Variable Name	Units	Value	Comments
Particle Diameter*	cm	0.0381	From Permit 235-B Amendment Volume II of V Pages 36-39 (PDF)-1998 Material ranges from fine to coarse. Use an average for medium sand (0.010-0.020 in); 0.015 in or 0.0381 cm
Aquifer porosity*	unitless	0.43	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Bulk density	g/cc	1.65	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Aquifer thickness	m	10	From Permit 235-B Amendment Volume V of V Pgs. 467-473 (PDF)-1998 Avg depth of uppermost aquifer
Mixing zone depth	m		Derived by MULTIMED
Hydraulic conductivity	m/yr	130	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998 Average hydraulic conductivity of $4.12 \times 10^{-4}$ cm/sec
Hydraulic gradient	unitless	0.0031	From Groundwater Contour Map (January 2016)
Groundwater seepage velocity	m/yr		Derived by MULTIMED
Retardation coefficient	unitless		Derived by MULTIMED
Longitudinal dispersivity	m		Derived by MULTIMED
Transverse dispersivity	m		Derived by MULTIMED
Vertical dispersivity	m		Derived by MULTIMED
Organic carbon content	%	0.003	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Receptor distance from well	m	Varies	Distance from analysis location to point of compliance.
Z-distance from water table	m	0	Assume water table is at bottom of liner.

Note: According to Amendment Application (1998) the Evangeline Aquifer is the principal aquifer in the region and is considered one of the most prolific aquifers in the Texas Coastal Plain. The aquifer is composed of at least the Goliad Sand and includes sections of sand in the Fleming Formation. The Goliad consists of fine to coarse, mostly gray calcareous sand interbedded with sandstone and varicolored clay.  
 (assume medium sand (0.015 in) particle diameter or (0.0381 cm)

**\* If Aquifer porosity is known MULTIMED will not use particle diameter.**

APPENDIX C.7  
MULTIMED AQUIFER-SPECIFIC DATA-OVERLINER DEMONSTRATION



**MULTIMED AQUIFER - SPECIFIC DATA**

**Overliner Demonstration**

Variable Name	Units	Value	Comments
Particle Diameter*	cm	0.0381	From Permit 235-B Amendment Volume II of V Pages 36-39 (PDF)-1998 Material ranges from fine to coarse. Use an average for medium sand (0.010-0.020 in); 0.015 in or 0.0381 cm
Aquifer porosity*	unitless	0.43	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Bulk density	g/cc	1.65	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Aquifer thickness	m	10	From Permit 235-B Amendment Volume V of V Pgs. 467-473 (PDF)-1998 Avg depth of uppermost aquifer
Mixing zone depth	m		Derived by MULTIMED
Hydraulic conductivity	m/yr	130	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998 Average hydraulic conductivity of $4.12 \times 10^{-4}$ cm/sec
Hydraulic gradient	unitless	0.002	From Groundwater Contour Map (January 2016)
Groundwater seepage velocity	m/yr		Derived by MULTIMED
Retardation coefficient	unitless		Derived by MULTIMED
Longitudinal dispersivity	m		Derived by MULTIMED
Transverse dispersivity	m		Derived by MULTIMED
Vertical dispersivity	m		Derived by MULTIMED
Organic carbon content	%	0.003	From Permit 235-B Amendment Volume V of V Pages 467-473 (PDF)-1998
Receptor distance from well	m	Varies	Distance from analysis location to point of compliance.
Z-distance from water table	m	0	Assume water table is at bottom of liner.

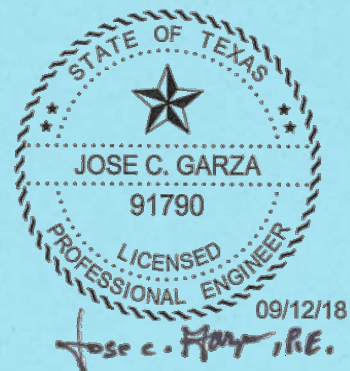
Note: According to Amendment Application (1998) the Evangeline Aquifer is the principal aquifer in the region and is considered one of the most prolific aquifers in the Texas Coastal Plain. The aquifer is composed of at least the Goliad Sand and includes sections of sand in the Fleming Formation. The Goliad consists of fine to coarse, mostly gray calcareous sand interbedded with sandstone and varicolored clay.  
(assume medium sand (0.015 in) particle diameter or (0.0381 cm)

**\* If Aquifer porosity is known MULTIMED will not use particle diameter.**



APPENDIX C.7.1

'APPENDIX E ALTERNATE LINER DESIGN REPORT-CITY OF  
KINGSVILLE MUNICIPAL SOLID WASTE DISPOSAL FACILITY PERMIT  
AMENDMENT APPLICATION MSW 235-B', PAGES 467-473 FROM  
PERMIT 235-B AMENDMENT VOLUME V OF V



**APPENDIX E**

**ALTERNATE LINER DESIGN REPORT**

City of Kingsville  
Municipal Solid Waste Disposal Facility  
Permit Amendment Application MSW 235-B



THIS CERTIFICATION IS INTENDED FOR PERMITTING PURPOSES ONLY AND  
INCLUDES PAGES 1 THROUGH 7.

November 1997

Pages 467 from Permit 235-B Amendment Volume V of V

## ALTERNATE LINER DESIGN REPORT

The City of Kingsville, Texas is proposing a municipal solid waste landfill facility and wishes to consider an alternate design. The proposed site has an expected life of 29 years, area of approximately 120 acres in size, an excavation depth of 20 feet to the bottom of the liner, and an estimated horizontal projection of the leachate collection layer from the top to the collector of 155 ft. Through an extensive ground-water characterization study, the following information was acquired:

Aquifer Specific Data	
Aquifer porosity	0.43 (Silty Clay Loam)
Bulk density	1.65 g/cc = 103 lbm/ft <sup>3</sup>
Aquifer thickness	10m = 32.81 ft.
Average hydraulic conductivity	4.12 X 10 <sup>-4</sup> cm/sec
Hydraulic gradient	0.00331 ft/ft = 0.00331 m/m
Seepage velocity	3.3 ft/yr
Aquifer temperature	21°C
pH	7.2
Organic carbon content	0.003

Four scenarios were considered in evaluating this proposed site:

**Case 1** - A closed landfill with a synthetic GeoClay barrier liner (3.0 X 10<sup>-9</sup> cm/sec), a 60 mil HDPE membrane liner (2 x 10<sup>-12</sup> cm/sec), a Geocomposite drainage layer (10 cm/sec), a 24 inch protective soil layer, 60 feet of waste, an 18 inch soil cover layer, a 60 mil HDPE membrane, a Geocomposite drainage layer, and a 24 inch infiltration and vegetative erosion control layer.

**Case 2** - A closed landfill with a standard composite Subtitle "D" Liner with a Geocomposite drainage layer, 60 feet of waste, and a standard Subtitle "D" cover.

**Case 3** - An open landfill with a synthetic GeoClay barrier liner (3.0 X 10<sup>-9</sup> cm/sec), a 60 mil HDPE membrane liner (2 x 10<sup>-12</sup> cm/sec), a Geocomposite drainage layer (10 cm/sec), a 24 inch protective soil layer, 30 feet of waste (open face 2 acres w/ 320 foot drain length at 4H:1V), and 12 inches of daily soil cover.

**Case 4** - An open landfill with a standard composite Subtitle "D" Liner with a Geocomposite drainage layer, 30 feet of waste (open face 2 acres w/ 320 foot drain length at 4H:1V), and 12 inches of daily soil cover.

### Results of HELP Model

	Avg. Impingement on Drainage Layer, inches	Average Annual Head on Barrier Layer, inches	Avg. Percolation Thru Barrier Layer, ft <sup>3</sup> /yr
Case 1	0.00002	0.000	0.003
Case 2	0.00002	0.000	0.003
Case 3	1.00798	0.000	0.007
Case 4	0.88389	0.000	0.009

#### Evaluation of Leakage Through a Composite Liner

To calculate the leakage rate through a composite liner, it is necessary to determine the impingement rate  $e$  (volume of leachate reaching the leachate collection system). From the HELP3 model printout for Case 4, the average annual precipitation is 40.590 inches (295,000 cubic feet), the average annual evapotranspiration is 20.510 inches (148,900 cubic feet), and the peak daily impingement onto the drainage layer is 0.07075 inches/day (513.7 ft<sup>3</sup>/day).

Maximum thickness of leachate in the leachate collection system  $T_{max}$  must be less than the thickness of the leachate collection system, and  $T_{max}$  must be less than 30 cm as per 31 TAC 330.203.

Thus:

$$\begin{aligned}
 e &= 0.07075 \text{ inches/day} = 2.1 \times 10^{-8} \text{ m/s} \\
 k &= 1.0 \times 10^{-1} \text{ cm/sec} = 1.0 \times 10^{-1} \text{ m/s} \\
 \tan \beta &= 2.0\% \\
 L &= 155 \text{ ft} = 47.2 \text{ meters}
 \end{aligned}$$

$$T_{max} = \frac{47.2 * \sqrt{0.0000008.4 + 0.0004} - 0.020}{1.9996}$$

$$T_{max} = 0.000495 \text{ meters} = 0.0195 \text{ inches}$$

This value compares well with 0.019 inches calculated in Case 4 and is less than the maximum allowed head of 30 cm (12 inches).

However, when evaluating leakage through a liner to use in a fate and transport model (i.e., Multimed), a more conservative value is recommended. One reasonably conservative estimate would be to assume the sand drainage layer is saturated, or  $h = 12$  inches.

Leakage through a composite liner:

$$\begin{aligned}
 a &= 0.16 \text{ sq. in.} = 0.0001 \text{ m}^2 \\
 h_{tb} &= 12.0 \text{ in.} = 0.305 \text{ m.} \\
 k_{st} &= 1.0 \times 10^7 \text{ cm/sec} = 1.0 \times 10^9 \text{ m/s}
 \end{aligned}$$

For good contact:

$$\begin{aligned}
 Q_{tb} &= 0.21 * (1.0 \times 10^4 \text{ m}^2)^{0.1} * (0.305 \text{ m})^{0.9} * (1.0 \times 10^9 \text{ m/sec})^{0.74} \\
 Q_{tb} &= 0.63 \times 10^8 \text{ m}^3/\text{sec}/\text{hole} = 0.1438 \text{ gal/day}/\text{hole}
 \end{aligned}$$

For poor contact:

$$Q_{tb} = (1.15/0.21) * 0.1438 = 0.7875 \text{ gal}/\text{hole}/\text{day}$$

Assuming 7 holes per acre, the estimated leakage through a composite liner with poor contact would be:

$$\begin{aligned}
 Q &= (7 \text{ holes}/\text{acre}) * (2 \text{ acres}) * (0.7875 \text{ gal}/\text{day}/\text{hole}) \\
 Q &= 11.0 \text{ gal}/\text{day} = \text{INFiltration Rate} = 0.00188 \text{ m}/\text{yr}
 \end{aligned}$$

#### Evaluation of Leakage Through a GeoClay Synthetic Liner

To calculate the leakage rate through a synthetic GeoClay liner, it is necessary to determine the impingement rate  $e$  (volume of leachate reaching the leachate collection system). From the HELP3 model printout for Case 2, the average annual precipitation is 40.590 inches (295,000 cubic feet), the average annual evapotranspiration is 20.882 inches (151,600 cubic feet), and the peak daily impingement onto the drainage layer is 0.07850 inches/day (570.0 ft<sup>3</sup>/day).

Maximum thickness of leachate in the leachate collection system  $T_{max}$  must be less than the thickness of the leachate collection system, and  $T_{max}$  must be less than 30 cm as per 31 TAC 330.203.

Thus:

$$\begin{aligned}
 e &= 0.0785 \text{ inches}/\text{day} = 2.3 \times 10^8 \text{ m/s} \\
 k &= 1.0 \times 10^1 \text{ cm}/\text{sec} = 1.0 \times 10^1 \text{ m/s} \\
 \tan \beta &= 2.0\% \\
 L &= 155 \text{ ft} = 47.2 \text{ meters}
 \end{aligned}$$

$$T_{max} = \frac{47.2 * \sqrt{0.00000092 + 0.0004} - 0.020}{1.9996}$$

$$T_{\max} = 0.0005426 \text{ meters} = 0.0214 \text{ inches}$$

This value compares well with 0.022 inches calculated in Case 3 and is less than the maximum allowed head of 30 cm (12 inches).

However, when evaluating leakage through a liner to use in a fate and transport model (i.e., Multimod), a more conservative value is recommended. One reasonably conservative estimate would be to assume the sand drainage layer is saturated, or  $h = 12$  inches.

Leakage through a composite liner:

$$\begin{aligned} a &= 0.16 \text{ sq. in.} = 0.0001 \text{ m}^2 \\ h_{tb} &= 12.0 \text{ in.} = 0.305 \text{ m.} \\ k_{st} &= 3.0 \times 10^{-9} \text{ cm/sec} = 3.0 \times 10^{-11} \text{ m/s} \end{aligned}$$

For good contact:

$$\begin{aligned} Q_{tb} &= 0.21 * (1.0 \times 10^{-4} \text{ m}^2)^{0.1} * (0.305 \text{ m})^{0.9} * (3.0 \times 10^{-11} \text{ m/sec})^{0.74} \\ Q_{tb} &= 4.677 \times 10^{-10} \text{ m}^3/\text{sec}/\text{hole} = 0.01068 \text{ gal/day}/\text{hole} \end{aligned}$$

For poor contact:

$$Q_{tb} = (1.15/0.21) * 0.01068 = 0.05847 \text{ gal}/\text{hole}/\text{day}$$

Assuming 7 holes per acre, the estimated leakage through a composite liner with poor contact would be:

$$\begin{aligned} Q &= (7 \text{ holes/acre}) * (2 \text{ acres}) * (0.05847 \text{ gal/day}/\text{hole}) \\ Q &= 0.8185 \text{ gal/day} = \text{INFiltration Rate} = 0.000140 \text{ m}/\text{yr} \end{aligned}$$

Analysis of the 30 cm (12 inches) head on High Drainage Layers:

The 12 inch head on these synthetic liners with Geocomposite drainage layers seems unreasonable. Therefore, let's answer some questions prior to proceeding to input the MultiMed Model.

First, What flow would be required to create a 12" head on the drainage layer?

Solving the Head Equation in reverse for impingement rate:

$$T_{\max} = 12" = 0.3048 \text{ meters}$$

$$\therefore 0.3048m = \frac{47.2 * (\sqrt{4 * (\frac{e}{0.1}) + 0.0004} - 0.020)}{1.9996}$$

$e = 0.00001708 \text{ m/sec} = 58.10 \text{ inches/day!!!!!!}$

This impingement rate is **more than the max annual rainfall** coming in one day;  
**more than a 25 year, 24 hour storm**;  
**more than a 100 year, 24 hour storm**; and  
**equals 3,155,530 gallons/day** impingement

just to create 12 inches of head on the drainage layer! Nevertheless, the two comparative cases (cases 11&12) have been run. They illustrate that the Subtitle D Liner will not pass the criteria under 12" head, but that the alternateve GeoClay liner will.

A better conservative estimate for this type of system would be an assumption of a 25 year, 24 hour storm (9 inches/day) hitting the landfill, and using the HELP3 model to estimate the drainage layer impingement in each case. The peak daily precipitation rate for the HELP3 model cases was 7.92 inches. Therefore, we shall increase the impingement on the lower synthetic liner by the ratio of (9.00"/7.92") This generates the following impingement rates on the liners for cases 1 through 4:

Case No.	25 yr, 24 hr Storm HELP Perc'n thru Barrier Layer, ft3/day	25 yr, 24 hr Storm HELP Perc'n thru Barrier Layer, inch/day	25 yr, 24 hr Storm HELP Perc'n thru Barrier Layer, meter/year
1 - COK Alt. Liner Closed	0.0000114	0.000000571	0.0000053
2 - STD Liner Closed	0.0000114	0.000000571	0.0000053
3 - COK Alt. Liner Open	0.0000682	0.00000343	0.0000318
4 - STD Liner Open	0.00025	0.0000126	0.000117

These infiltration rates were used as input to the MultiMed Model and produced the following results:

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Evaluation of leachate concentration at Point of Compliance

Based on the above calculations, the infiltration rate to be input into the Multimed models are:

- For GeoClay Barrier Liner(Closed): Infiltration = 0.031 gal/day = 0.0000053 m/yr
- For Std Subtitle "D" Liner(Open): Infiltration = 0.031 gal/day = 0.0000053 m/yr
- For GeoClay Barrier Liner(Open): Infiltration = 0.1862 gal/day = 0.0000318 m/yr
- For Std Subtitle "D" Liner(Open): Infiltration = 0.6826 gal/day = 0.000117 m/yr

The first Multimed model was run for Case 1 (Closed landfill, alternate design, steady state). The second model run for Case 2 (Closed landfill, Subtitle "D", steady state). The third model run for Case 3 (Open landfill, alternate design, steady state). The fourth model run for Case 4 (Open landfill, Subtitle "D", steady state). Results of these models are tabulated below:

**Results of Multimed Models**

	Concentration at POC	Dilution Attenuation Factor
Case 1 (steady state)	0.0002089	4,787
Case 2 (steady state)	0.0002089	4,787
Case 3 (steady state)	0.001253	798
Case 4 (steady-state)	0.0004606	217

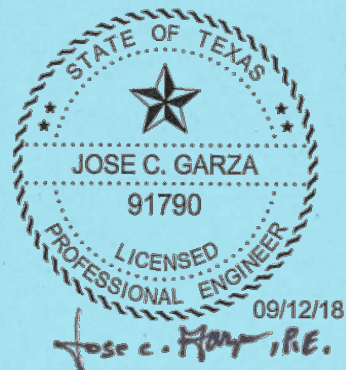
Conclusions

As can be seen by comparing the Dilution Attenuation Factors (DAF's) for the alternate design scenarios, Case 1 and Case 3 (4,787 and 798, respectively) with the minimum required DAF's listed in Table 2, it has been demonstrated through the use of the HELP and Multimed models that the alternate design is sufficient for all constituents.



**APPENDIX C.7.2**

**'CITY OF KINGSVILLE MSWLF-PERMIT 235-B ATTACHMENT 4-  
GEOLOGY REPORT, 4.0 REGIONAL AQUIFERS', PAGES 36-39 FROM  
235-B AMENDMENT VOLUME II OF V**



## 4.0 Regional Aquifers

The Evangeline Aquifer is the principal aquifer in the region and is considered one of the most prolific aquifers in the Texas Coastal Plain. The aquifer is composed of at least the Goliad Sand and includes sections of sand in the Fleming Formation. Only in South Texas the base of the Evangeline coincides with the base of the Goliad. The upper boundary of the Evangeline probably follows closely the top of the Goliad Sand where present, but this relationship is somewhat speculative (Muller, 1979). (See Figure 4.11) Ground water flow direction in the Evangeline is in a Northerly direction based on a water level map of the Goliad sand. There are two very significant cones of depression in the Evangeline (Goliad) aquifer located to the northwest of the City of Kingsville MSWLF site. These depressions are primarily due to large groundwater production rates by the City of Kingsville and the Exxon King Ranch Gas Plant. The extent of salt water intrusion from the Gulf of Mexico into the Evangeline (Goliad) aquifer is shown on Figure 4.16.

The Goliad consists of fine to coarse, mostly gray calcareous sand interbedded with sandstone and varicolored clay. Recharge within the site area occurs along the outcrop which is located in western Hidalgo, central-eastern Starr, central Jim Hogg, Duval, southeastern Webb, northeastern Brooks, northern Jim Wells, and extreme northeast Zapata counties, as well as other counties to the north. The maximum width of the outcrop is west of Falfurrias where the Goliad Sand extends for nearly 50 miles at the surface and completely overlaps the underlying Lagarto Clay and Oakville Sandstone and nearly overlaps the Catahoula Tuff (Shafer, 1973). (See Figure 4.12)

The water of the Goliad is under artesian pressure and is yielded to flowing and nonflowing wells. The average coefficient of transmissibility determined during drawdown of the fresh to slightly saline water section of the Goliad Sand in southwestern Kleberg County measured in well no. RR-83-41-803, was about 34,400 gpd per foot. The specific capacity of the well was 17.8 gpm per foot. This was derived from a screened interval of 126 feet near the north boundary of Kenedy and south boundary of Kleberg Counties.

Fresh water of domestic use quality in the Evangeline is found in well developed sands at depths of 500 feet and greater in the MSWLF area. From surface to the fresh water sands in the Evangeline the lithology is predominately a clay described as silty, calcareous, firm to hard with occasionally silty sands.

The regional Chicot aquifer lies approximately 220 feet below ground surface in the vicinity of the MSWLF according to two deep well logs obtained from a local mineral company. (See Section 4.2) The Light Olive Green Clay layer serves as aquiclude between the uppermost aquifer below the landfill site and the Chicot aquifer. In Kleberg County, and specifically the MSWLF, the waters from the Chicot aquifer are generally slightly-saline to saline and yield only marginal quantities of water.

The local unconfined water table aquifer tends to flow in all directions away from the landfill site. The only exception is that for a period of time after excessive rainfall events, ground water in this local uppermost aquifer tends to flow toward the site from the northwest. This determination is based on water levels recorded in wells completed for use in the current expansion phase. However, the largest gradients for ground water flow are in the northeast and southwest directions. The flow toward the southwest is along a caliche channel which slopes to the southwest toward some lower elevation caliche pits. The flow toward the northeast is toward the Santa Gertrudis creek. However, the ground water tends to flow through some fairly tight clay in that direction. The high point of ground water at the MSWLF site is at least partially a following of the surface topography and influenced by direct recharge from any ponding which is not promptly removed. Attachment 5, Appendix E gives a more thorough analysis of ground water direction and rate of ground water flow.

The initial interpretation, based on available data and monitor well density and location, indicated a predominate flow to the north or west. Completion of monitor and observation wells in the current expansion program indicate a northeast flow direction. Later analysis shows that ground water flows slowly away from MSWLF in all directions. This is based on measurements of the top of the saturated zone as evidence by water levels in wells. The initial flow direction determined by REI when the landfill was started was toward the northeast.

#### 4.1 Water Quality

The water quality of the Goliad is highly variable. Chloride contents in the wells sampled ranged from 94 to 9,100 mg/l, exceeding 250 mg/l in 60% of the samples. Sulfate content ranged from 26 to 4,630 mg/l. In Kleberg County, 33% of the samples exceeded 250 mg/l sulfate. Dissolved-solids content ranged from 601 to 49,900 mg/l. Over 75% exceeded 1,000 mg/l dissolved-solids. In summary, ground water that meets most of the quality standards of the U.S. Public Health Service is available from wells less than 1,000 feet deep in the Goliad Sand, Principally in southern Jim Wells County, the western one-half of Kleberg County, and in a few other relatively small areas throughout the report area. Shallow, moderately saline to very saline water overlies the fresh to slightly saline water at most places (Shafer, 1973). (See Figure 4.13)

The Beaumont Clay and Lissie Formation, undifferentiated, (Chicot Aquifer) yields small quantities of slightly to moderately saline water to a few shallow wells used mostly for stock needs in eastern Kleberg and Kenedy Counties. Test wells drilled near Riviera, 15 miles south of Kingsville, in southern Kleberg County show that in this area the shallow sands of the Beaumont and Lissie (Chicot) usually contain very saline water. This group is not considered a supply of useable water because of the highly mineralized water associated with formations in most places. The casings of many wells are cemented through these

City of Kingsville MSWLF - Permit 235 B  
 Attachment 4 - Geology Report

formations. (Shafer, 1973)

Water held in the Beaumont Clay and Lissie Formation, undifferentiated, (Chicot) is under water-table (unconfined) conditions. There were no recoverable aquifer tests from reference material on this formation as it occurs in the area of the site. This formation is not recognized as a useable source of ground water.

Historical ground water monitoring from in-place monitor wells indicates that the sulfates range approximately from 45 to 500 mg/l, chlorides from approximately 50 to 500 mg/l, and dissolved-solids from approximately 500 to 6,000 mg/l. Values of pH have consistently ranged between 7.00 and 8.00. More detailed analytical data from the ground water monitor wells at the site is given in Table 5.1 in Attachment 5.

**4.2 Hydraulic Connection**

No hydraulic connection was found between the uppermost fluvial-deltaic beds which will host the MSWLF and the deeper Chicot and Evangeline (Goliad) aquifers.

Deep elevations prepared from water well data located in the vicinity show that the Chicot aquifer is located approximately 200 feet below ground surface in the MSWLF vicinity. This data is confirmed by electric logs from two (2) deep uranium tests located on the southeast side and adjacent to the MSWLF acreage block ( URI, Inc. well nos. 2001 & 2016). These wells exhibit the top of the main Chicot sand body at depths of 220 & 225' of measured depth, respectively. The top of the deeper Evangeline (Goliad) sands are found at approximately 500' MD. A confining clay, at the base of the fluvial-deltaic section which will host the MSWLF, is indicated in both URI wells to depths of 120' and 130' respectively. In addition, four deep borings (wells 21,23,24,25) at the MSWLF confirm that the "light olive green clay" is ubiquitous under the site with a minimum proven thickness of 38'.

TABLE 4.2.1

WELL #	ELEVATION (feet)	TOTAL DEPTH (feet)	TOP LT OLIVE GRN CLAY (ft.,+M.S.L.)	FOOTAGE OF CLAY
21	52.4	84	+6.4	38
23	49.5	86	+13.5	38
24	47.4	72	+15.4	40
25	61.1	88	+11.1	38

The "light olive green clay" is the aquiclude for the MSWLF facility.

### 4.3 Recharge

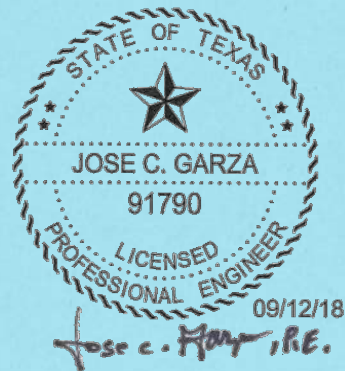
Recharge within a 5 mile radius is from downward percolation of surface water, infiltration from streams, impoundments and water retained in abandoned caliche pits. (Figure 4.14) Flow through the soils is very slow.

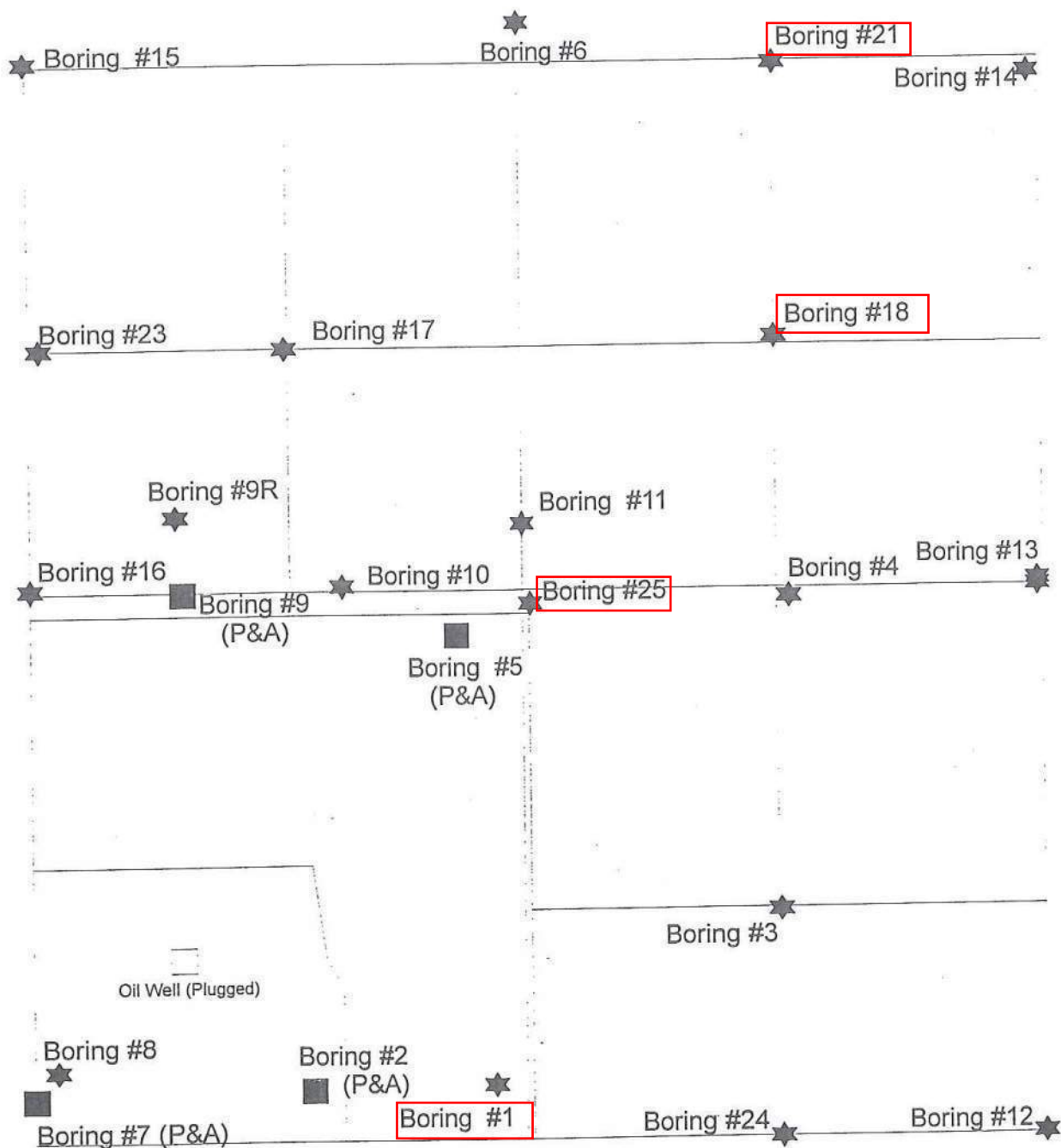
### 4.4 Water Use

A survey of, and for, water wells within a 1 mile radius of the MSWLF site was prepared by Agency Information Consultants (AIC). All known water wells within the survey area produce water for domestic use from the Evangeline Aquifer (Goliad Sand). Thirty one wells were identified in the survey area. (See Figure 4.15) Depth to the top of the perforated or screened interval varies from 524 feet to 726 feet, with an average depth of 621 feet. (See Figures 4.12 & 4.13) There are no known water wells completed in the Chicot aquifer for potable water. There are a few stock wells. The water from the Chicot is mostly very saline. This salinity causes casing corrosion problems with the good fresh water wells in the Goliad aquifer unless they are cemented properly through the Chicot.

APPENDIX C.7.3

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'FIGURE 5.16 BORING  
PLOT PLAN', PAGE 197 FROM PERMIT 235-B AMENDMENT VOLUME  
II OF V





**Figure 5.16 Boring Plot Plan**  
City of Kingsville, Tx      Municipal Solid Waste Landfill

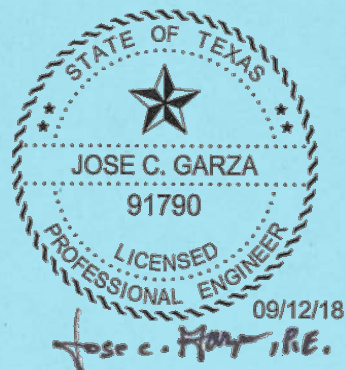
LAT: 27° 26' 41.95"      LONG: 97° 48' 55.89"

0      400      800  
Scale: 1" = 400'

Finch Energy & Environmental Services, Inc.

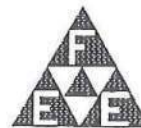
APPENDIX C.7.4

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'SUBSURFACE  
EXPLORATION RECORD B/W NO. 21', PAGE 371 FROM PERMIT 235-B  
AMENDMENT VOLUME II OF V



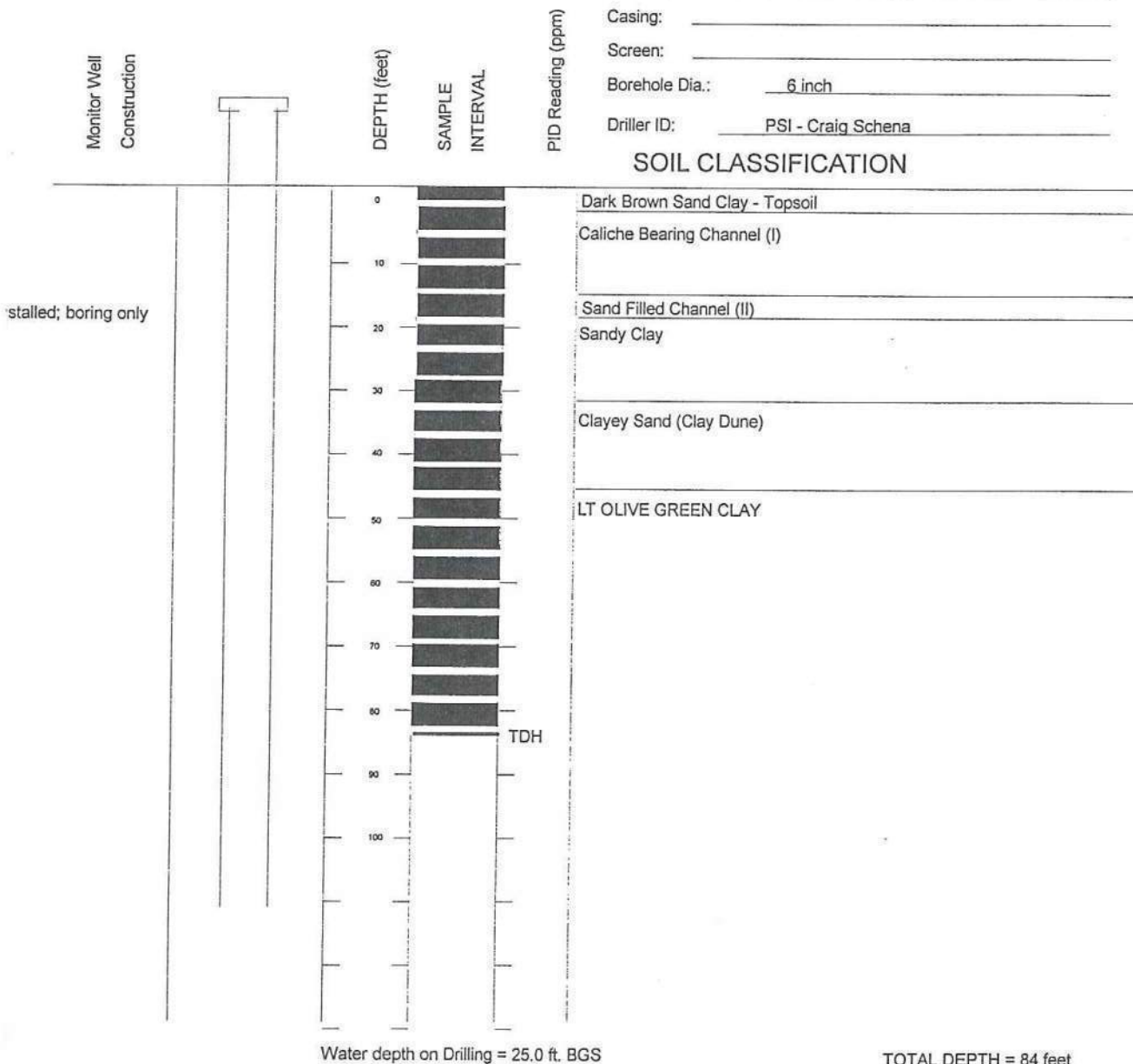


FINCH ENERGY AND ENVIRONMENTAL SERVICES, Inc.  
 P.O. Box 73, Kingsville, Texas 78364-0073



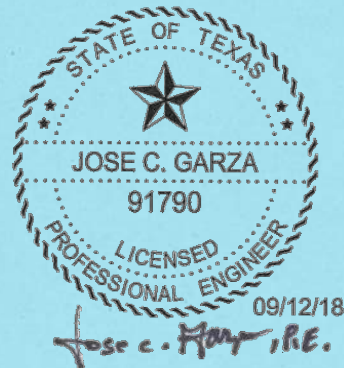
SUBSURFACE EXPLORATION RECORD

Client: <u>City of Kingsville</u>	Boring/Well No.: <u>21</u>
Project Name: <u>Kingsville Landfill</u>	Date Drilled: <u>April 27, 1998</u>
Project Location: <u>5 mi SE of City</u>	Boring Method: <u>HOLLOW STEM AUGER</u>
LAT: <u>27° 26' 09"</u> LONG: <u>97° 48' 47.6"</u>	Sample Method: <u>Shelby Tube</u>
MSWLF ID: <u>Permit #235-B</u>	Surface Elevation: <u>52.41' MSI</u>
	Depth to Water: <u>17.8' BGS</u>
	Total Depth: <u>84' BGS</u>
	Casing: _____
	Screen: _____
	Borehole Dia.: <u>6 inch</u>
	Driller ID: <u>PSI - Craig Schena</u>

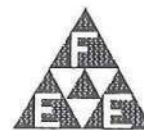


APPENDIX C.7.5

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'SUBSURFACE  
EXPLORATION RECORD B/W NO. 18', PAGE 369 FROM PERMIT 235-B  
AMENDMENT VOLUME II OF V



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 P.O. Box 73, Kingsville, Texas 78364-0073  
 (512) 592-9810 (512) 592-5552 FAX

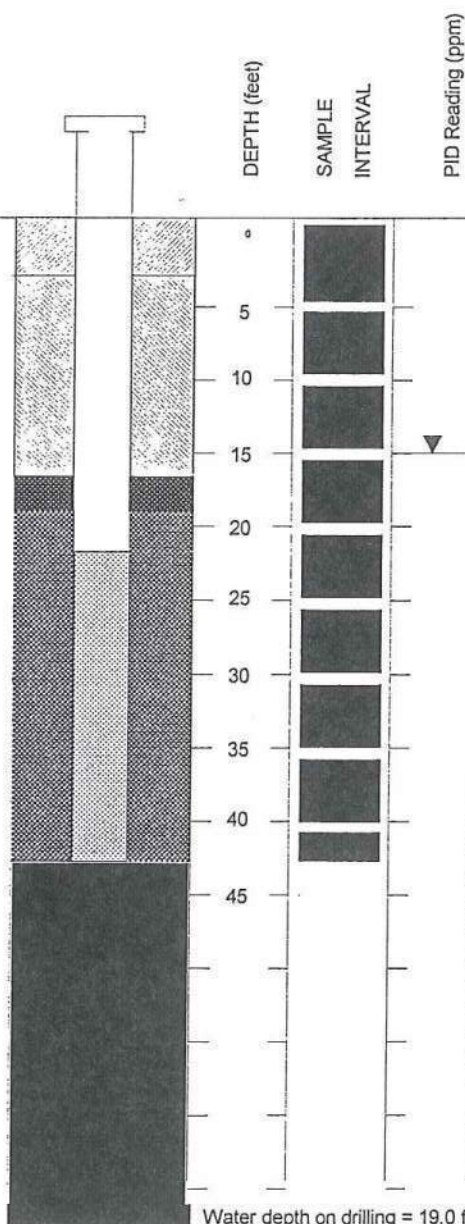


SUBSURFACE EXPLORATION RECORD

Client: City of Kingsville  
 Project Name: Kingsville Landfill  
 Project Location: 5 mi. SE of City  
 LAT: 27° 27' 01.4" LONG: 97° 49' 04 "  
 MSWLF ID: Permit #235-B

Boring/Well No.: 18  
 Date Drilled: July 9, 1997  
 Boring Method: Hollow Stem Auger  
 Sample Method: 5 foot core barrel  
 Surface Elevation: 50.04' MSL  
 Depth to Water: 15' BGS  
 Total Depth: 42' BGS  
 Casing: 2" S-40 PVC - 0-22' BGS  
 Screen: 20' of 2" S-40 PVC - 22' BGS  
 Borehole Dia.: 6 inches  
 Driller: PSI - Craig Schena

Monitor Well  
 Construction



SOIL CLASSIFICATION

DARK BROWN SANDY CLAY TOPSOIL

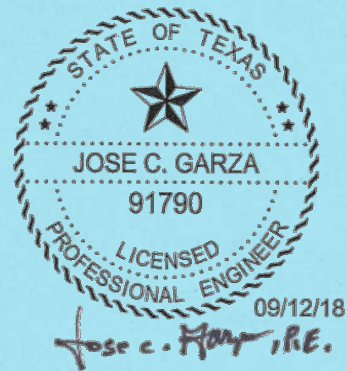
SAND FILLED CHANNEL (II)

SANDY CLAY  
 SILTY CLAY

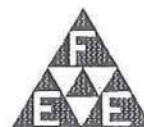
TOTAL DEPTH = 42 ft.

APPENDIX C.7.6

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'SUBSURFACE  
EXPLORATION RECORD B/W NO. 25', PAGE 374 FROM PERMIT 235-B  
AMENDMENT VOLUME II OF V

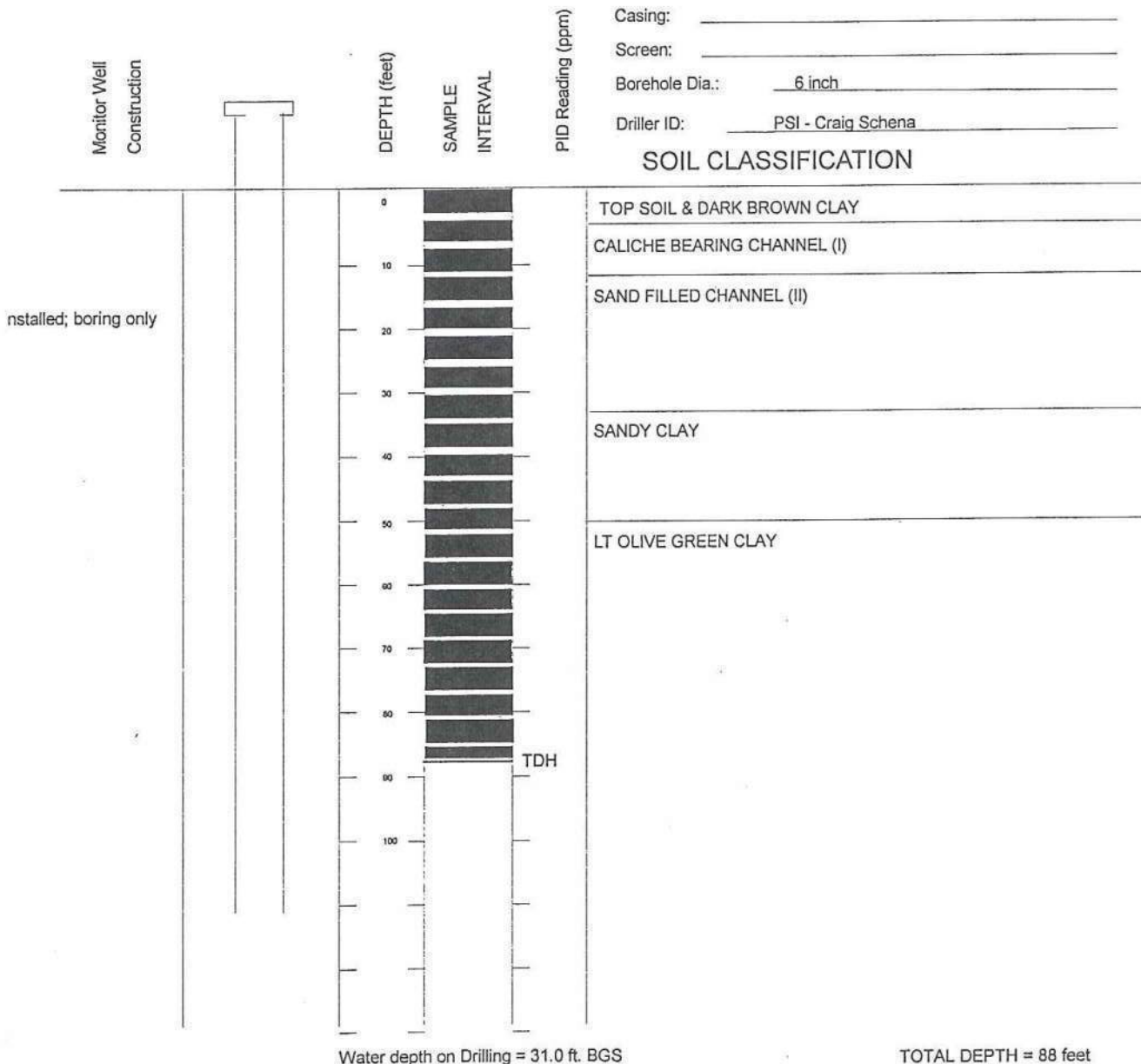


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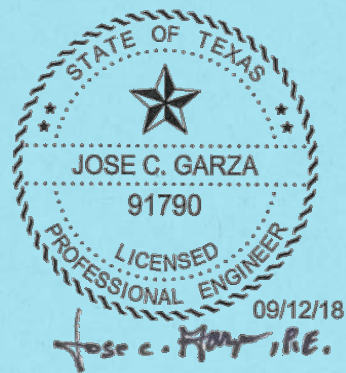
SUBSURFACE EXPLORATION RECORD

Client: <u>City of Kingsville</u>	Boring/Well No.: <u>25</u>
Project Name: <u>Kingsville Landfill</u>	Date Drilled: <u>April 29, 1998</u>
Project Location: <u>5 mi SE of City</u>	Boring Method: <u>HOLLOW STEM AUGER</u>
LAT: <u>27° 26' 55.2"</u> LONG: <u>97° 48' 41.8"</u>	Sample Method: <u>SPLIT SPOON</u>
MSWLF ID: <u>Permit #235-B</u>	Surface Elevation: <u>61.12' MSL</u>
	Depth to Water: <u>21.1' BGS</u>
	Total Depth: <u>88' BGS</u>
	Casing: _____
	Screen: _____
	Borehole Dia.: <u>6 inch</u>
	Driller ID: <u>PSI - Craig Schem</u>

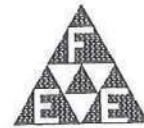


APPENDIX C.7.7

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'SUBSURFACE  
EXPLORATION RECORD B/W NO. 1', PAGE 351 FROM PERMIT 235-B  
AMENDMENT VOLUME II OF V



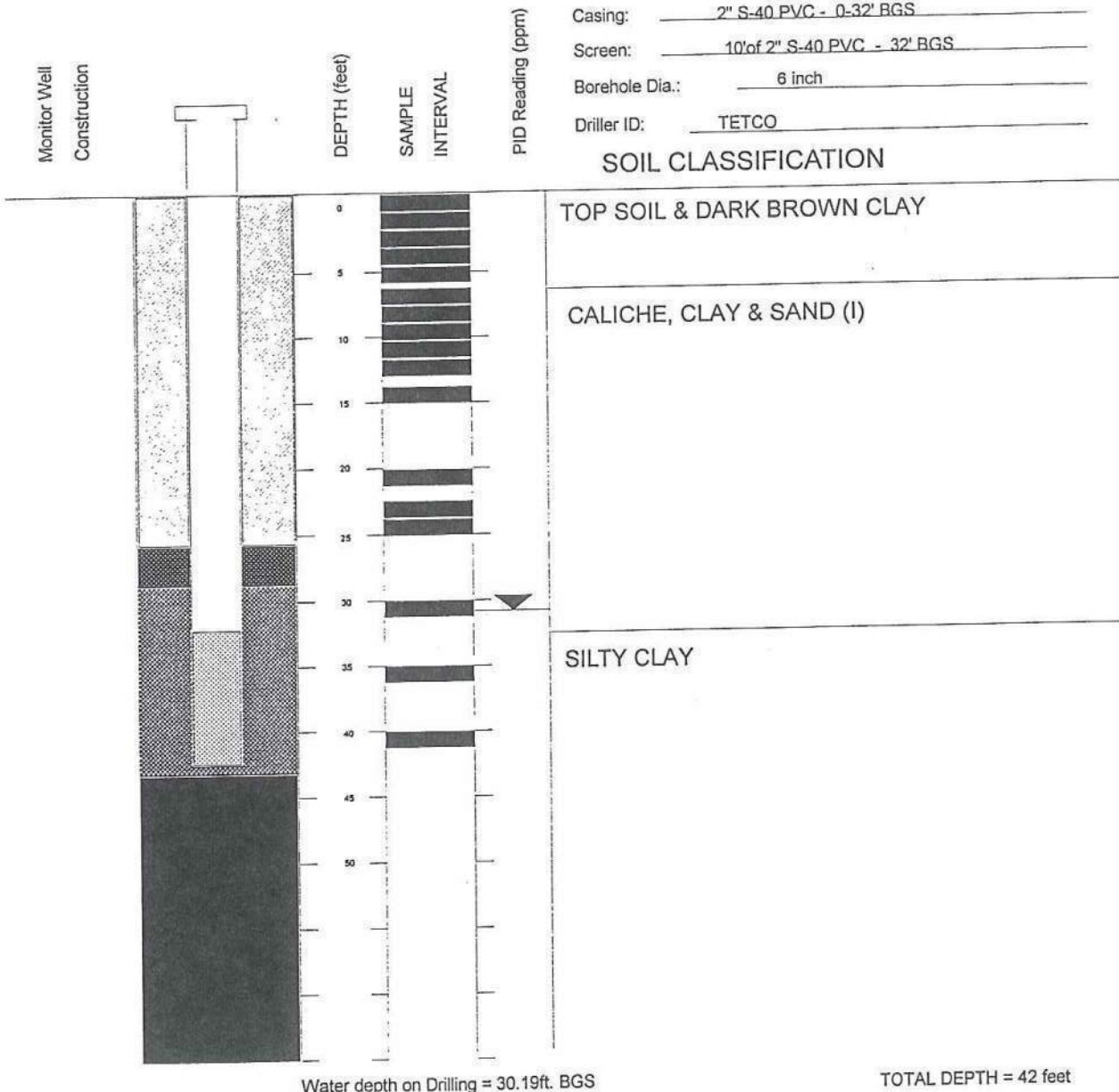
FINCH ENERGY AND ENVIRONMENTAL SERVICES, Inc.  
 P.O. Box 73, Kingsville, Texas 78364-0073



SUBSURFACE EXPLORATION RECORD

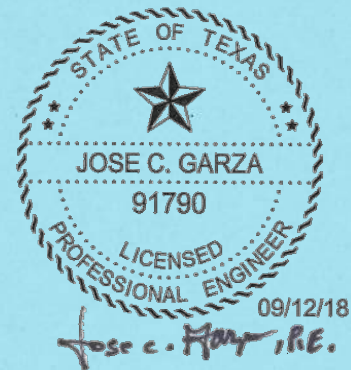
Client: City of Kingsville  
 Project Name: Kingsville Landfill  
 Project Location: 5 mi SE of City  
 LAT: 27° 26' 42.2" LONG: 97° 49' 10.6"  
 MSWLF ID: Permit #235-B

Boring/Well No.: 1  
 Date Drilled: June 19, 1984  
 Boring Method: Hollow Stem Auger  
 Sample Method: SHELBY TUBE & SPLIT SPOON  
 Surface Elevation: 59.25' MSI  
 Depth to Water: 31.0' BGS  
 Total Depth: 42' BGS  
 Casing: 2" S-40 PVC - 0-32' BGS  
 Screen: 10' of 2" S-40 PVC - 32' BGS  
 Borehole Dia.: 6 inch  
 Driller ID: TETCO



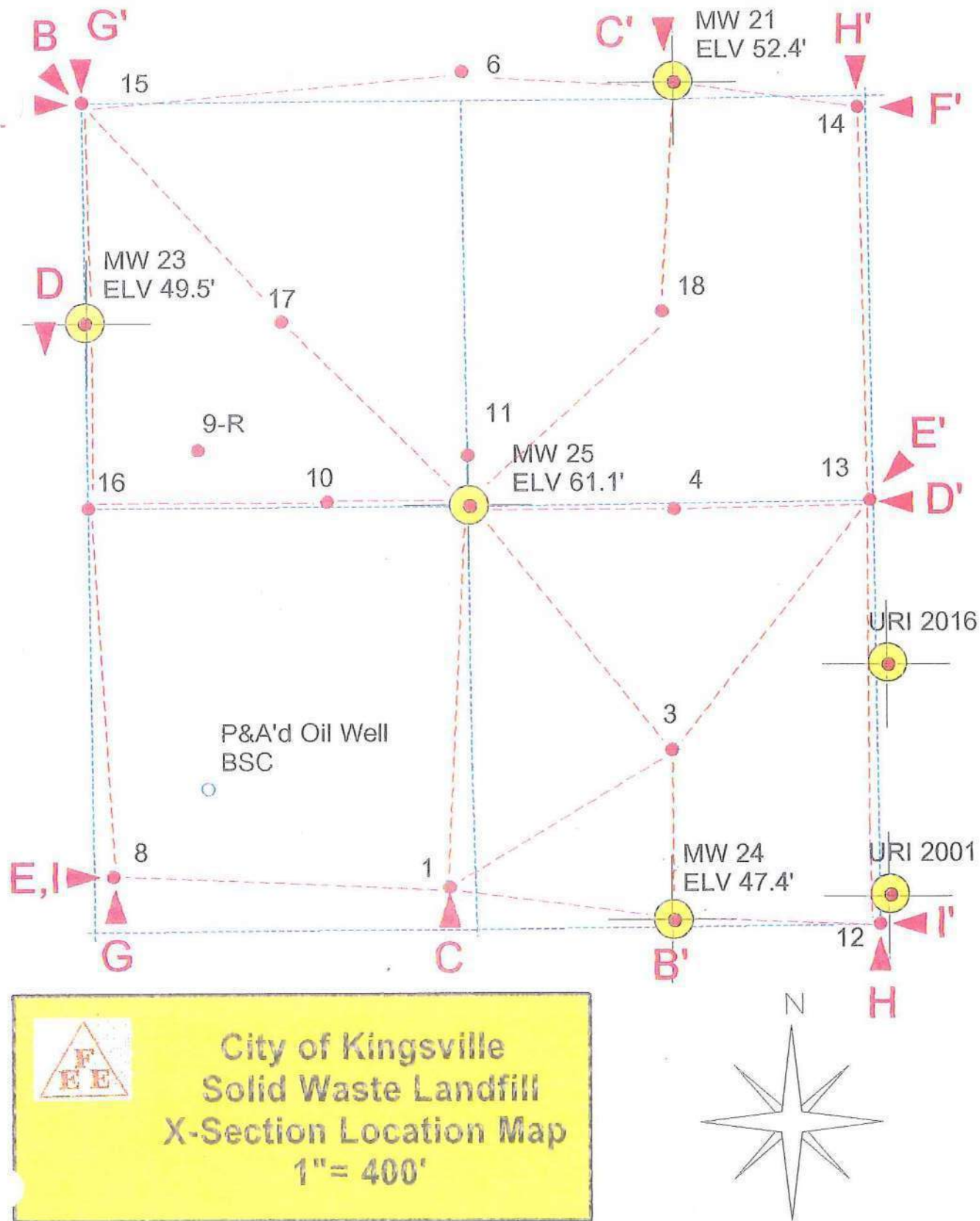
APPENDIX C.7.8

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'X-SECTION LOCATION  
MAP', PAGE 68 FROM PERMIT 235-B AMENDMENT VOLUME II OF V





FOR PERMIT PURPOSES ONLY



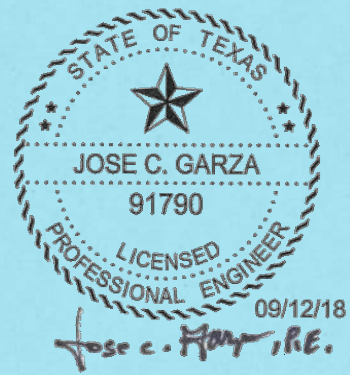
Page 68 from Permit 235-B Amendment Volume II of V

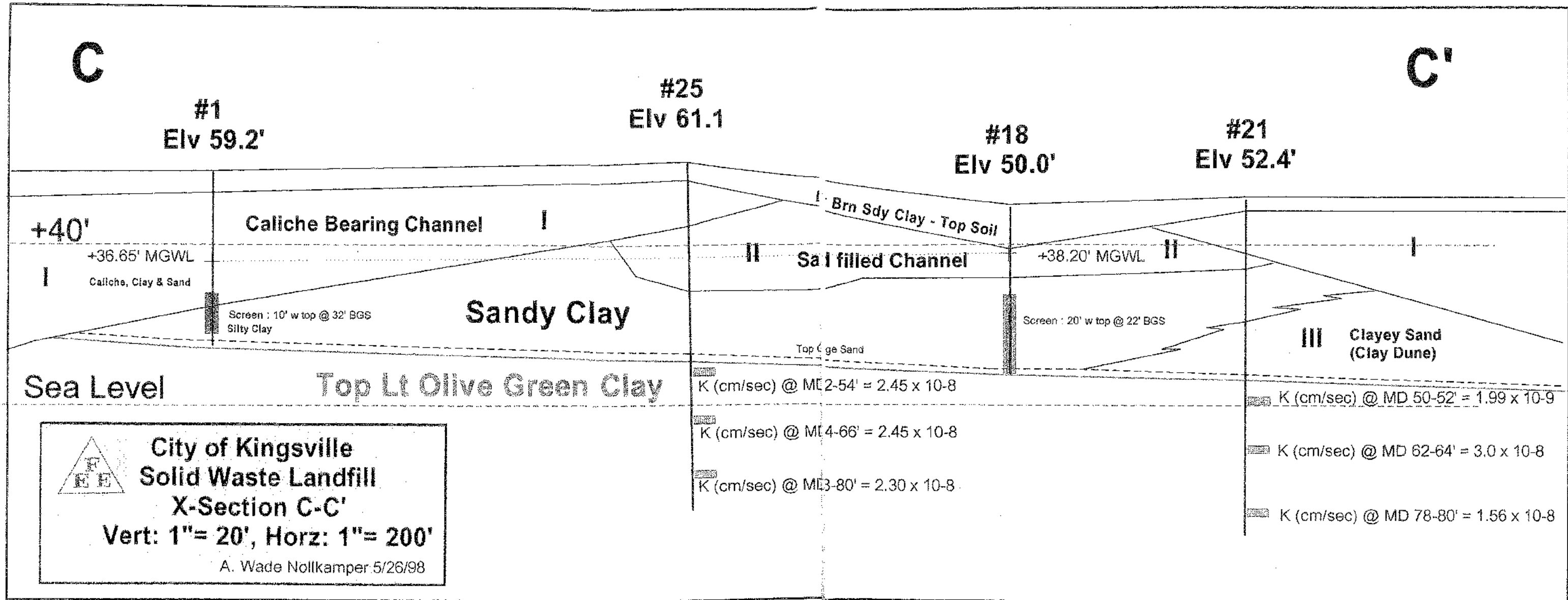
REVISION 1

48

APPENDIX C.7.9

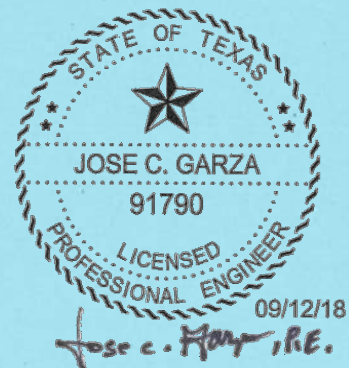
'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'X-SECTION C-C'',  
PAGE 71 FROM PERMIT 235-B AMENDMENT VOLUME II OF V





APPENDIX C.7.10

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'CORRELATION OF  
GEOLOGIC UNITS ALONG A-A KLEBERG AND SOUTHERN JIM  
WELLS COUNTIES'', PAGE 45 FROM PERMIT 235-B AMENDMENT  
VOLUME II OF V



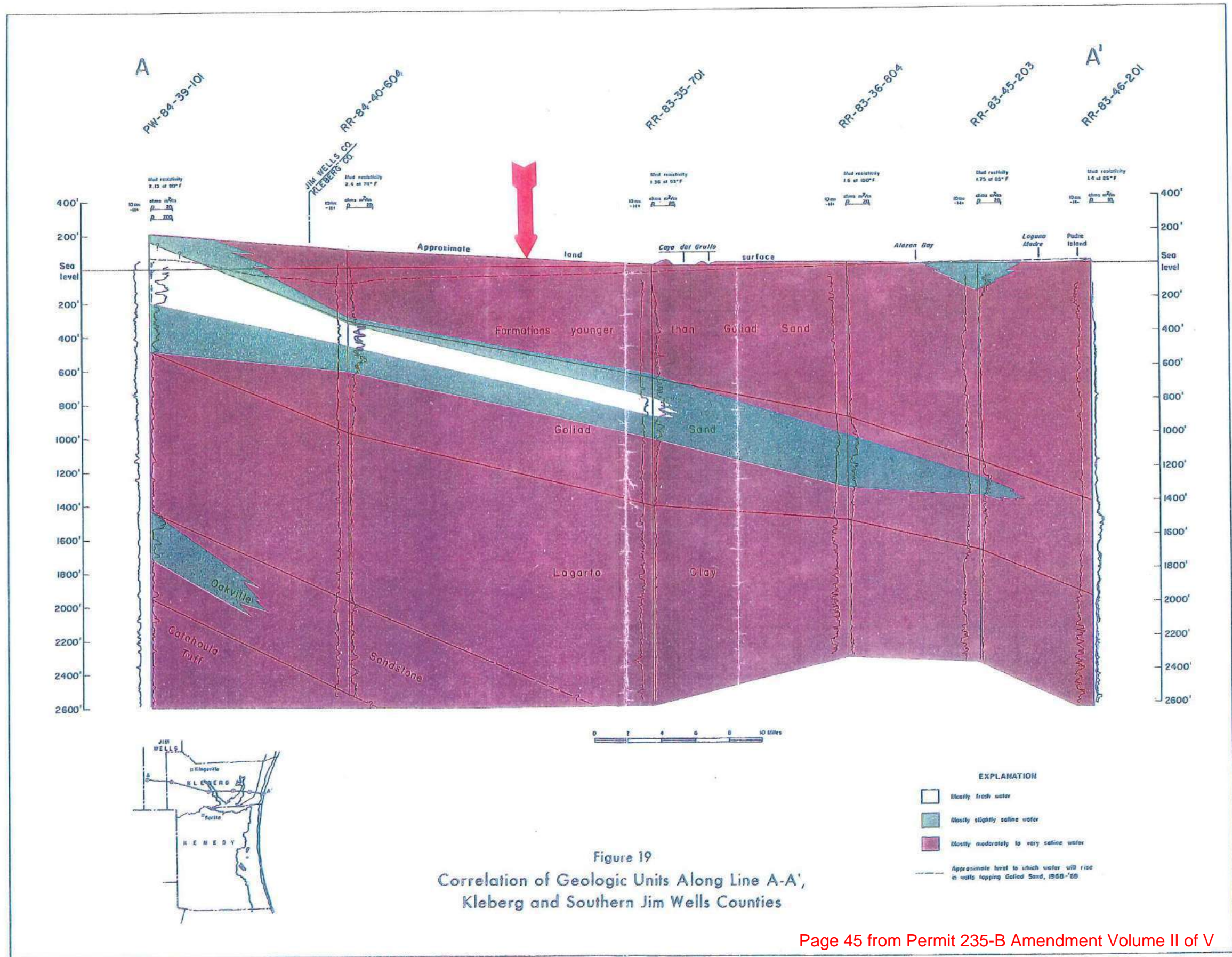
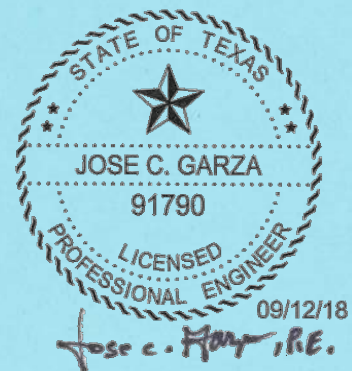


Figure 19  
 Correlation of Geologic Units Along Line A-A',  
 Kleberg and Southern Jim Wells Counties

Page 45 from Permit 235-B Amendment Volume II of V

APPENDIX C.7.11

'CITY OF KINGSVILLE MSWLF-PERMIT 235-B 'STRATIGRAPHIC AND  
HYDROGEOLOGIC SECTION I-I'', PAGE 43 FROM PERMIT 235-B  
AMENDMENT VOLUME II OF V



FOR PERMIT PURPOSES ONLY

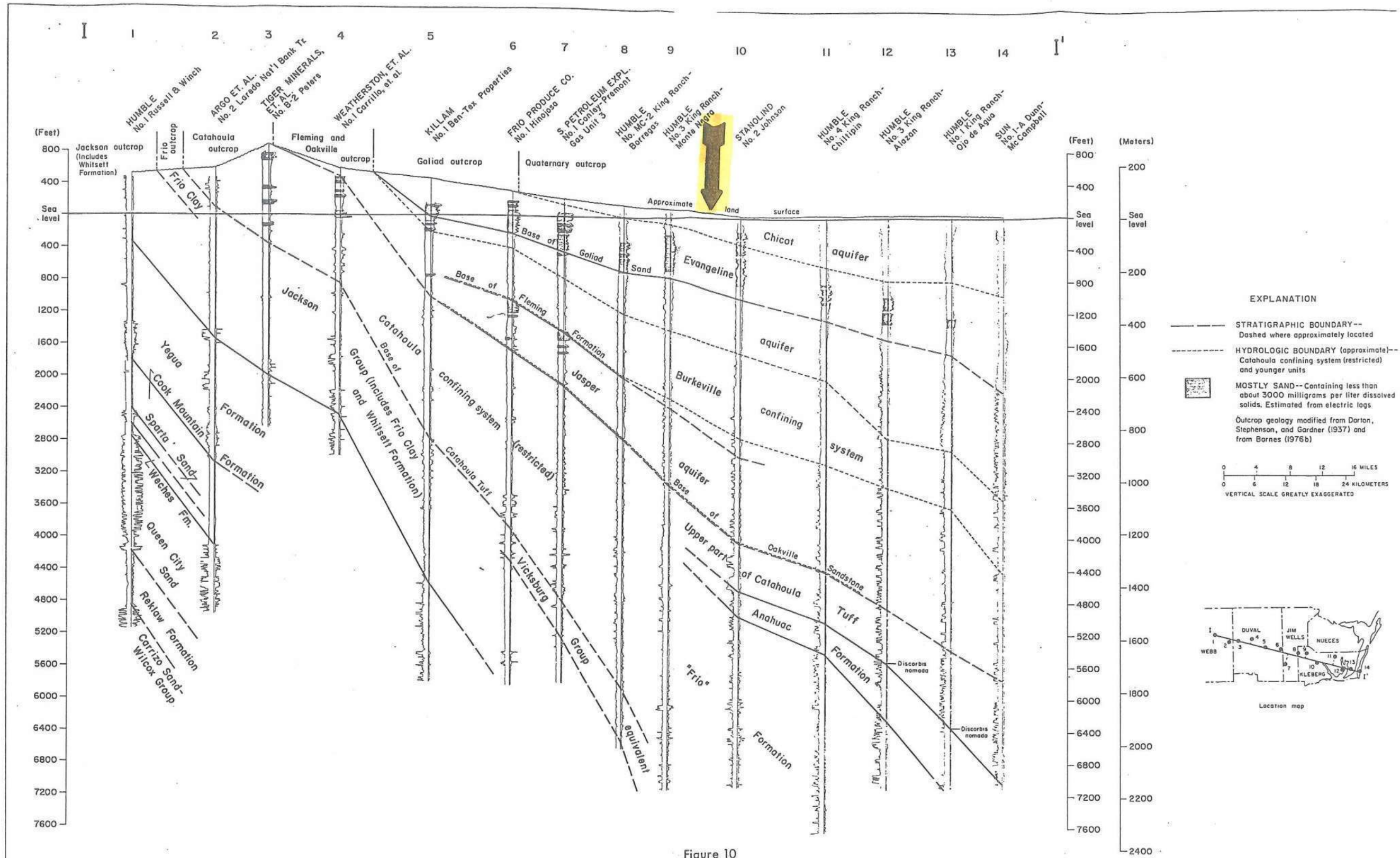
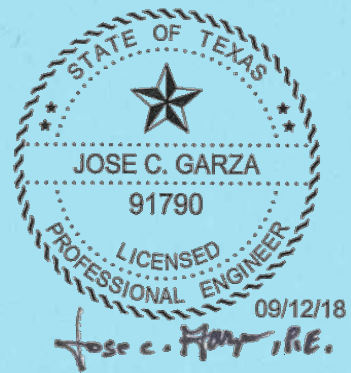


Figure 10  
 Stratigraphic and Hydrogeologic Section I-I'

APPENDIX D  
CALCULATIONS OF THE DILUTION ATTENUATION FACTOR (DAF)





**CALCULATIONS OF THE DILUTION ATTENUATION FACTOR**

Example Calculation for the Interim Case with Alternative Liner

Result from MULTIMED model:

Chemical concentration at the point of compliance =  $0.2943 \times 10^{-4}$  mg/l  
 (see MULTIMED model output)

To find the resulting DAF, take the reciprocal:

$$\text{DAF} = 1 / 0.2943 \times 10^{-4} \text{ mg/l}$$

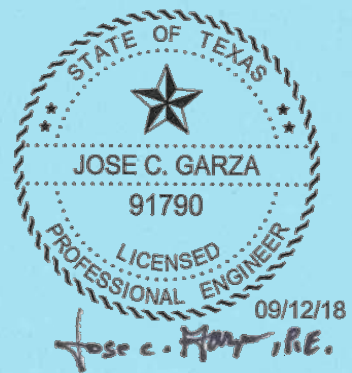
$$\text{DAF} = 33,979$$

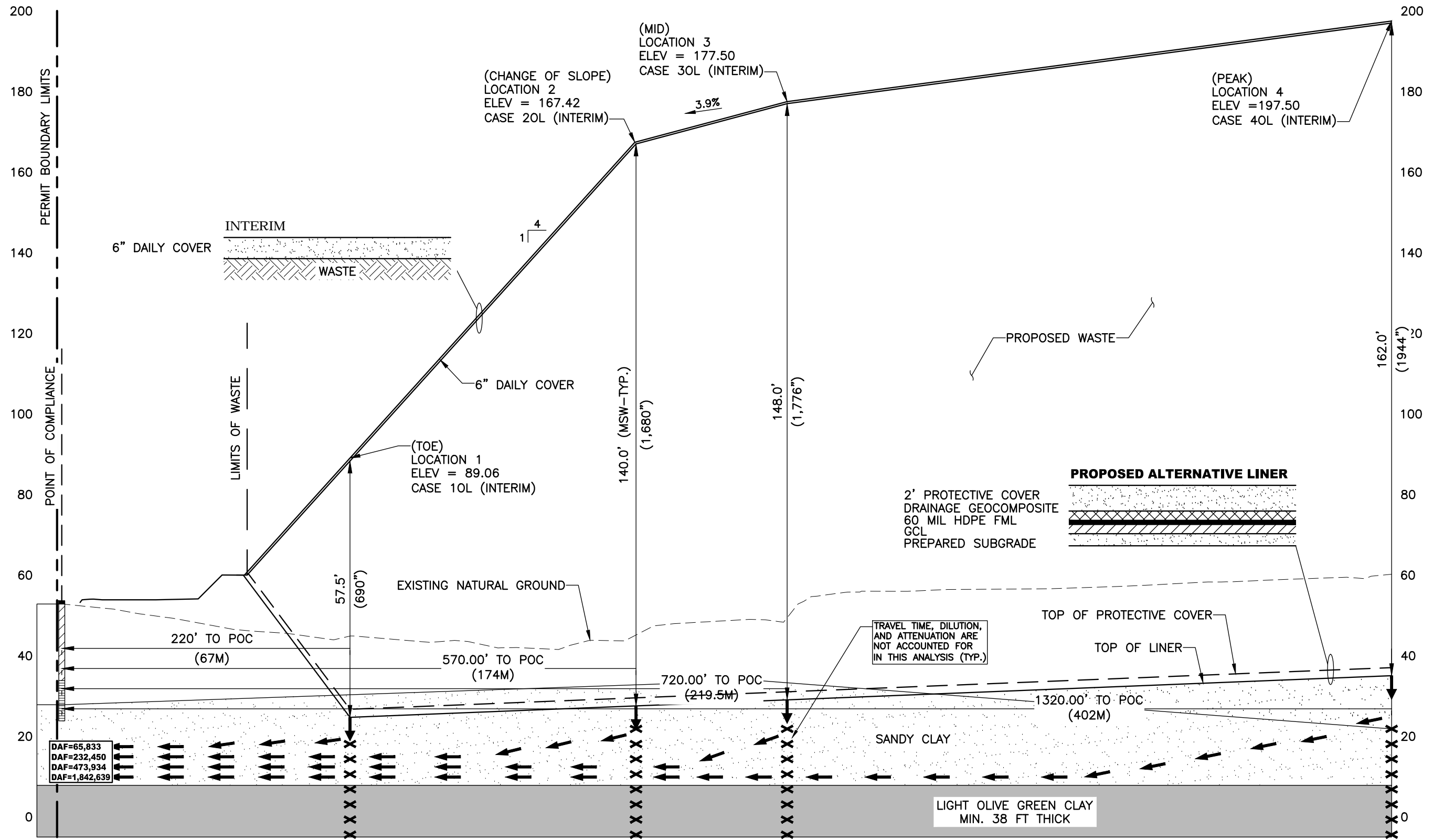
**Table 1**

Location	Interim Case DAF	Closed Case DAF
Alternative Liner Location 1	33,979	85,106
Alternative Liner Location 2	57,471	201,288
Alternative Liner Location 3	80,645	282,566
Alternative Liner Location 4	286,533	1,003,814

Location	Interim Case DAF	Closed Case DAF
Overliner Location 1	18,797	65,833
Overliner Location 2	77,640	232,450
Overliner Location 3	158,253	473,934
Overliner Location 4	615,385	1,842,639

APPENDIX D.1  
TYPICAL PROFILE-ALTERNATIVE LINER INTERIM LANDFILL DAF





**ALTERNATIVE LINER DEMONSTRATION – INTERIM LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE ALTERNATIVE LINER.
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

**MULTIMED INFORMATION**

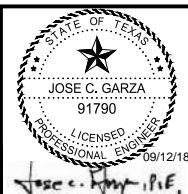
AVERAGE AQUIFER THICKNESS = 32.81FT (10M)  
 HYDRAULIC CONDUCTIVITY =  $4.12 \times 10^{-4}$  CM/SEC OR  
 130 M/YR  
 HYDRAULIC GRADIENT =  $i = 0.003125$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

SEP 11, 2018 2:49 PM TORRE01809 I:\16JOBS\16L0438\8514-CITY OF KINGSVILLE\8514-03\CAD-PART-III\8514-03-MULTIMED-SECTIONS.DWG

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Date	09/12/2018
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REVIEWED	JMR 09/12/2018

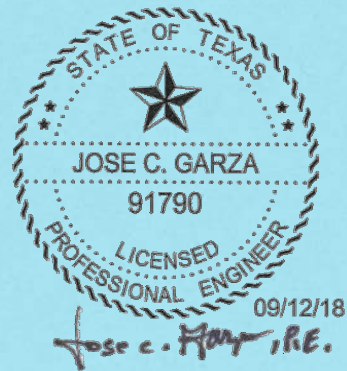
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**Hanson Professional Services Inc.**  
 4501 Gollihar Rd.  
 Corpus Christi, Texas 78411

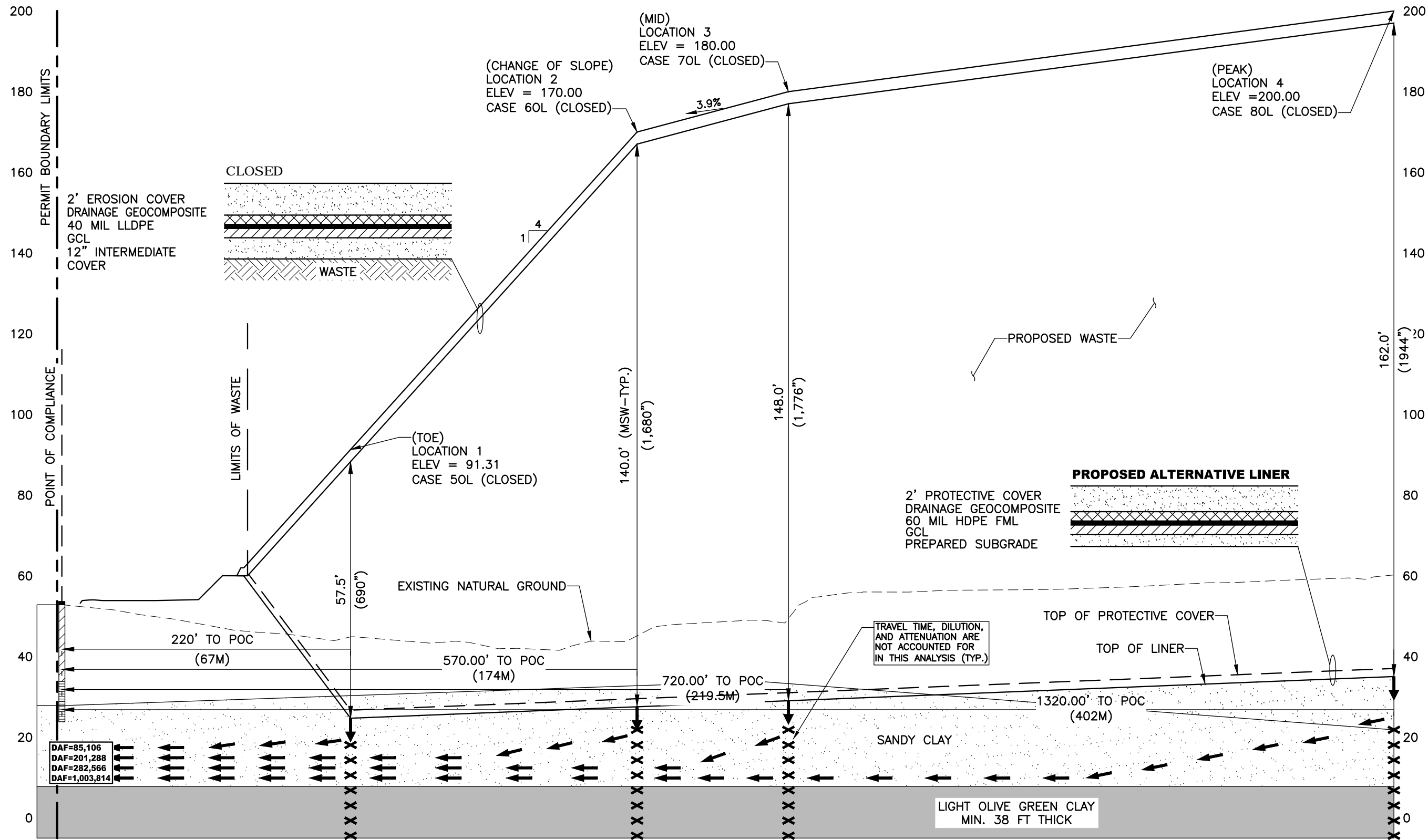
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PART III, ATTACHMENT 5, APPENDIX D  
 TYPICAL PROFILE-ALTERNATIVE LINER  
 INTERIM LANDFILL DAF  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:**  
**III.5-D.1**

APPENDIX D.2  
TYPICAL PROFILE-ALTERNATIVE LINER CLOSED LANDFILL DAF





**ALTERNATIVE LINER DEMONSTRATION – CLOSED LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE ALTERNATIVE LINER.
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

**MULTIMED INFORMATION**

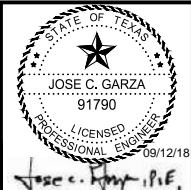
AVERAGE AQUIFER THICKNESS = 32.81FT (10M)  
 HYDRAULIC CONDUCTIVITY =  $4.12 \times 10^{-4}$  CM/SEC OR  
 130 M/YR  
 HYDRAULIC GRADIENT =  $i = 0.003125$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

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DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018



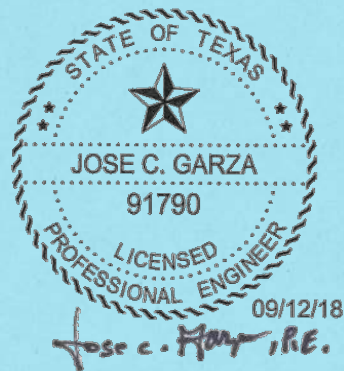
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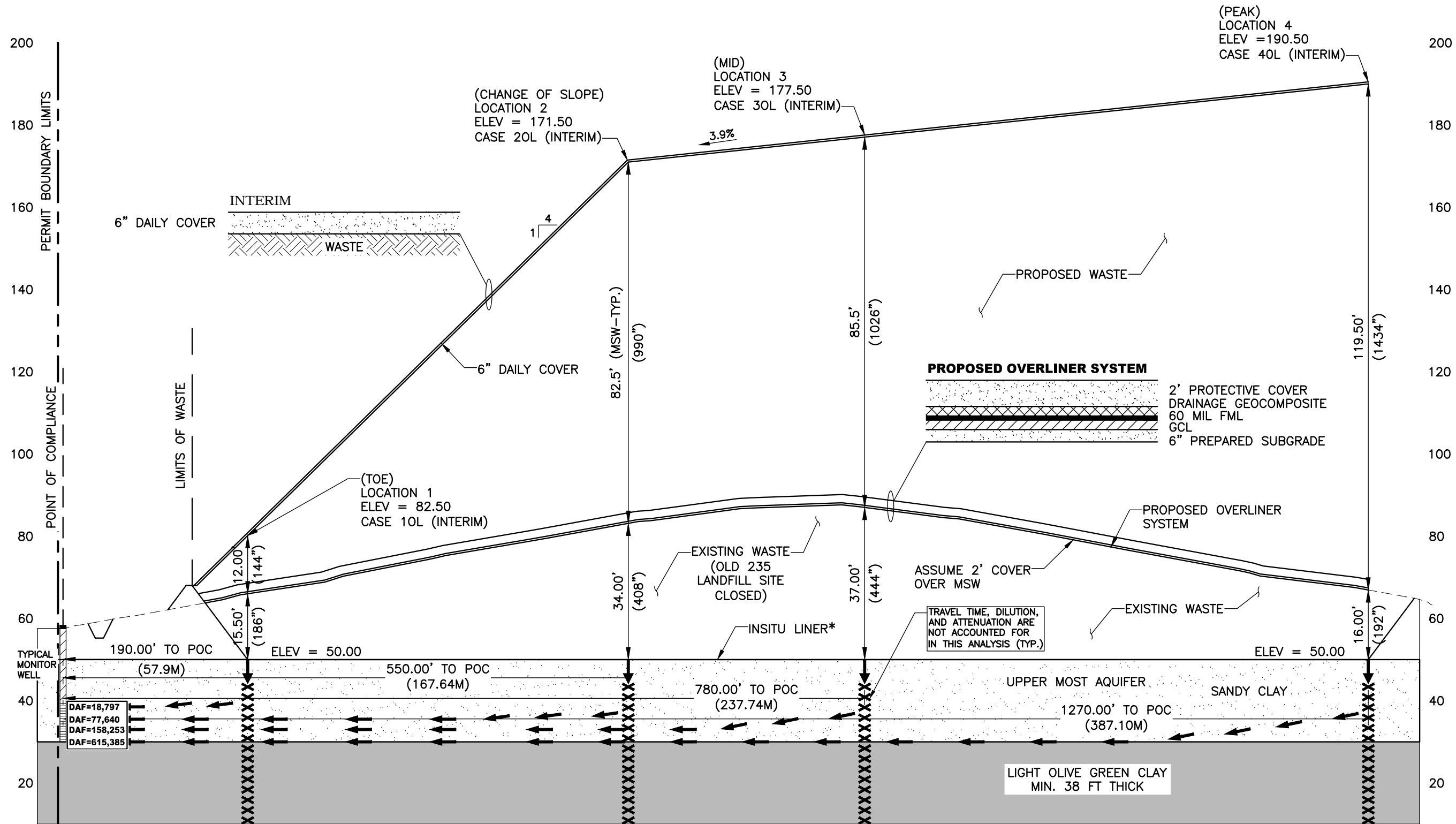
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PART III, ATTACHMENT 5, APPENDIX D  
 TYPICAL PROFILE-ALTERNATIVE LINER  
 CLOSED LANDFILL DAF  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

FIGURE:  
 III.5-D.2

APPENDIX D.3  
TYPICAL PROFILE-ALTERNATIVE LINER AND OVERLINER INTERIM  
LANDFILL DAF





**\*OVERLINER DEMONSTRATION - INTERIM LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE INSITU LINER (ASSUMED EQUAL TO PERCOLATION THROUGH OVERLINER).
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

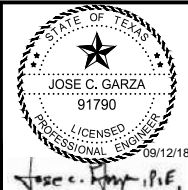
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AVERAGE AQUIFER THICKNESS	= 32.81FT (10M)
HYDRAULIC CONDUCTIVITY	= $4.12 \times 10^{-4}$ CM/SEC
HYDRAULIC GRADIENT	= $i = 0.002$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

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REVIEWED	JMR 09/12/2018

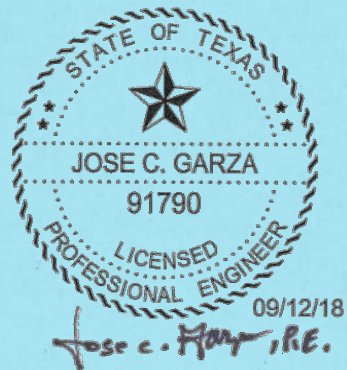
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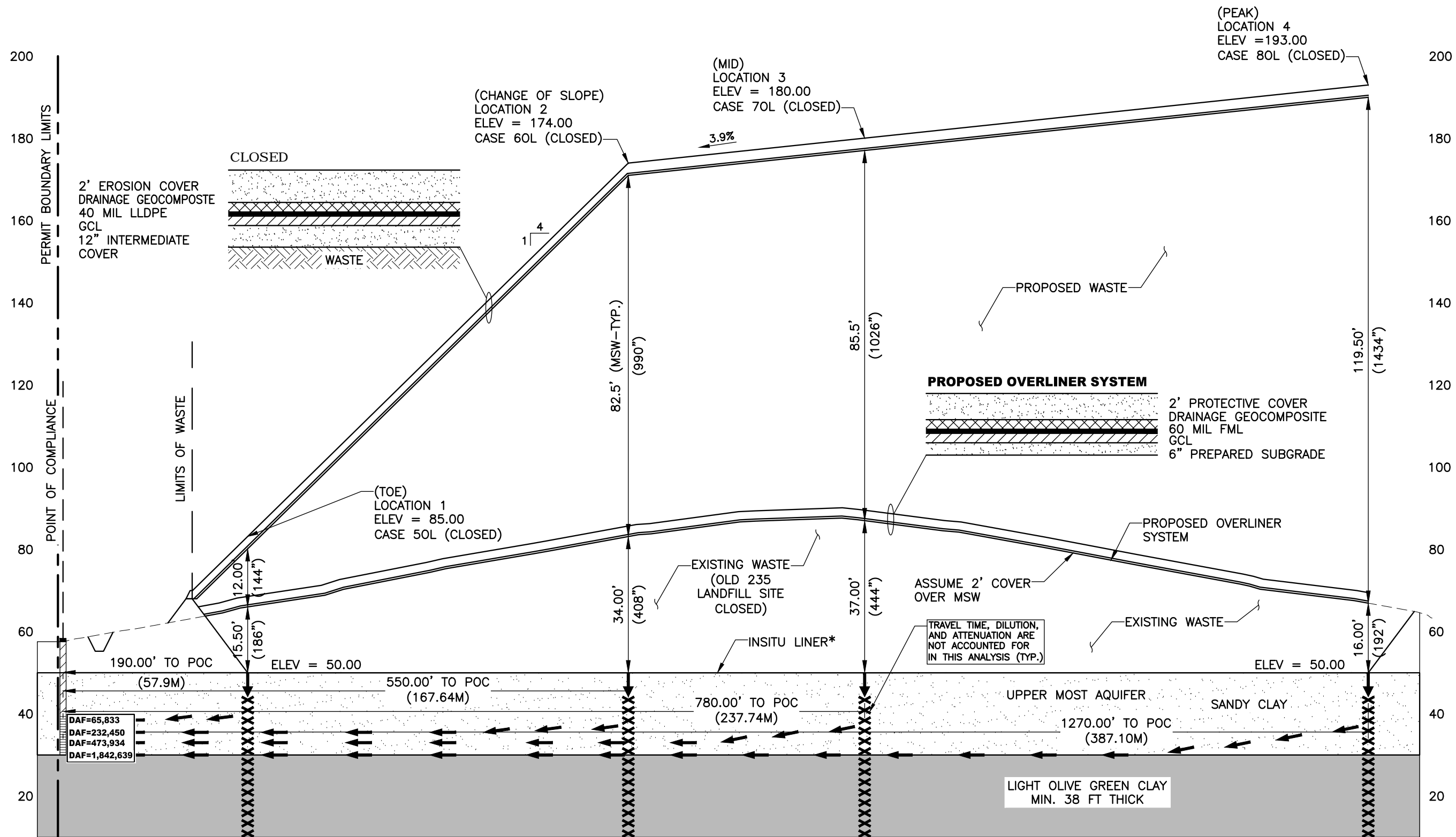
PART III, ATTACHMENT 5, APPENDIX D  
 TYPICAL PROFILE-ALTERNATIVE LINER  
 AND OVERLINER INTERIM LANDFILL DAF  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:**  
**III.5-D.3**

APPENDIX D.4  
TYPICAL PROFILE-ALTERNATIVE LINER AND OVERLINER CLOSED  
LANDFILL DAF







**\*OVERLINER DEMONSTRATION - CLOSED LANDFILL CONDITION**

1. USE HELP TO MODEL PERCOLATION THROUGH THE INSITU LINER (ASSUMED EQUAL TO PERCOLATION THROUGH OVERLINER).
2. USE MULTIMED TO CALCULATE THE DILUTION ATTENUATION FACTOR (DAF).

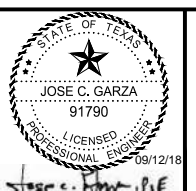
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HYDRAULIC CONDUCTIVITY =	$4.12 \times 10^{-4}$ CM/SEC
HYDRAULIC GRADIENT =	$i = 0.002$

**NOTES:**

1. EVANGELINE AQUIFER (500 FT BELOW GROUND SURFACE) (FRESH)
2. CHICOT AQUIFER (220 FT BELOW GROUND SURFACE)

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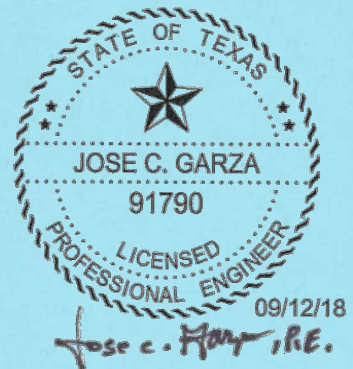
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PART III, ATTACHMENT 5, APPENDIX D  
 TYPICAL PROFILE-ALTERNATIVE LINER  
 AND OVERLINER CLOSED LANDFILL DAF  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:  
 III.5-D.4**

APPENDIX E  
LEACHATE DATA



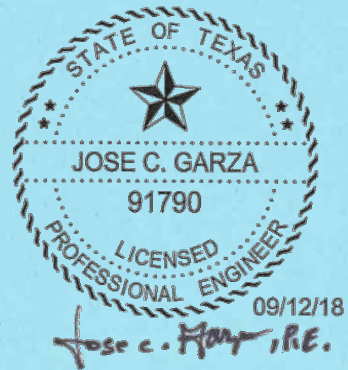
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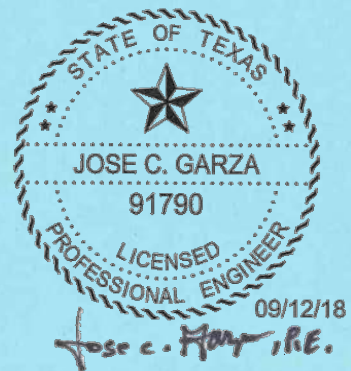
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An initial concentration ( $C_0$ ) equal to 1.0 mg/L was used for MULTIMED modeling, as detailed in Input Leachate Requirements (page 23) of the TCEQ's *Alternate Liner Design Handbook (1993)*.

**APPENDIX F**  
**MULTIMED MODEL OUTPUT**



APPENDIX F.1  
MULTIMED OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 1-  
LOCATION 1



CASE1  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
 --- -----

Case 1

Location 1  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN STD DEV	LIMITS MIN MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Reference temperature	C	CONSTANT	20.0 -999.	0.000E+00 100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Distribution coefficient	--	DERIVED	-999. -999.	0.000E+00 -999.
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00 -999.	0.000E+00 10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Molecular weight	g/M	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Mole fraction of solute	--	CONSTANT	0.000E+00 -999.	0.100E-08 1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00 -999.	0.100E-09 1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00 0.000E+00	0.000E+00 1.00
Not currently used		CONSTANT	-999. -999.	0.000E+00 1.00

Not currently used  
 CASE1  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

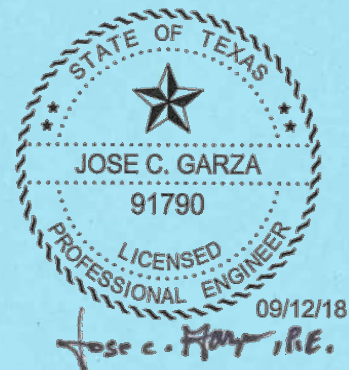
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.128E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	67.0	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.2943E-04

APPENDIX F.2  
MULTIMED OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 2-  
LOCATION 2





1 U. S. ENVIRONMENTAL PROTECTION AGENCY  
CASE2  
EXPOSURE ASSESSMENT  
MULTIMEDIA MODEL  
MULTIMED (Version 1.01, June 1991)

1 Run options  
-----

Case 2  
Location 2  
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
Run was DETERMIN  
Infiltration input by user  
Run was steady-state  
Reject runs if Y coordinate outside plume  
Reject runs if Z coordinate outside plume  
Gaussian source used in saturated zone model

1  
1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's Law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

Not currently used  
 CASE2  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

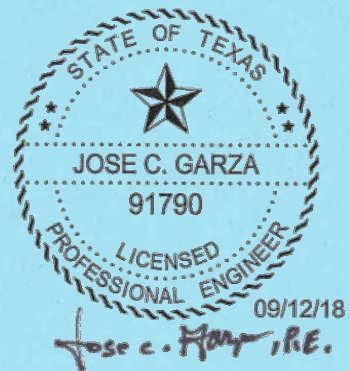
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.179E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	174.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1740E-04

APPENDIX F.3  
MULTIMED OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 3-  
LOCATION 3



U. S. ENVIRONMENTAL PROTECTION AGENCY  
CASE3  
EXPOSURE ASSESSMENT  
MULTIMEDIA MODEL  
MULTIMED (Version 1.01, June 1991)

1 Run options  
--- -----

Case 3

Location 3  
Chemical simulated is DEFAULT CHEMICAL

Option Chosen  
Run was Saturated zone model  
Infiltration input by user DETERMIN  
Run was steady-state  
Reject runs if Y coordinate outside plume  
Reject runs if Z coordinate outside plume  
Gaussian source used in saturated zone model

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm <sup>2</sup> /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

FOR PERMIT PURPOSES ONLY

Not currently used  
 CASE3  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

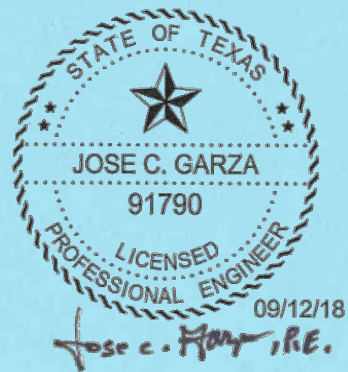
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.179E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	219.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1240E-04

APPENDIX F.4  
MULTIMED OUTPUT FOR ALTERNATIVE LINER INTERIM CASE 4-  
LOCATION 4



CASE4  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
 -----

Case 4

Location 4  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen                   Saturated zone model  
 Run was                         DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS	LIMITS
			MEAN   STD DEV	MIN           MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00   0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00   0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00   0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Reference temperature	C	CONSTANT	20.0 -999.	0.000E+00   100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Distribution coefficient	--	DERIVED	-999. -999.	0.000E+00   0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Air diffusion coefficient	cm <sup>2</sup> /s	CONSTANT	0.000E+00 -999.	0.000E+00   10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00 -999.	0.000E+00   100.
Molecular weight	g/M	CONSTANT	0.000E+00 -999.	0.000E+00   -999.
Mole fraction of solute	--	CONSTANT	0.000E+00 -999.	0.100E-08   1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00 -999.	0.000E+00   100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00 -999.	0.100E-09   1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00 0.000E+00	0.000E+00   1.00
Not currently used		CONSTANT	-999. -999.	0.000E+00   1.00

FOR PERMIT PURPOSES ONLY

Not currently used  
 CASE4  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.179E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

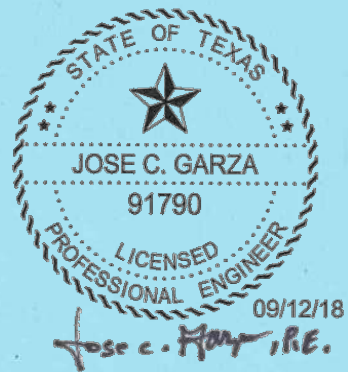
AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	402.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.3490E-05



**APPENDIX F.5**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 5-**  
**LOCATION 1**



U. S. ENVIRONMENTAL PROTECTION AGENCY  
 CASES

EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL

MULTIMED (Version 1.01, June 1991)

1 Run options  
 ---

Case 5

Location 1  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissoived phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	

Not currently used

CASE5

CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

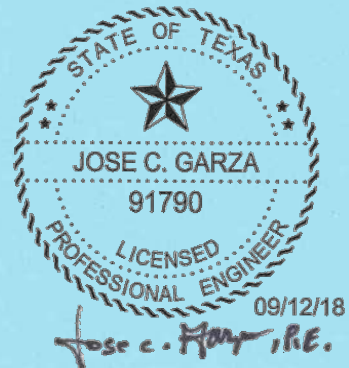
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	67.0	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1175E-04

**APPENDIX F.6**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 6-**  
**LOCATION 2**



CASE6  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
 ---

Case 6

Location 2  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	1/m-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	1/m-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	

Not currently used  
 CASE6  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

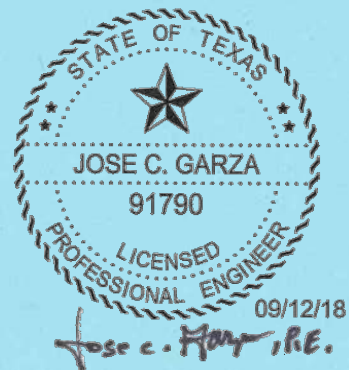
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	174.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.4968E-05

APPENDIX F.7  
MULTIMED OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 7-  
LOCATION 3



CASE7  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL

MULTIMED (Version 1.01, June 1991)

1 Run options  
 --- -----

Case 7

Location 3  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00



Not currently used  
 CASE7  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

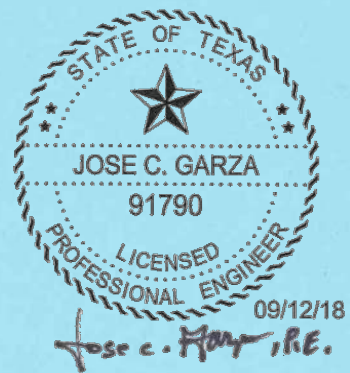
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS		
			MEAN	STD DEV	MIN	MAX		
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11		
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.		
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.		
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11		
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.		
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.		
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00		

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS		
			MEAN	STD DEV	MIN	MAX		
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.		
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990		
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00		
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06		
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06		
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09		
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.		
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09		
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09		
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.		
pH	--	CONSTANT	7.20	-999.	0.300	14.0		
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00		
Well distance from site	m	CONSTANT	219.	-999.	1.00	-999.		
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.		
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00		

CONCENTRATION AFTER SATURATED ZONE MODEL 0.3539E-05

APPENDIX F.8  
MULTIMED OUTPUT FOR ALTERNATIVE LINER CLOSED CASE 8-  
LOCATION 4



CASE8  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
 --- -----

Case 8

Location 4  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN STD DEV	LIMITS MIN MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Acid catalyzed hydrolysis rate	l/m-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Base catalyzed hydrolysis rate	l/m-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Reference temperature	C	CONSTANT	20.0 -999.	0.000E+00 100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Distribution coefficient	--	DERIVED	-999. -999.	0.000E+00 -999.
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00 -999.	0.000E+00 10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Molecular weight	g/M	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Mole fraction of solute	--	CONSTANT	0.000E+00 -999.	0.100E-08 1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00 -999.	0.100E-09 1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00 0.000E+00	0.000E+00 1.00
Not currently used		CONSTANT	-999. -999.	0.000E+00 1.00

Not currently used      CASE8      CONSTANT      -999.      -999.      0.000E+00      1.00

SOURCE SPECIFIC VARIABLES

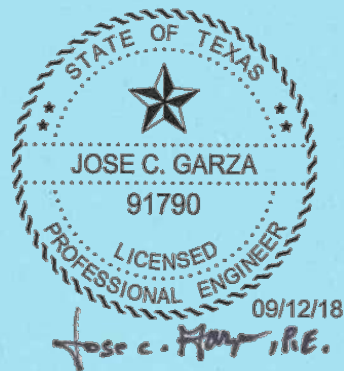
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.310E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	402.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.9962E-06

APPENDIX F.9  
MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER INTERIM  
CASE 10L-LOCATION 1



CASE10L  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
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CASE10L

Location 1  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm <sup>2</sup> /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	

Not currently used  
 CASE10L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

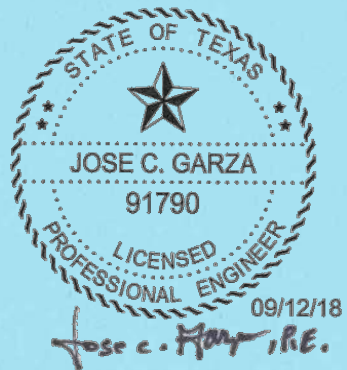
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.179E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	58.0	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.5320E-04

**APPENDIX F.10**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER INTERIM**  
**CASE 20L-LOCATION 2**





CASE20L  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
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CASE20L

Location 2  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN STD DEV	LIMITS MIN MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Reference temperature	C	CONSTANT	20.0 -999.	0.000E+00 100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Distribution coefficient	--	DERIVED	-999. -999.	0.000E+00 0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00 -999.	0.000E+00 10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Molecular weight	g/M	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Mole fraction of solute	--	CONSTANT	0.000E+00 -999.	0.100E-08 1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00 -999.	0.100E-09 1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00 0.000E+00	0.000E+00 1.00
Not currently used		CONSTANT	-999. -999.	0.000E+00 1.00

Not currently used  
 CASE20L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

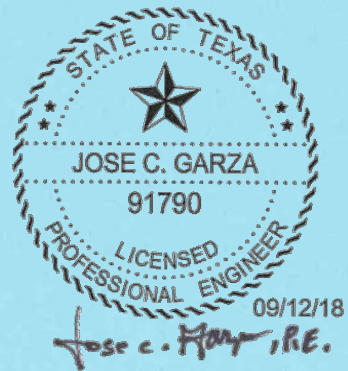
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.153E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	168.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1288E-04

APPENDIX F.11  
MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER INTERIM  
CASE 30L-LOCATION 3



CASE30L  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
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CASE30L

Location 3  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

Not currently used  
 CASE30L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

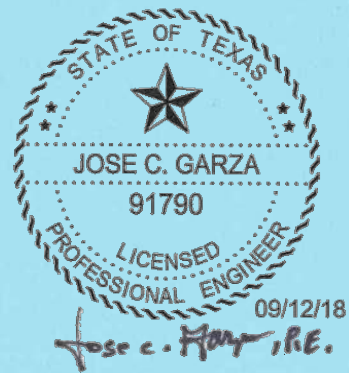
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.153E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	238.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.6319E-05

**APPENDIX F.12**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER INTERIM**  
**CASE 40L-LOCATION 4**



CASE40L  
 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
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CASE40L

Location 4  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	l/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	-999.	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	

Not currently used  
 CASE40L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.153E-06	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

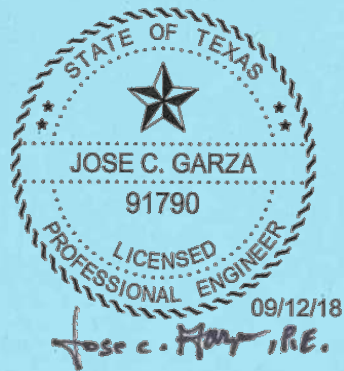
AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	387.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1625E-05



APPENDIX F.13  
MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER CLOSED  
CASE 50L-LOCATION 1



FOR PERMIT PURPOSES ONLY

1 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 CASE50L  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
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CASE50L

Location 1  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

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CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	-999.	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	

Not currently used  
 CASE50L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

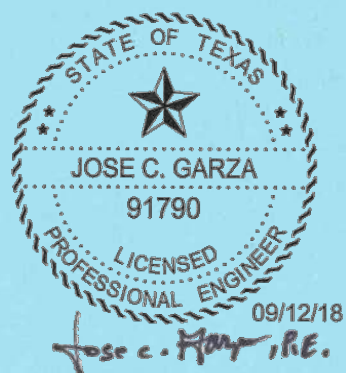
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	58.0	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.1519E-04

**APPENDIX F.14**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER CLOSED**  
**CASE 60L-LOCATION 2**



FOR PERMIT PURPOSES ONLY

U. S. ENVIRONMENTAL PROTECTION AGENCY  
 CASE60L

EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL

MULTIMED (Version 1.01, June 1991)

1 Run options  
 ---

CASE60L

Location 2  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1  
 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS	STD DEV	MIN	MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Air diffusion coefficient	cm <sup>2</sup> /s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00

Not currently used  
 CASE60L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

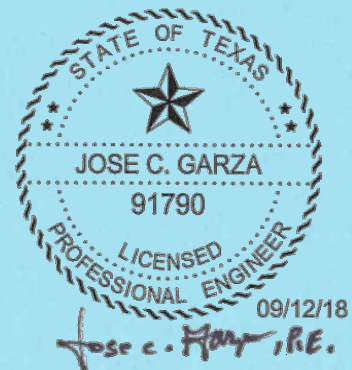
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS		
			MEAN	STD DEV	MIN	MAX		
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11		
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.		
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.		
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11		
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.		
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.		
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11		
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00		

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS		
			MEAN	STD DEV	MIN	MAX		
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.		
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990		
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00		
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06		
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06		
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09		
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.		
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09		
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09		
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.		
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.		
pH	--	CONSTANT	7.20	-999.	0.300	14.0		
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00		
Well distance from site	m	CONSTANT	168.	-999.	1.00	-999.		
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.		
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00		

CONCENTRATION AFTER SATURATED ZONE MODEL 0.4302E-05

**APPENDIX F.15**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER CLOSED**  
**CASE 70L-LOCATION 3**



CASE70L  
U. S. ENVIRONMENTAL PROTECTION AGENCY  
EXPOSURE ASSESSMENT  
MULTIMEDIA MODEL  
MULTIMED (Version 1.01, June 1991)

1 Run options  
--- -----

CASE70L

Location 3  
Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
Run was DETERMIN  
Infiltration input by user  
Run was steady-state  
Reject runs if Y coordinate outside plume  
Reject runs if Z coordinate outside plume  
Gaussian source used in saturated zone model

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1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Reference temperature	C	CONSTANT	20.0	-999.	0.000E+00	100.	
Normalized distribution coefficient	m1/g	CONSTANT	0.000E+00	-999.	0.000E+00	0.100E+11	
Distribution coefficient	--	DERIVED	-999.	-999.	0.000E+00	-999.	
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00	-999.	0.000E+00	10.0	
Reference temperature for air diffusion	C	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Molecular weight	g/M	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Mole fraction of solute	--	CONSTANT	0.000E+00	-999.	0.100E-08	1.00	
Vapor pressure of solute	mm Hg	CONSTANT	0.000E+00	-999.	0.000E+00	100.	
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00	-999.	0.100E-09	1.00	
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00	0.000E+00	0.000E+00	1.00	
Not currently used		CONSTANT	-999.	-999.	0.000E+00	1.00	



Not currently used  
 CASE70L  
 CONSTANT -999. -999. 0.000E+00 1.00

SOURCE SPECIFIC VARIABLES

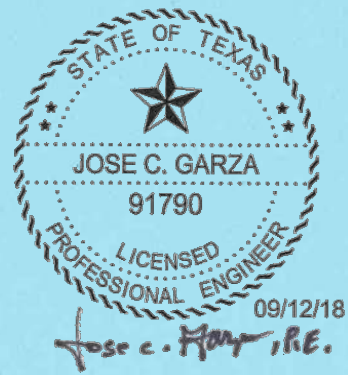
VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11	
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.	
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.	
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11	
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.	
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.	
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11	
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00	

AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS			LIMITS	
			MEAN	STD DEV	MIN	MAX	
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.	
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990	
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00	
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06	
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06	
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09	
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.	
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09	
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09	
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.	
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.	
pH	--	CONSTANT	7.20	-999.	0.300	14.0	
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00	
Well distance from site	m	CONSTANT	238.	-999.	1.00	-999.	
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.	
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00	

CONCENTRATION AFTER SATURATED ZONE MODEL 0.2110E-05

**APPENDIX F.16**  
**MULTIMED OUTPUT FOR ALTERNATIVE LINER/OVERLINER CLOSED**  
**CASE 80L-LOCATION 4**



1 U. S. ENVIRONMENTAL PROTECTION AGENCY  
 CASE80L  
 EXPOSURE ASSESSMENT  
 MULTIMEDIA MODEL  
 MULTIMED (Version 1.01, June 1991)

1 Run options  
 ---

CASE80L

Location 4  
 Chemical simulated is DEFAULT CHEMICAL

Option Chosen Saturated zone model  
 Run was DETERMIN  
 Infiltration input by user  
 Run was steady-state  
 Reject runs if Y coordinate outside plume  
 Reject runs if Z coordinate outside plume  
 Gaussian source used in saturated zone model

1 1

CHEMICAL SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS MEAN STD DEV	LIMITS MIN MAX
Solid phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Dissolved phase decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Overall chemical decay coefficient	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 0.100E+11
Acid catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Neutral hydrolysis rate constant	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Base catalyzed hydrolysis rate	1/M-yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Reference temperature	C	CONSTANT	20.0 -999.	0.000E+00 100.
Normalized distribution coefficient	ml/g	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Distribution coefficient	--	DERIVED	-999. -999.	0.000E+00 0.100E+11
Biodegradation coefficient (sat. zone)	1/yr	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Air diffusion coefficient	cm2/s	CONSTANT	0.000E+00 -999.	0.000E+00 10.0
Reference temperature for air diffusion	C	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Molecular weight	g/M	CONSTANT	0.000E+00 -999.	0.000E+00 -999.
Mole fraction of solute	--	CONSTANT	0.000E+00 -999.	0.100E-08 1.00
Vapor pressure of solute	mm HG	CONSTANT	0.000E+00 -999.	0.000E+00 100.
Henry's law constant	atm-m <sup>3</sup> /M	CONSTANT	0.000E+00 -999.	0.100E-09 1.00
Overall 1st order decay sat. zone	1/yr	DERIVED	0.000E+00 0.000E+00	0.000E+00 1.00
Not currently used		CONSTANT	-999. -999.	0.000E+00 1.00

CASE80L  
CONSTANT -999. -999. 0.000E+00 1.00

Not currently used

1

SOURCE SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Infiltration rate	m/yr	CONSTANT	0.511E-07	-999.	0.100E-09	0.100E+11
Area of waste disposal unit	m^2	CONSTANT	0.486E+06	-999.	0.100E-01	-999.
Duration of pulse	yr	CONSTANT	-999.	-999.	0.100E-08	-999.
Spread of contaminant source	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Recharge rate	m/yr	CONSTANT	0.368E-01	-999.	0.000E+00	0.100E+11
Source decay constant	1/yr	CONSTANT	0.000E+00	-999.	0.000E+00	-999.
Initial concentration at landfill	mg/l	CONSTANT	1.00	-999.	0.000E+00	-999.
Length scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Width scale of facility	m	DERIVED	-999.	-999.	0.100E-08	0.100E+11
Near field dilution		DERIVED	1.00	0.000E+00	0.000E+00	1.00

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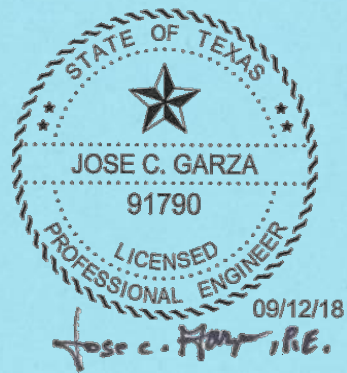
AQUIFER SPECIFIC VARIABLES

VARIABLE NAME	UNITS	DISTRIBUTION	PARAMETERS		LIMITS	
			MEAN	STD DEV	MIN	MAX
Particle diameter	cm	CONSTANT	0.381E-01	-999.	0.100E-08	100.
Aquifer porosity	--	CONSTANT	0.430	-999.	0.100E-08	0.990
Bulk density	g/cc	CONSTANT	1.65	-999.	0.100E-01	5.00
Aquifer thickness	m	CONSTANT	10.0	-999.	0.100E-08	0.100E+06
Source thickness (mixing zone depth)	m	DERIVED	-999.	-999.	0.100E-08	0.100E+06
Conductivity (hydraulic)	m/yr	CONSTANT	130.	-999.	0.100E-06	0.100E+09
Gradient (hydraulic)		CONSTANT	0.200E-02	-999.	0.100E-07	-999.
Groundwater seepage velocity	m/yr	DERIVED	-999.	-999.	0.100E-09	0.100E+09
Retardation coefficient	--	DERIVED	-999.	-999.	1.00	0.100E+09
Longitudinal dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Transverse dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Vertical dispersivity	m	FUNCTION OF X	-999.	-999.	-999.	-999.
Temperature of aquifer	C	CONSTANT	21.0	-999.	0.000E+00	100.
pH	--	CONSTANT	7.20	-999.	0.300	14.0
Organic carbon content (fraction)		CONSTANT	0.300E-02	-999.	0.100E-05	1.00
Well distance from site	m	CONSTANT	387.	-999.	1.00	-999.
Angle off center	degree	CONSTANT	0.000E+00	-999.	0.000E+00	360.
Well vertical distance	m	CONSTANT	0.000E+00	-999.	0.000E+00	1.00

CONCENTRATION AFTER SATURATED ZONE MODEL 0.5427E-06

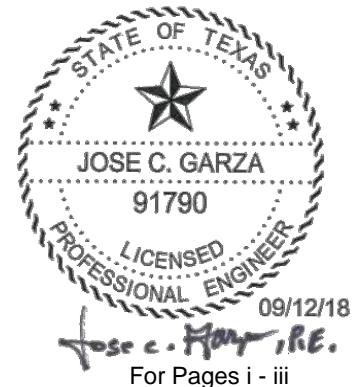
**CITY OF KINGSVILLE LANDFILL**  
**PART III**  
**ATTACHMENT 6**  
**FACILITY SURFACE WATER**  
**DRAINAGE REPORT**

**ATTACHMENT 6**  
**FACILITY SURFACE WATER DRAINAGE REPORT**



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3. PROPOSED SURFACE WATER MANAGEMENT PRACTICES
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5. SITE POST-DEVELOPMENT CONDITIONS
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  - 5.2 Soil Groups and Final Drainage Areas
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  - 5.6 City of Kingsville MSW 235-B Permit
  - 5.7 Perimeter Channels, Collector Channels, and Chutes
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  - 5.10 Diversion Berms or Swales
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### **APPENDIX 6A**

#### **SITE PRE-DEVELOPMENT CONDITIONS**

- 6A.1 25 Year Pre-Development Conditions Summary Table
- 6A.2 Site Pre-Development Conditions-Existing Permitted Conditions
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## **ATTACHMENT 6**

### **1.0 INTRODUCTION**

The City of Kingsville Landfill (Kingsville Landfill) is located in Kleberg County, Texas, at the northeast corner of the intersection of Farm to Market Road 2619 and County Road 2130. The northern boundary of the property is approximately 2,811 feet from FM 1717, while the eastern boundary is approximately 1,300 feet from N. County Road 1070 (See Part I, Attachment 2, Figure I.1 - Site Location Map).

The Kingsville Landfill has been in existence since February 1977 and is intended to provide waste disposal for residences and businesses in Kleberg County and surrounding Texas counties. The nearest community is the City of Kingsville, whose city limits are approximately 1.45 miles from the northeast corner of the landfill boundary. The facility has undergone two permit amendments to date allowing it to extend its initial permit boundaries, and increase the permitted maximum elevation (Refer to Part I, Attachment 1, Section 1.2 – Permit History).

The existing Kingsville Landfill includes a scale house, an office building, a maintenance shop, enclosed within a perimeter fence. These facilities will continue to be operational for the life of the landfill. No new buildings or infrastructure improvements will be constructed as part of the proposed permit amendment.

This Facility Surface Water Drainage Report (FSWDR) for the City of Kingsville Landfill TCEQ Permit MSW 235-C has been designed to collect, route, retain, and detain stormwater runoff from the facility. The Plan for the landfill contains design features that follow best management practices that meet or exceed the regulations applicable to stormwater management outlined in Title 30 of the Texas Administrative Code (30 TAC), Section 330, Municipal Solid Waste as follows;

Rule §330.63 Contents of Part III of the Application

*(c) Facility surface water drainage report. The owner or operator of a municipal solid waste (MSW) facility shall include a statement that the facility design complies with the requirements of §330.303 of this title (relating to Surface Water Drainage for Municipal Solid Waste Facilities). Additionally, applications for landfill and compost units shall include a surface water drainage report to satisfy the requirements of Subchapter G of this chapter (relating to Surface Water Drainage)...*

Rule §330.303 Surface Water Drainage for Municipal Solid Waste Facilities

*(a) A facility must be constructed, maintained, and operated to manage run-on and runoff during the peak discharge of a 25-year rainfall event and must prevent the off-site discharge of waste and feedstock material, including, but not limited to, in-process and/or processed materials.*

*(b) Surface water drainage in and around a facility shall be controlled to minimize surface water running onto, into, and off treatment area.*

Rule §330.305 Additional Surface Water Drainage Requirements for Landfills

*(a) Existing or permitted drainage patterns must not be adversely altered.*

*(b) The owner or operator shall design, construct, and maintain a run-on control system capable of preventing flow onto the active portion of the landfill during peak discharge from at least a 25-year rainfall event.*

*(c) The owner or operator shall design, construct, and maintain a runoff management system from the active portion of the landfill to collect and control at least the water volume resulting from a 24-hour, 25-year storm.*

*(d) The landfill design must provide effective erosional stability on top dome surfaces and external embankment side slopes during all phases of landfill operation, closure, and post-closure care in accordance with the following.*

*(e) Dikes, embankments, drainage structures, or diversion channels sized and graded to handle the design runoff must be provided. The slopes of the sides and toe will be graded in such a manner as to minimize the potential for erosion. The surface water protection and erosion control practices must maintain low non-erodible velocities, minimize soil erosion losses below permissible levels, and provide long-term, low maintenance geotechnical stability to the final cover.*

Rule §330.307 Flood Protection for Landfills

*(a) The facility shall be protected from flooding by suitable levees constructed to provide protection from a 100-year frequency flood and in accordance with the rules of the commission relating to levee improvement districts and approval of plans for reclamation projects or the rules of the county or city having jurisdiction under Texas Water Code, §16.236, as implemented by Chapter 301, Subchapter C of this title (relating to Approval of Levees and Other Improvements).*

*(b) Flood protection levees must be designed and constructed to prevent the washout of solid waste from the facility.*

The property boundary is 196.88 acres, the proposed updated Permit boundary is 176.33 acres, and the proposed waste footprint is 121.30 acres.

The pre-development calculations represent conditions at the site prior to any landfill development. The post-developed condition calculations represent conditions at the site after the landfill has been closed, final cover has been placed, and all components of the designed drainage system have been established. The existing City of Kingsville Landfill TCEQ Permit MSW 235-B has been referenced and utilized to evaluate the site pre-development conditions and the site post-development conditions in Appendices 6A and 6B, respectively.

Stormwater modeling has been completed with the software program HydroCAD. HydroCAD is a computer aided design program used to model hydrology and hydraulics of stormwater using either TR-20 or TR-55 procedures developed by the Soil Conservation Service (now the Natural Resource Conservation Service). HydroCAD was selected for the modeling software due to the large number of drainage areas and stormwater control devices at the landfill facility.

## **2.0 EXISTING SURFACE WATER DRAINAGE**

The City of Kingsville Landfill TCEQ Permit MSW 235-C (existing City of Kingsville Landfill TCEQ Permit MSW 235-B) is located on uplands south of Santa Gertrudis Creek. The overall property consists of gently undulating grasslands with limited forest cover. The property generally slopes to the northeast with no major topographic features. The nearest 100-year floodplain is located to the northeast of the site along Santa Gertrudis Creek. The existing Kingsville Landfill is not located within the 100-year floodplain as designated by the Federal Emergency Management Agency (FEMA) Firm Community Panel Numbers 48273C03205E and 48273C0325E included in Appendix 6B.17. Surrounding land use is predominantly agricultural.

## **3.0 PROPOSED SURFACE WATER MANAGEMENT SYSTEM**

The proposed surface water management system will utilize stormwater best management practices (BMPs). The landfill will be developed as an above ground hill and designed to allow stormwater runoff to be collected in diversion berms or swales located near the upper grade break and on the landfill slopes. Stormwater will then be conveyed to let-down structures or chutes down the side slopes to the perimeter channel system and into either a retention pond or detention pond. The perimeter channels will be constructed prior to placing fill above ground in each adjacent landfill sector. The

perimeter channels will be vegetated. Erosion protection will be provided at critical discharge locations where velocities are five feet per second (5 ft./sec.) or greater such as chutes or culvert discharges. These areas will be lined with concrete articulated block or flexible revetment system. Energy dissipaters will be required downstream of the chutes within the final cover area where flow enters unlined channels.

During landfilling operations, stormwater controls will be implemented to minimize run-on from flowing into the active portion of the site. Contaminated runoff from the working face will be contained with stormwater controls as well. This is shown in Appendix 6B.15.14 Working Face Containment and Diversion Berms.

The SWPPP has been prepared according to the requirements of the *Texas Commission on Environmental Quality (TCEQ) Permit Number TXR050000 – General Permit to Discharge Under the Texas Pollutant Discharge Elimination System (TPDES) – Multi-Sector General Permit (MSGP)*, effective on August 14, 2016. The MSGP classifies industrial activities by Sectors containing various Standard Industrial Classification (SIC) Codes. The City of Kingsville Landfill falls under Sector L: Landfills and Land Application Sites under Activity Code LF – Landfills, Land Application Sites, and Open Dumps that Receive or Have Previously Received Industrial Waste under subtitle C of RCRA and including those that are subject to regulation under subtitle D of RCRA. Stormwater discharges at the facility were previously authorized by the submittal of a Notice of Intent (NOI) filed on November 26, 2001 and renewed on October 10, 2006 and November 3, 2011. Currently, discharges are authorized by an NOI submitted in November 2016. A copy of the current NOI and the MSGP are included in Appendix A. Discharges from the facility are not received by a Municipal Separate Storm Sewer System (MS4). Eventually stormwater discharges from outfalls on the west side of the facility flow into Santa Gertrudis Creek, then San Fernando Creek (TCEQ Classified Segment 2492A), and then Baffin Bay/Alazan Bay/Cayo del Grulla/Laguna Salada (TCEQ Classified Segment 2492A). Eventually stormwater discharges from outfalls on the south side of the facility flow into Baffin Bay/Alazan Bay/Cayo del Grulla/Laguna Salada (TCEQ Classified Segment 2492A).

The facility has been designed to prevent discharge of pollutants into the waters of the State or waters of the United States, as defined by the Texas Water Code and the Federal Clean Water Act.

All onsite surface drainage features are designed to collect and route stormwater through diversion berms, chutes, perimeter channels, and into three storage ponds. The three storage ponds are Pond A, Pond B, and Pond C. Pond A and Pond C are retention ponds and Pond B is a detention pond. The only stormwater discharge from the site will be at

Pond B via two drainage culverts. This is further discussed in Section 5.0 Site Post-Development Conditions.

#### **4.0 SITE PRE-DEVELOPMENT CONDITIONS**

The pre-development drainage characteristics of the landfill site are described in Appendix 6A-Site Pre-Development conditions. A summary of the pre-development conditions is summarized in Appendix 6A.1, 25 Year Pre-Development Conditions Summary Table. Pre-development drainage information from the City of Kingsville Landfill Permit Amendment 235-B, Attachment 6, Appendix 6A Pre-Development Conditions (Table of Contents and Pages 1-32) contained in Appendix 6A.2.1, Pre-Development Drainage Map Solid Waste Landfill Permit 235-B Amendment Figure 1 contained in Appendix 6A.2.2, and Pre-Development Slope Map Solid Waste Landfill Permit 235-B Amendment Figure A-2 contained in Appendix 6A.2.3 were all used to develop the summary table in Appendix 6A.1.

The City of Kingsville Landfill Permit Amendment 235-B illustrates that Watershed A contains drainage areas PA1, PA2, and PA3; Watershed B contains drainage areas PB1, PB2, and PB3; and Watershed C contains areas PC1, PC2, and PC3 for existing permitted conditions. A HydroCad model was developed to simulate the results from the pre-development drainage conditions using the same data. Results using HydroCAD were similar. HydroCAD results are shown in Appendix 6A.2.4 (HydroCAD Model Pre-Development Conditions 25 Year Existing Permitted Conditions). In addition, a separate HydroCAD model was developed to include a proposed updated boundary as shown in Appendix 6A.2.7 (Pre-Development Drainage Map Solid Waste Landfill Permit 235-B Amendment Figure A-1 (Updated Permitted Conditions)). The proposed updated permit boundary introduces drainage area PB4 located near the east boundary of the permit boundary. HydroCAD results are shown in Appendix 6A.2.5 (HydroCAD Model Pre-Development Conditions 25 Year Updated Permitted Conditions).

Results contained in the Appendix 6A.1 summary table illustrate that the combined total for the 25 year pre-development condition at the northwest corner of the landfill site adjacent to F.M. 2619 in the roadside ditch is approximately 49.3 cubic feet per second (cfs) to 51.1 cfs for both the existing permitted conditions and proposed updated conditions. The only stormwater discharge from the permit boundary will be at this northwest location (Pond B) via two (2) 21" x 128' reinforced concrete pipe (RCP) culverts with a discharge of 33.7 cfs for the 24 hr duration-25 year frequency storm and 42.5 cfs for the 24 hr duration-100 year frequency storm which is less than the combined 25 year pre-development flows as described in this section and in section 5.0 Site Post-Development Conditions.

## 5.0 SITE POST-DEVELOPMENT CONDITIONS

The post-development surface water management system design will include landfill final cover, a system of diversion berms or swales, let-down structures or chutes, perimeter channels, drainage culverts, two retention ponds and one detention pond. Onsite stormwater surface runoff from final cover will sheet flow to the diversion berms constructed at vertical intervals down the slope of the landfill. The diversion berms will convey runoff into the chutes that will convey the stormwater runoff down the slope of the landfill and into the perimeter channel drainage system. The chutes will be lined with concrete articulated block or flexible revetment system. Channels that exhibit velocities of 5 ft/sec or more will be also be lined with the same system. Collector channels along the landfill perimeter road at the northeast will collect landfill surface stormwater runoff not collected in the chutes. The stormwater will be conveyed to post inlets which will direct it across the road to Pond C via drainage culverts. In other areas to the east and south of the landfill, stormwater runoff not collected by the chutes will sheetflow into the adjacent perimeter channels which will in turn be directed into either Pond A or Pond C. At the north and northwest areas of the landfill, runoff not collected in the chutes will sheetflow into Pond B. The perimeter landfill channel system is divided into four segments; East, South, North, and West. The East channel system flows into Pond C, the South and West flow into Pond A, and the North flows into Pond C. Surface water from outside the boundary of the landfill will continue to be collected or directed as shown in Section 4.0 Site Pre-Development Conditions via existing roadside ditches along FM 2619 and C.R. 2130 that border the property. All surface stormwater runoff will be contained onsite with retention Ponds A and C with the exception of a discharge at Pond B. This discharge is less than the pre-development condition and post-development condition as shown in Appendices 6B.8.1 (Portion of Attachment 6 Groundwater and Surface Water Protection Plan (Pre-Development/Post Development Drainage Conditions and Design [Annotated]), 6B.8.2 (Portion of Appendix 6A-Pre-Development Conditions (Figure A-1 Pre-Development Drainage Map) [Annotated]), 6B.8.3 (Portion of Appendix 6B-Final Development Conditions (Figure B-1 Final Development Drainage Map) [Annotated]), and 6B.8.4 (Portion of Appendix 6C Detention Ponds and Discharge Culverts (25-Year Storm Strategy/Comparative Summary of Peak Flow) [Annotated]).

### 5.1 RAINFALL

Appendix 6B.1 USGS Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas-Depth of Precipitation for 25 Yr-24 Hr and 100 Yr-24 Hr [Annotated] was used to determine the rainfall depth at the site location. 8.7 inches and 11.5 inches was selected for the 25 Yr-24 Hr and 100 Yr-24 storms, respectively. These values were used for modeling purposes.

## 5.2 SOIL GROUPS AND FINAL DRAINAGE AREAS

Appendix 6B.2 contains Table 6B-1 Hydrologic Soils Groups for On-Site Soils (from NRCS, 2015) that was used to determine the hydrologic soil group. This Table indicates that the soil is predominantly a clay loam and sandy loam. It also lists the drainage area designations and areas in acres. The total onsite drainage areas are approximately 164.60 acres.

## 5.3 Time of Concentration (Tc) Values for Landfill Top/Slope Drainage Areas

Appendix 6B.3 illustrates values for the time of concentration (tc) at the top and slope drainage areas of the landfill. A conservative value of tc=10 min was used at the slopes.

## 5.4 HYDROCAD MODEL

The computer model HydroCAD was used to develop discharge rates, volumes, and velocities for the 24-hour duration, 25-year and 100-year storm frequencies. All drainage elements were modeled using HydroCAD. The HydroCAD stormwater model used the following analysis methods:

Runoff Calculation Method:	SCS TR-20
Reach Routing Method:	Storage-Indication Routing Method (also known as Modified-Puls Method)
Pond Routing Method:	Storage-Indication Routing Method (also known as Modified-Puls Method)
Storm Distribution:	SCS Type III-24-hour storm
Unit Hydrograph:	SCS

The post-development models are in Appendices 6B.4 (HydroCad Model Post Development-25 Year) and Appendix 6B.5 (HydroCAD Model Post Development-100 Year). Cross sections are shown in the models for perimeter channels, collector channels, and chutes with average depths at peak storage. Peak elevations and storage are shown for Pond A, Pond B, and Pond C. A summary of the results are described below in sections 5.5 PONDS AND 5.7 PERIMETER CHANNELS, COLLECTOR CHANNELS, AND CHUTES. Typical drainage cross sections are shown in Appendix 6B.18. The analyses meet or exceed state and federal requirements for landfills.

## 5.5 PONDS

A HydroCAD pond results summary for the post-development 24-hour duration, 25-year & 100-year storm frequencies are in Appendices 6B.6 (HydroCAD Model



Post Development 25 Year Pond Summary) and 6B.7 (HydroCAD Model Post Development 100 Year Pond Summary). The post-development drainage plan for the 25 year and the 100 year are in Appendices 6B.6.1 (Post Development Drainage Plan-25 Year) and 6B.7.1 (Post Development Drainage Plan-100 Year). The landfill surface stormwater runoff will be routed to three ponds, Pond A, Pond B, and Pond C. Pond A is a retention pond (no discharge) located at the southwest corner, Pond B is a detention pond (33.70 cfs/42.46 cfs discharge for 25-Year/100-Year) located at the northwest corner, and Pond C is a retention pond (no discharge) located at the northeast corner of the permit boundary. All ponds will have adequate freeboard.

## **5.6 CITY OF KINGSVILLE MSW 235-B PERMIT**

Information from the Kingsville MSW 235-B Permit is contained in Appendix 6B.8 (Kingsville Landfill Permit Amendment 235-B). It was utilized to make the comparative analysis between pre-development conditions and post-development conditions. Modeling results demonstrate that the peak discharge flow for the 24-hour duration, 25-year frequency is 33.70 cfs via two (2) 21" x 128 ft. RCP culverts at Pond B after detention. The discharge is to an existing roadside ditch along FM 2619. Pre-development flow in this ditch is approximately 50 cfs. The post-development flow in this ditch will be 33.70 cfs for the 25-year storm and 42.46 cfs for the 100-year storm which is lower than the pre-development flows. The velocities will range between 7-9 ft/sec and therefore the receiving ditch will require erosion protection as discussed in previous sections.

## **5.7 PERIMETER CHANNELS, COLLECTOR CHANNELS, AND CHUTES**

A summary of perimeter channels, collector channels, and chutes are located in Appendices 6B.9 (Perimeter Channels, Collector Channels, and Chutes-25 Year Summary Table) and 6B.10 (Perimeter Channels, Collector Channels, and Chutes-100 Year Summary Table). The table illustrates the geometry as well as peak flows, velocities, slopes, hydraulic grade line elevations, and freeboard for all identified channels and chutes.

## **5.8 SOUTHERN DRAINAGE PLAN**

Appendix 6B.11 Figure 1 illustrates the overall southern drainage plan. Appendix 6B.11.1 Figure 2 is the Enlarged Southern Drainage Plan, and Appendix 6B.11.2 Figure 3 is the Cross Sections that illustrates the drainage channels relative to the existing waste locations. As shown the drainage channels will be articulated concrete block or flexible revetment placed over 60 mil HDPE geomembrane on prepared subgrade.

## **5.9 POST DEVELOPMENT CHUTES-HYDROCAD MODEL**

The drainage chutes have been modeled using HydroCAD as shown in Appendices 6B.12 (HydroCAD Model 25 Year Post Development Chutes) and 6B.13 (HydroCAD Model 100 Year Post Development Chutes). Chute cross sections are shown. The chutes will be no more than 2 ft. deep, 5 ft. wide, at 4:1 side slopes. All chutes will accommodate the 24-hour duration 25 year and 100 year storm frequencies with adequate freeboard. Appendix 6B.14 (Engineering Handbook Chute-Spillways-Chute Spillway Design) was used to design the SAF stilling basin criteria at the bottom of the chute. As discussed in previous sections, articulated concrete blocks or flexible revetment will be used for the chutes and high velocity areas. Included is manufacturer data and specifications for the block and geotextile. Chute details are located in Appendices 6B.14.1 and 6B.14.2 (Chute Details).

## **5.10 DIVERSION BERMS OR SWALES**

The diversions berms (swales) have been modeled using HydroCAD as shown in Appendix 6B.15 (HydroCAD Model Post Development Diversion Berms (Swales) NRCS & Rational Methods). The post-development plan for the diversion berms is shown in Appendix 6B.15.1 (Post Development Typical Diversion Berm Drainage Plan). This plan illustrates the proposed layout of the diversion berms. The largest drainage area was used to design a typical diversion berm and flow will be conveyed to a corresponding chute as shown on the drawing. The National Engineering Handbook (NEH) was used to determine the velocity versus slope for shallow concentrated flow using short grass criteria. This is shown in Appendix 6B.15.2 (National Engineering Handbook (NEH) Figure 15-4 Velocity Versus Slope for Shallow Concentrated Flow [Annotated]).

Swales were analyzed with a 0.5% slope and a 1.0% slope. The HydroCAD swales input data for 0.5% diversion berm slope (along the 25% slope of the landfill) is contained in Appendix 6B.15.3 (HydroCAD-Swales Input Data (Swale B1S-0.5% Slope)). The HydroCAD swales input data for 1.0% diversion berm slope (along the 25% slope of the landfill) is contained in Appendix 6B.15.4 (HydroCAD-Swales Input Data (Swale B1S-1.0% Slope)). The HydroCAD swales input data for the largest drainage area at the top of the landfill (B1T) is shown in Appendix 6B.15.5 (HydroCAD-Swales Input Data (Swale B1T-0.5% & 1.0% Slope)). The HydroCAD input data for drainage area B1S and B1T is in Appendices 6B.15.6 (HydroCAD-Swales Input Data (Drainage Area B1S)) and 6B.15.7 (HydroCAD-Swales Input Data (Drainage Area B1T)), respectively. Both the 0.5% slope and 1.0% diversion berm slopes were modeled with HydroCAD using the NRCS method and the Rational Method. The NRCS method is shown in Appendices 6B.15.8 (HydroCAD-Model 25 Year Post Development Diversion Berms (NRCS

Method) and 6B.15.11 (HydroCAD Model 100 Year Post Development Diversion Berms (NRCS Method). The Rational Method is shown in Appendices 6B.16.9 (HydroCAD-Model 25 Year Post Development Diversion Berms (Rational Method)) and 6B.15.12 (HydroCAD Model 100 Year Post Development Diversion Berms (Rational Method)). A summary of the results is in Appendix 6B.15.10 (Summary of 25 Year Intensity Flow Rates By Rational Method and NRCS Method for Swale Design) and Appendices 6B.15.11 (Summary of 100 Year Intensity Flow Rates by Rational Method and NRCS Method for Swale Design) and 6B.15.13 (Summary of 100 Year Intensity Flow Rates by Rational Method and NRCS Method for Swale Design). Cross sections are shown in the model. The analyses demonstrates that a typical diversion berm (swale) 3 ft. tall with 2:1 side slopes flowing at a 1% slope into the chute will suffice for both the 24-hr duration/25 year storm and 100 year storm frequencies with an acceptable velocity of approximately 3.7 ft./sec. (below 5 ft./sec) to prevent erosion and allowable freeboard of at least one foot (1 ft.).

#### **5.11 SOIL LOSS ESTIMATE FOR FINAL COVER**

The Revised Universal Soil Loss Equation (RUSLE) for top of slope (4%) and side slope (25%) interim cover and post closure is in Appendix 6B.16.1. The RUSLE is described as follows:

- A= computed soil loss (tons/acre/year)
- R= the rainfall and runoff factor (unitless)
- K= the soil erodibility factor (unitless)
- LS= the topographic factor (unitless)
- C= the cover and management factor (unitless)
- P= the support practice factor (unitless)

Detailed calculations and assumptions are provided in Appendix 6B.16.1 (Revised Universal Soil Loss Equation (RUSLE) for Top of Slope (4%) and Side Slope (25%) Interim Cover & Post Closure. The RUSLE calculation results show that the soil loss is 0.36 tons/acre/year for final conditions at top of slope and 2.39 tons/acre/year at the side slope and are both below the allowable 3 tons/acre/year. Also, the soil loss is 2.52 tons/acre/year for interim conditions at top of slope and 18.61 tons/acre/year at the side slope and are both below the allowable 50 tons/acre/year.

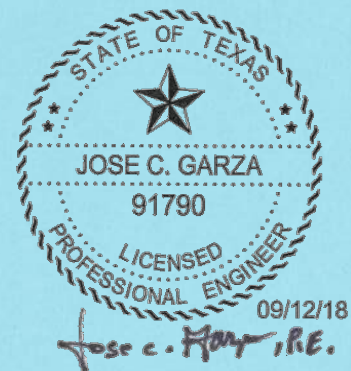
## 6.0 CONCLUSION

The following conclusions summarize the results of the Facility Surface Water Drainage Report:

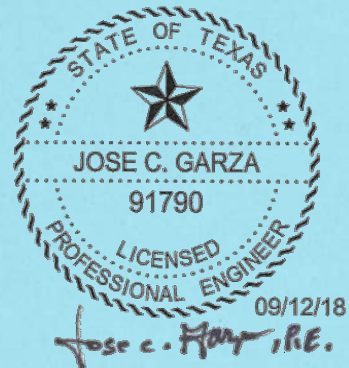
- The surface water management system for the proposed City of Kingsville Landfill TCEQ Permit MSW 235-C meets or exceeds the regulations applicable to stormwater management outlined in Title 30 of the Texas Administrative Code (30 TAC), Section 330, Municipal Solid Waste as outlined in section 1.0 INTRODUCTION.
- The surface water management plan system provides the required conveyance with a minimum of 1 foot of freeboard.
- It is designed to minimize surface water flow into the working face of the landfill and to minimize discharge pollutants.
- Erosion will be reduced using Best Management Practices. Temporary and permanent erosion control measures are provided to prevent and reduce sediment generation at the site.
- Drainage structures (diversion berms (swales), chutes, perimeter channels, and collector channels) are designed as a minimum to convey peak flow rates from the 25-year, 24-hour storm event.
- Site development will not significantly alter regional drainage patterns.
- The proposed development will not restrict the flow of the 100-year flood, reduce the temporary storage capacity of the floodway or result in wash-out of solid waste.
- All areas of solid waste disposal will be adequately protected from the 24 hr duration, 25 year frequency storm event.
- All stormwater will be retained onsite with the exception of the discharge at the northwest corner of the site at detention Pond B. Discharge at this location will be less than pre-development flows as outlined in section 4.0 SITE PRE-DEVELOPMENT CONDITIONS and section 5.0 SITE POST-DEVELOPMENT CONDITIONS.

The designs, drawings, figures, data, and conclusions described herein are based upon current site conditions and existing information available. This Facility Surface Water Drainage Report (FSWDR) has been prepared for permitting purposes only.

**APPENDIX 6A**  
**SITE PRE-DEVELOPMENT CONDITIONS**



**APPENDIX 6A.1**  
**25 YEAR PRE-DEVELOPMENT CONDITIONS SUMMARY TABLE**



**25 YEAR PRE-DEVELOPMENT CONDITIONS SUMMARY TABLE**

**\* Existing Permitted Conditions**

Drainage Area	Area Sq. Mi.	Area AC.	Curve No. CN	Time of Concentration Tc-hr	Time of Concentration Tc-min	Rain Distribution Type	Frequency Year	Rainfall (24-hour) Inches	Peak Discharge CFS
<b>Watershed A</b>									
PA1	0.031	19.84	46	0.4	24.0	III	25	8.7	27.3
PA2	0.05	32	40	0.69	41.4	III	25	8.7	22.0
PA3	0.03	19.2	40	0.64	38.4	III	25	8.7	13.7
<b>Watershed B</b>									
PB1	0.041	26.24	40	0.61	36.6	III	25	8.7	19.0
PB2	0.006	3.84	42	0.32	19.2	III	25	8.7	4.3
PB3	0.01	6.4	40	0.44	26.4	III	25	8.7	5.4
<b>Watershed C</b>									
PC1	0.071	45.44	42	0.6	36.0	III	25	8.7	39.6
PC2	0.015	9.6	47	0.28	16.8	III	25	8.7	15.7
PC3	0.005	3.2	41	0.38	22.8	III	25	8.7	3.1

Combined Total  
49.3 cfs

**\* Kingsville Landfill Permit Amendment 235-B Attachment 6  
 Appendix 6A Pre-Development Conditions**

**\*\*Existing Permitted Conditions**

Drainage Area	Area Sq. Mi.	Area AC.	Curve No. CN	Time of Concentration Tc-hr	Time of Concentration Tc-min	Rain Distribution Type	Frequency Year	Rainfall (24-hour) Inches	Peak Discharge CFS
<b>Watershed A</b>									
PA1	0.031	19.84	46	0.4	24.0	III	25	8.7	28.7
PA2	0.05	32	40	0.69	41.4	III	25	8.7	22.3
PA3	0.03	19.2	40	0.64	38.4	III	25	8.7	13.9
<b>Watershed B</b>									
PB1	0.041	26.24	40	0.61	36.6	III	25	8.7	19.5
PB2	0.006	3.84	42	0.32	19.2	III	25	8.7	4.5
PB3	0.01	6.4	40	0.44	26.4	III	25	8.7	5.5
<b>Watershed C</b>									
PC1	0.071	45.44	42	0.6	36.0	III	25	8.7	40.9
PC2	0.015	9.6	47	0.28	16.8	III	25	8.7	17.1
PC3	0.005	3.2	41	0.38	22.8	III	25	8.7	3.2

Combined Total  
51.1 cfs

**\*\* Duplicated Existing Permitted Conditions from Kingsville Landfill Permit Amendment 235-B Attachment 6  
 Appendix 6A Pre-Development Conditions Using HydroCAD-Results Comparable**

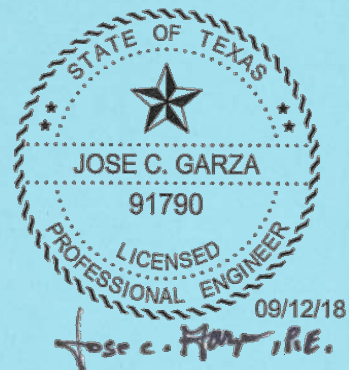
**\*\*\*Updated Permitted Conditions**

Drainage Area	Area Sq. Mi.	Area AC.	Curve No. CN	Time of Concentration Tc-hr	Time of Concentration Tc-min	Rain Distribution Type	Frequency Year	Rainfall (24-hour) Inches	Peak Discharge CFS
<b>Watershed A</b>									
PA1	0.031	19.84	46	0.4	24.0	III	25	8.7	28.7
PA2	0.05	32	40	0.69	41.4	III	25	8.7	22.3
PA3	0.03	19.2	40	0.64	38.4	III	25	8.7	13.9
<b>Watershed B</b>									
PB1	0.041	26.24	40	0.61	36.6	III	25	8.7	19.5
PB2	0.006	3.84	42	0.32	19.2	III	25	8.7	4.5
PB3	0.01	6.4	40	0.44	26.4	III	25	8.7	5.5
***PB4	0.021	13.38	40	0.26	15.6	III	25	8.7	13.9
<b>Watershed C</b>									
PC1	0.071	45.44	42	0.6	36.0	III	25	8.7	40.9
PC2	0.015	9.6	47	0.28	16.8	III	25	8.7	17.1
PC3	0.005	3.2	41	0.38	22.8	III	25	8.7	3.2

Combined Total  
51.1 cfs

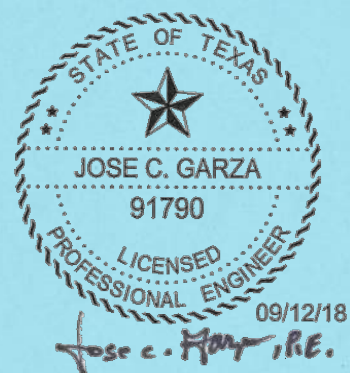
**\*\*\*Updated Permitted Conditions Includes the Addition of Drainage Area PB4  
 Results Using HydroCAD**

APPENDIX 6A.2  
SITE PRE-DEVELOPMENT CONDITIONS-EXISTING PERMITTED  
CONDITIONS





APPENDIX 6A.2.1  
KINGSVILLE LANDFILL PERMIT AMENDMENT 235-B ATTACHMENT 6  
APPENDIX 6A PRE-DEVELOPMENT CONDITIONS (TABLE OF  
CONTENTS AND PAGES 1-32)



**APPENDIX 6A**

Kingsville Landfill Permit Amendment 235-B  
Attachment 6**Appendix 6A  
Pre-Development Conditions****TABLE OF CONTENTS**

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 TR-55 Runoff Curve Number

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**Drainage Area PA1**

I. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area __ acres _X_ sq.mi. _____ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.01	0.39
Kingsville, A/D	Unimproved Area, 2 - 7% slope	49			0.02	0.98
Kingsville, A/D	Unimproved Area, > 7% slope	59			0.001	0.06
Totals =					0.031	1.43

1. Use only one CN source per line.

$$CN \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{1.43}{0.031} = 46 \quad \text{Use CN} = 46$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1,  
 fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
2.2		

$S = 1000/CN - 10: \quad S = 11.7$

$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 2.23$

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 TR-55 Time of Concentration

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 Attachment 6

**Drainage Area PA1 (Trial)**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="A-B"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
	ft. <input type="text" value="200"/>	<input type="text"/>
	in. <input type="text" value="4.5"/>	<input type="text"/>
	ft/ft <input type="text" value="0.01"/>	<input type="text"/>
	hr. <input type="text" value="0.28"/>	+ <input type="text"/> = <input type="text" value="0.28"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="B - C"/>	<input type="text"/>
	<input type="text" value="grass"/>	<input type="text"/>
	ft <input type="text" value="450"/>	<input type="text"/>
	ft/ft <input type="text" value="0.06"/>	<input type="text"/>
	ft/s <input type="text" value="4"/>	<input type="text"/>
	hr. <input type="text" value="0.03"/>	+ <input type="text"/> = <input type="text" value="0.03"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID	<input type="text" value="C - D"/>	<input type="text"/>	<b>See</b>
	ft <sup>2</sup> <input type="text" value="10"/>	<input type="text"/>	<b>Page 29</b>
	ft. <input type="text" value="20.2"/>	<input type="text"/>	
	ft. <input type="text" value="0.50"/>	<input type="text"/>	
	ft./ft. <input type="text" value="0.0125"/>	<input type="text"/>	
	<input type="text" value="0.03"/>	<input type="text"/>	
	ft./s <input type="text" value="3.5"/>	<input type="text"/>	
	ft. <input type="text" value="1000"/>	<input type="text"/>	
	hr <input type="text" value="0.08"/>	+ <input type="text"/> = <input type="text" value="0.08"/>	
			hr. <input type="text" value="0.39"/>

Pre-Development Conditions  
 TR-55 Time of Concentration

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA1 (Final)**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	A-B		
	grass		
	0.13		
ft.	200		
in.	4.5		
ft/ft	0.01		
hr.	0.28	+	= 0.28

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	B - C		
	grass		
ft	450		
ft/ft	0.06		
ft/s	4		
hr.	0.03	+	= 0.03

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	C - D		
ft <sup>2</sup>	8.36		
ft.	18.46		
ft.	0.45		
ft./ft.	0.0125		
	0.03		
ft./s	3.3		
ft.	1000		
hr.	0.08	+	= 0.08

See  
 Page 30

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr. 0.40

Pre-Development Conditions  
 TR-55 Graphical Peak Discharge Method

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA1 (Trial and Final)**

1. Data:

Drainage Area  $A_m =$  0.031 sq.mi.  
 Runoff Curve number CN = 46 (from worksheet 2)  
 Time of concentration  $T_c =$  0.40 hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  (      acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$   
 (use CN with table 4-1)

inches	2.35		
--------	------	--	--

5. Compute  $I_a/P$

0.27		
------	--	--

6. Unit peak discharge,  $q_u$   
 (use  $T_c$  and  $I_a/P$  with exhibit 4 - III)

csm/in	400		
--------	-----	--	--

7. Runoff, Q  
 (from worksheet 2)

inches	2.2		
--------	-----	--	--

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

1.0		
-----	--	--

9. Peak discharge,  $q_p$   
 (where  $q_p = q_u A_m Q F_p$ )

cfs	27.3		
-----	------	--	--

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Pre-Development Conditions  
 TR-55 Runoff Curve Number

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA2**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ X_ sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.05	1.95
Totals =					0.05	1.95

1. Use only one CN source per line.

$$\sqrt{\text{(weighted) total product}} = \frac{1.95}{0.05} = 39 \quad \text{Use CN} = 40$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.6		

$$S = 1000 / CN - 10: \quad S = 15$$

$$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.6$$

Appendix 6A  
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Pre-Development Conditions  
 TR-55 Time of Concentration

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA2**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="F - G"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
in.	<input type="text" value="4.5"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
hr.	<input type="text" value="0.39"/>	+ <input type="text"/> = <input type="text" value="0.39"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="G - E"/>	<input type="text"/>
	<input type="text" value="grass"/>	<input type="text"/>
ft	<input type="text" value="1700"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
ft/s	<input type="text" value="1.6"/>	<input type="text"/>
hr.	<input type="text" value="0.30"/>	+ <input type="text"/> = <input type="text" value="0.30"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text"/>	<input type="text"/>
ft <sup>2</sup>	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft./ft.	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft./s	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
hr	<input type="text"/>	+ <input type="text"/> = <input type="text" value="0.00"/>

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr.

Pre-Development Conditions  
 TR-55 Graphical Peak Discharge Method

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA2**

1. Data:

Drainage Area  $A_m =$  0.05 sq.mi.  
 Runoff Curve number  $CN =$  40 (from worksheet 2)  
 Time of concentration  $T_c =$  0.69 hr (from worksheet 3)  
 Rainfall distribution type  $=$  III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed  $=$  0 % of  $A_m$  (      acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$   
 (use CN with table 4-1)

inches	3.00		
--------	------	--	--

5. Compute  $I_a/P$

	0.34		
--	------	--	--

6. Unit peak discharge,  $q_u$   
 (use  $T_c$  and  $I_a/P$  with exhibit 4 - III)

csm/in	275		
--------	-----	--	--

7. Runoff, Q  
 (from worksheet 2)

inches	1.6		
--------	-----	--	--

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

	1.0		
--	-----	--	--

9. Peak discharge,  $q_p$   
 (where  $q_p = q_u A_m Q F_p$ )

cfs	22.0		
-----	------	--	--

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Pre-Development Conditions  
 TR-55 Runoff Curve Number

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA3**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.03	1.17
Totals =					0.03	1.17

1. Use only one CN source per line.

$$N \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{1.17}{0.03} = 39 \quad \text{Use CN} = 40$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.6		

$S = 1000 / CN - 10; \quad S = 15$

$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.6$

Pre-Development Conditions  
 TR-55 Time of Concentration

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA3**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	H - I	
	grass	
	0.13	
ft.	300	
in.	4.5	
ft/ft	0.01	
hr.	0.39	+ [ ] = [ 0.39 ]

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	I - E	
	grass	
ft	1450	
ft/ft	0.01	
ft/s	1.6	
hr.	0.25	+ [ ] = [ 0.25 ]

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	[ ]	[ ]
ft <sup>2</sup>	[ ]	[ ]
ft.	[ ]	[ ]
ft.	[ ]	[ ]
ft./ft.	[ ]	[ ]
	[ ]	[ ]
ft./s	[ ]	[ ]
ft.	[ ]	[ ]
hr	[ ]	+ [ ] = [ 0.00 ]

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr. [ 0.64 ]

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Pre-Development Conditions  
 TR-55 Graphical Peak Discharge Method

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PA3**

1. Data:

Drainage Area  $A_m = 0.03$  sq.mi.  
 Runoff Curve number  $CN = 40$  (from worksheet 2)  
 Time of concentration  $T_c = 0.64$  hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  (\_\_\_\_ acres/mi.<sup>2</sup> covered)

	Storm #1	Storm #2	Storm #3
2. Frequency year	25		
3. Rainfall, P (24-hour) inches	8.7		
4. Initial abstraction, $I_a$ (use CN with table 4-1) inches	3.00		
5. Compute $I_a/P$	0.34		
6. Unit peak discharge, $q_u$ (use $T_c$ and $I_a/p$ with exhibit 4 - III) csm/in	285		
7. Runoff, Q (from worksheet 2) inches	1.6		
8. Pond & swamp adjustment factor, $F_p$ (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)	1.0		
9. Peak discharge, $q_p$ (where $q_p = q_u A_m Q F_p$ ) cfs	13.7		

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Pre-Development Conditions  
 TR-55 Runoff Curve Number

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 Attachment 6

**Drainage Area PB1**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ X_ sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.04	1.56
Kingsville, A/D	Unimproved Area, 3 - 7% slope	49			0.001	0.05
Totals =					0.041	1.61

1. Use only one CN source per line.

$$I \text{ (weighted) } = \frac{\text{total product}}{\text{total area}} = \frac{1.61}{0.041} = 39 \quad \text{Use CN} = 40$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.6		

$$S = 1000 / CN - 10: \quad S = 15$$

$$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.6$$

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**Drainage Area PB1**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="j-k"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
in.	<input type="text" value="4.5"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
hr.	<input type="text" value="0.39"/>	+ <input type="text"/> = <input type="text" value="0.39"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="k-l"/>	<input type="text"/>
	<input type="text" value="grass"/>	<input type="text"/>
ft	<input type="text" value="1250"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
ft/s	<input type="text" value="1.6"/>	<input type="text"/>
hr.	<input type="text" value="0.22"/>	+ <input type="text"/> = <input type="text" value="0.22"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text"/>	<input type="text"/>
ft <sup>2</sup>	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft./ft.	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft./s	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
hr	<input type="text"/>	+ <input type="text"/> = <input type="text" value="0.00"/>

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr.

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**Drainage Area PB1**

1. Data:

Drainage Area  $A_m =$  0.041 sq.mi.  
 Runoff Curve number CN = 40 (from worksheet 2)  
 Time of concentration  $T_c =$  0.61 hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  ( \_\_\_\_\_ acres/mi.<sup>2</sup> covered)

2. Frequency	year	Storm #1 25	Storm #2	Storm #3
3. Rainfall, P (24-hour)	inches	8.7		
4. Initial abstraction, $I_a$ (use CN with table 4-1)	inches	3.00		
5. Compute $I_a/P$		0.34		
6. Unit peak discharge, $q_u$ (use $T_c$ and $I_a/p$ with exhibit 4 - III)	csm/in	290		
7. Runoff, Q (from worksheet 2)	inches	1.6		
8. Pond & swamp adjustment factor, $F_p$ (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)		1.0		
9. Peak discharge, $q_p$ (where $q_p = q_u A_m Q F_p$ )	cfs	19.0		

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**Drainage Area PB2**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ X sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.004	0.16
Kingsville, A/D	Unimproved Area, 3 - 7% slope	49			0.002	0.10
Totals =					0.006	0.25

1. Use only one CN source per line.

$$N \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{0.25}{0.006} = 42 \quad \text{Use CN} = 42$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.8		

$S = 1000 / CN - 10: \quad S = 14$

$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.8$

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**Drainage Area PB2**

**Sheet flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="m-1"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
in.	<input type="text" value="4.5"/>	<input type="text"/>
ft/ft	<input type="text" value="0.016"/>	<input type="text"/>
hr.	<input type="text" value="0.32"/>	+ <input type="text"/> = <input type="text" value="0.32"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft	<input type="text"/>	<input type="text"/>
ft/ft	<input type="text"/>	<input type="text"/>
ft/s	<input type="text"/>	<input type="text"/>
hr.	<input type="text" value="0.00"/>	+ <input type="text"/> = <input type="text" value="0.00"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID	<input type="text"/>	<input type="text"/>
ft <sup>2</sup>	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft./ft.	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft./s	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
hr	<input type="text"/>	+ <input type="text"/> = <input type="text" value="0.00"/>
hr.	<input type="text" value="0.32"/>	

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**Drainage Area PB2**

1. Data:

Drainage Area  $A_m =$  0.006 sq.mi.  
 Runoff Curve number  $CN =$  42 (from worksheet 2)  
 Time of concentration  $T_c =$  0.32 hr (from worksheet 3)  
 Rainfall distribution type  $=$  III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed  $=$  0 % of  $A_m$  (      acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$

(use CN with table 4-1)

inches	2.76		
--------	------	--	--

5. Compute  $I_a/P$

	0.32		
--	------	--	--

6. Unit peak discharge,  $q_u$

(use  $T_c$  and  $I_a/p$  with exhibit 4 - III)

csm/in	400		
--------	-----	--	--

7. Runoff, Q

(from worksheet 2)

inches	1.8		
--------	-----	--	--

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

	1.0		
--	-----	--	--

9. Peak discharge,  $q_p$

(where  $q_p = q_u A_m Q F_p$ )

cfs	4.3		
-----	-----	--	--

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**Drainage Area PB3**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ x sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.01	0.39
Totals =					0.01	0.39

1. Use only one CN source per line.

$$N \text{ (weighted): } \frac{\text{total product}}{\text{total area}} = \frac{0.39}{0.01} = 39 \quad \text{Use CN} = 40$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.6		

$$S = 1000 / CN - 10: \quad S = 15$$

$$Q = \frac{[P - 0.2s]2}{(P + 0.8s)} \quad Q = 1.6$$

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**Drainage Area PB3**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="n-o"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
in.	<input type="text" value="4.5"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
hr.	<input type="text" value="0.39"/>	+ <input type="text"/> = <input type="text" value="0.39"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="o-m"/>	<input type="text"/>
	<input type="text" value="grass"/>	<input type="text"/>
ft	<input type="text" value="300"/>	<input type="text"/>
ft/ft	<input type="text" value="0.01"/>	<input type="text"/>
ft/s	<input type="text" value="1.6"/>	<input type="text"/>
hr.	<input type="text" value="0.05"/>	+ <input type="text"/> = <input type="text" value="0.05"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text"/>	<input type="text"/>
ft <sup>2</sup>	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft./ft.	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft./s	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
hr	<input type="text"/>	+ <input type="text"/> = <input type="text" value="0.00"/>

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr.

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**Drainage Area PB3**

1. Data:

Drainage Area  $A_m =$  0.01 sq.mi.  
 Runoff Curve number  $CN =$  40 (from worksheet 2)  
 Time of concentration  $T_c =$  0.44 hr (from worksheet 3)  
 Rainfall distribution type  $=$  III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed  $=$  0 % of  $A_m$  (      acres/mi.<sup>2</sup> covered)

		Storm #1	Storm #2	Storm #3
2. Frequency	year	25		
3. Rainfall, P (24-hour)	inches	8.7		
4. Initial abstraction, $I_a$ (use CN with table 4-1)	inches	3.00		
5. Compute $I_a/P$		0.34		
6. Unit peak discharge, $q_u$ (use $T_c$ and $I_a/p$ with exhibit 4 - III)	csm/in	340		
7. Runoff, Q (from worksheet 2)	inches	1.6		
8. Pond & swamp adjustment factor, $F_p$ (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)		1.0		
9. Peak discharge, $q_p$ (where $q_p = q_u A_m Q F_p$ )	cfs	5.4		

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**Drainage Area PCT**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area __ acres _x_ sq.mi. _____ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.05	1.95
Kingsville, A/D	Unimproved Area, 3 - 7% slope	49			0.02	0.98
Kingsville, A/D	Unimproved Area, > 7% slope	59			0.001	0.06
Totals =					0.071	2.99

1. Use only one CN source per line.

$$CN \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{2.99}{0.071} = 42 \quad \text{Use CN} = 42$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.8		

$S = 1000 / CN - 10: \quad S = 13.81$

$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.8$

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**Drainage Area PC1**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	j-p	
	grass	
	0.13	
ft.	300	
in.	4.5	
ft/ft	0.01	
hr.	0.39	+ [ ] = [ 0.39 ]

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	p-q	
	grass	
ft	650	
ft/ft	0.025	
ft/s	1.6	
hr.	0.11	+ [ ] = [ 0.11 ]

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	q-r		See
ft <sup>2</sup>	17.5		Page 31
ft.	70.01		
ft.	0.25		
ft./ft.	0.018		
	0.03		
ft./s	2.6		
ft.	950		
hr	0.10	+ [ ] = [ 0.10 ]	

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr. [ 0.60 ]



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**Drainage Area PC1**

1. Data:

Drainage Area  $A_m = 0.071$  sq.mi.  
 Runoff Curve number  $CN = 42$  (from worksheet 2)  
 Time of concentration  $T_c = 0.60$  hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  (\_\_\_\_ acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$   
 (use CN with table 4-1)

inches	2.76		
--------	------	--	--

5. Compute  $I_a/P$

	0.32		
--	------	--	--

6. Unit peak discharge,  $q_u$   
 (use  $T_c$  and  $I_a/p$  with exhibit 4 - III)

csm/in	310		
--------	-----	--	--

7. Runoff, Q  
 (from worksheet 2)

inches	1.8		
--------	-----	--	--

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

	1.0		
--	-----	--	--

9. Peak discharge,  $q_p$   
 (where  $q_p = q_u A_m Q F_p$ )

cfs	39.6		
-----	------	--	--

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**Drainage Area PC2**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ X_ sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.004	0.16
Kingsville, A/D	Unimproved Area, 3 - 7% slope	49			0.01	0.49
Kingsville, A/D	Unimproved Area, > 7% slope	59			0.001	0.06
Totals =					0.015	0.71

1. Use only one CN source per line.

$$N \text{ (weighted): } \frac{\text{total product}}{\text{total area}} = \frac{0.71}{0.015} = 47 \quad \text{Use CN} = 47$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
2.3		

$S = 1000 / CN - 10: \quad S = 11$

$Q = \frac{(P - 0.2s)2}{(P + 0.8s)} \quad Q = 2.3$

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**Drainage Area PC2**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two-year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.5}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	a-l		
	grass		
	0.13		
ft.	150		
in.	4.5		
ft/ft	0.01		
hr.	0.22	+	
		=	0.22

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	u-w		
	grass		
ft.	180		
ft/ft	0.06		
ft/s	4		
hr.	0.01	+	
		=	0.01

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>
20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

Segment ID	w-x		
ft <sup>2</sup>	3.54		
ft.	11.72		
ft.	0.30		
ft./ft.	0.036		
	0.03		
ft./s	4.2		
ft.	650		
hr.	0.04	+	
		=	0.04
			hr. 0.28

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 Attachment 6

**Drainage Area PC2**

1. Data:

Drainage Area  $A_m = 0.015$  sq.mi.  
 Runoff Curve number  $CN = 47$  (from worksheet 2)  
 Time of concentration  $T_c = 0.28$  hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  (\_\_\_ acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$   
 (use CN with table 4-1)

inches	2.26		
--------	------	--	--

5. Compute  $I_a/P$

	0.26		
--	------	--	--

6. Unit peak discharge,  $q_u$   
 (use  $T_c$  and  $I_a/p$  with exhibit 4 - III)

csm/in	455		
--------	-----	--	--

7. Runoff, Q  
 (from worksheet 2)

inches	2.3		
--------	-----	--	--

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

	1.0		
--	-----	--	--

9. Peak discharge,  $q_p$   
 (where  $q_p = q_u A_m Q F_p$ )

cfs	15.7		
-----	------	--	--

Pre-Development Conditions  
 TR-55 Runoff Curve Number

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PC3**

1. Runoff Curve Number (CN)

Soil Name and hydrologic group (Appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN			Area _ acres _ x sq.mi. _ %	Product of CN x Area
		Table 2-2	Fig. 2-3	Fig. 2-4		
Kingsville, A/D	Unimproved Area, 0 - 2% slope	39			0.004	0.16
Kingsville, A/D	Unimproved Area, 3 - 7% slope	49			0.001	0.05
Totals =					0.005	0.21

1. Use only one CN source per line.

$$N \text{ (weighted)} = \frac{\text{total product}}{\text{total area}} = \frac{0.21}{0.005} = 41 \quad \text{Use CN} = 41$$

2. Runoff

Frequency ..... yr.  
 Rainfall, P (24-hour) ..... in.  
 Runoff, Q ..... in.  
 (use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4)

Storm #1	Storm #2	Storm #3
25		
8.7		
1.7		

$S = 1000 / CN - 10: \quad S = 14$

$Q = \frac{(P - 0.2s)^2}{(P + 0.8s)} \quad Q = 1.7$

Appendix 8A  
 May 1998  
 Revision 1

Pre-Development Conditions  
 TR-55 Time of Concentration

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area PC3**

**Sheet Flow** (applicable to Tc only)

1. Surface description (table 3-1)
2. Mannings roughness coeff., n (table 3-1)
3. Flow length, L (total < 300 ft)
4. Two -year 24-hr rainfall, P<sub>2</sub>
5. Land slope, s
6.  $T_t = \frac{0.007 (nL)^{0.58}}{P_2^{0.5} s^{0.4}}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="y-s"/>	
	<input type="text" value="grass"/>	<input type="text"/>
	<input type="text" value="0.13"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
in.	<input type="text" value="4.5"/>	<input type="text"/>
ft./ft.	<input type="text" value="0.015"/>	<input type="text"/>
hr.	<input type="text" value="0.33"/>	+ <input type="text"/> = <input type="text" value="0.33"/>

**Shallow Concentrated Flow**

7. surface description (paved or unpaved)
8. Flow length, L
9. Watercourse slope, S
10. average velocity, V (figure 3-1)
11.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text" value="s-t"/>	<input type="text"/>
	<input type="text" value="grass"/>	<input type="text"/>
ft.	<input type="text" value="300"/>	<input type="text"/>
ft./ft.	<input type="text" value="0.015"/>	<input type="text"/>
ft./s	<input type="text" value="1.6"/>	<input type="text"/>
hr.	<input type="text" value="0.05"/>	+ <input type="text"/> = <input type="text" value="0.05"/>

**Channel Flow**

12. Cross sectional flow area, a
13. Wetted perimeter, Pw
14. Hydraulic radius, r = a/Pw
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$  Compute V
18. Flow Length, L
19.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub>

Segment ID	<input type="text"/>	<input type="text"/>
ft <sup>2</sup>	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
ft./ft.	<input type="text"/>	<input type="text"/>
	<input type="text"/>	<input type="text"/>
ft./s	<input type="text"/>	<input type="text"/>
ft.	<input type="text"/>	<input type="text"/>
hr.	<input type="text"/>	+ <input type="text"/> = <input type="text" value="0.00"/>

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19) hr.

Pre-Development Conditions  
 TR-55 Graphical Peak Discharge Method

Kingsville Landfill Permit Application 235-B  
 Attachment 6

**Drainage Area FC3**

1. Data:

Drainage Area  $A_m =$  0.005 sq.mi.  
 Runoff Curve number CN = 41 (from worksheet 2)  
 Time of concentration  $T_c =$  0.38 hr (from worksheet 3)  
 Rainfall distribution type = III (I, IA, II, III)  
 Pond and swamp areas spread throughout watershed = 0 % of  $A_m$  (\_\_\_\_ acres/mi.<sup>2</sup> covered)

2. Frequency

	Storm #1	Storm #2	Storm #3
year	25		

3. Rainfall, P (24-hour)

inches	8.7		
--------	-----	--	--

4. Initial abstraction,  $I_a$

inches	2.88		
--------	------	--	--

(use CN with table 4-1)

5. Compute  $I_a/P$

	0.33		
--	------	--	--

6. Unit peak discharge,  $q_u$

csm/in	360		
--------	-----	--	--

(use  $T_c$  and  $I_a/p$  with exhibit 4 - III)

7. Runoff, Q

inches	1.7		
--------	-----	--	--

(from worksheet 2)

8. Pond & swamp adjustment factor,  $F_p$  (use percent pond and swamp area with table 4-2. Factor is 1.0 for zero percent pond and swamp area.)

	1.0		
--	-----	--	--

9. Peak discharge,  $q_p$

cfs	3.1		
-----	-----	--	--

(where  $q_p = q_u A_m Q F_p$ )

Appendix 6A  
 May 1998  
 Revision 1

Kingsville Landfill Permit Amendment 235-B  
 PreDevelop Channel C-D Trial 1  
 Worksheet for Triangular Channel

Attachment 6

Project Description	
Project File	d:\98 files\kingsville landfill permit 235b\predevel.fm2
Worksheet	Seg CD
Flow Element	Triangular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data	
Mannings Coefficient	0.030
Channel Slope	0.012500 ft/ft
Depth	1.00 ft
Left Side Slope	17.000000 H : V
Right Side Slope	3.000000 H : V

Results		
Discharge	34.66	cfs
Flow Area	10.00	ft <sup>2</sup>
Wetted Perimeter	20.19	ft
Top Width	20.00	ft
Critical Depth	0.94	ft
Critical Slope	0.017063	ft/ft
Velocity	3.47	ft/s
Velocity Head	0.19	ft
Specific Energy	1.19	ft
Froude Number	0.86	
Flow is subcritical.		



Kingsville Landfill Permit Amendment 235-B  
 Pre-Development Channel C-D Final Appendix 6A  
 Worksheet for Triangular Channel

Project Description	
Project File	d:\98 files\kingsville landfill permit 235b\final.fm2
Worksheet	6A C-D final
Flow Element	Triangular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coefficient	0.030
Channel Slope	0.012500 ft/ft
Left Side Slope	17.000000 H : V
Right Side Slope	3.000000 H : V
Discharge	27.30 cfs

Results		
Depth	0.91	ft
Flow Area	8.36	ft <sup>2</sup>
Wetted Perimeter	18.46	ft
Top Width	18.29	ft
Critical Depth	0.86	ft
Critical Slope	0.017616	ft/ft
Velocity	3.27	ft/s
Velocity Head	0.17	ft
Specific Energy	1.08	ft
Froude Number	0.85	
Flow is subcritical.		

May 1998  
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06/11/98  
 09:27:57 PM

Haestad Methods, Inc. 37 Brookside Road Waterbury, CT 06708 (203) 755-1666

FlowMaster v5.15  
 Page 1 of 1

Kingsville Landfill Permit Amendment 235-8  
 PreDevelopment Segment Q - R  
 Worksheet for Triangular Channel

Attachment 6

Project Description	
Project File	d:\98 files\kingsville landfill permit 235b\predevel.fm2
Worksheet	PreDev Q-R
Flow Element	Triangular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data	
Mannings Coefficient	0.030
Channel Slope	0.018000 ft/ft
Depth	0.50 ft
Left Side Slope	82.000000 H : V
Right Side Slope	58.000000 H : V

Results		
Discharge	46.15	cfs
Flow Area	17.50	ft <sup>2</sup>
Wetted Perimeter	70.01	ft
Top Width	70.00	ft
Critical Depth	0.49	ft
Critical Slope	0.021023	ft/ft
Velocity	2.64	ft/s
Velocity Head	0.11	ft
Specific Energy	0.61	ft
Froude Number	0.93	
Flow is subcritical.		

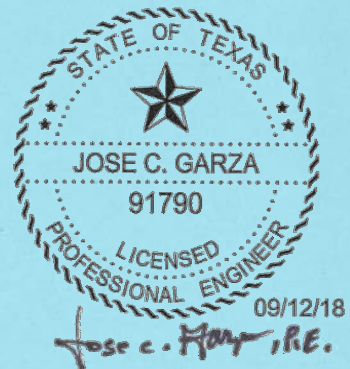
Kingsville Landfill Permit Amendment 235-B  
 PreDevelopment Segment W-X  
 Attachment 6  
 Worksheet for Triangular Channel

Project Description	
Project File	d:\98 files\kingsville landfill permit 235b\predevel.fm2
Worksheet	PreD WX Final
Flow Element	Triangular Channel
Method	Manning's Formula
Solve For	Channel Depth

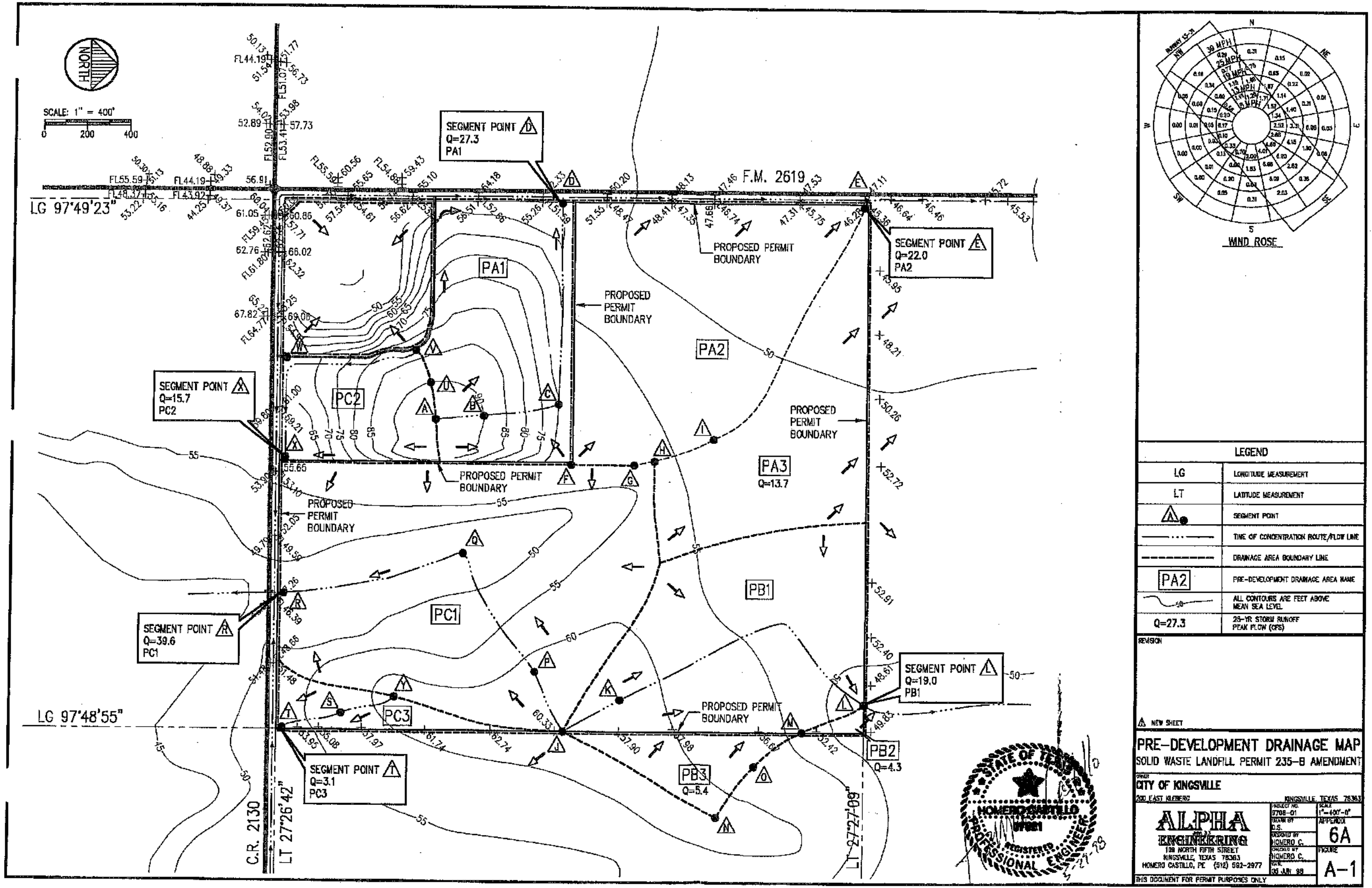
Input Data	
Mannings Coefficient	0.030
Channel Slope	0.036000 ft/ft
Left Side Slope	16.000000 H : V
Right Side Slope	3.000000 H : V
Discharge	15.00 cfs

Results		
Depth	0.61	ft
Flow Area	3.54	ft <sup>2</sup>
Wetted Perimeter	11.72	ft
Top Width	11.60	ft
Critical Depth	0.69	ft
Critical Slope	0.018964	ft/ft
Velocity	4.23	ft/s
Velocity Head	0.28	ft
Specific Energy	0.89	ft
Froude Number	1.35	
Flow is supercritical.		

APPENDIX 6A.2.2  
PRE-DEVELOPMENT DRAINAGE MAP SOLID WASTE LANDFILL  
PERMIT 235-B AMENDMENT FIGURE A-1

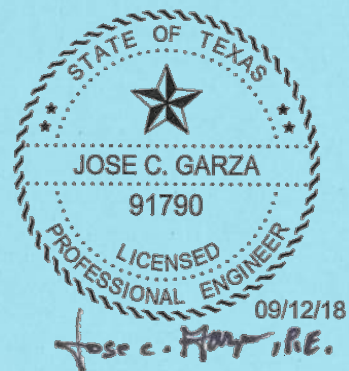


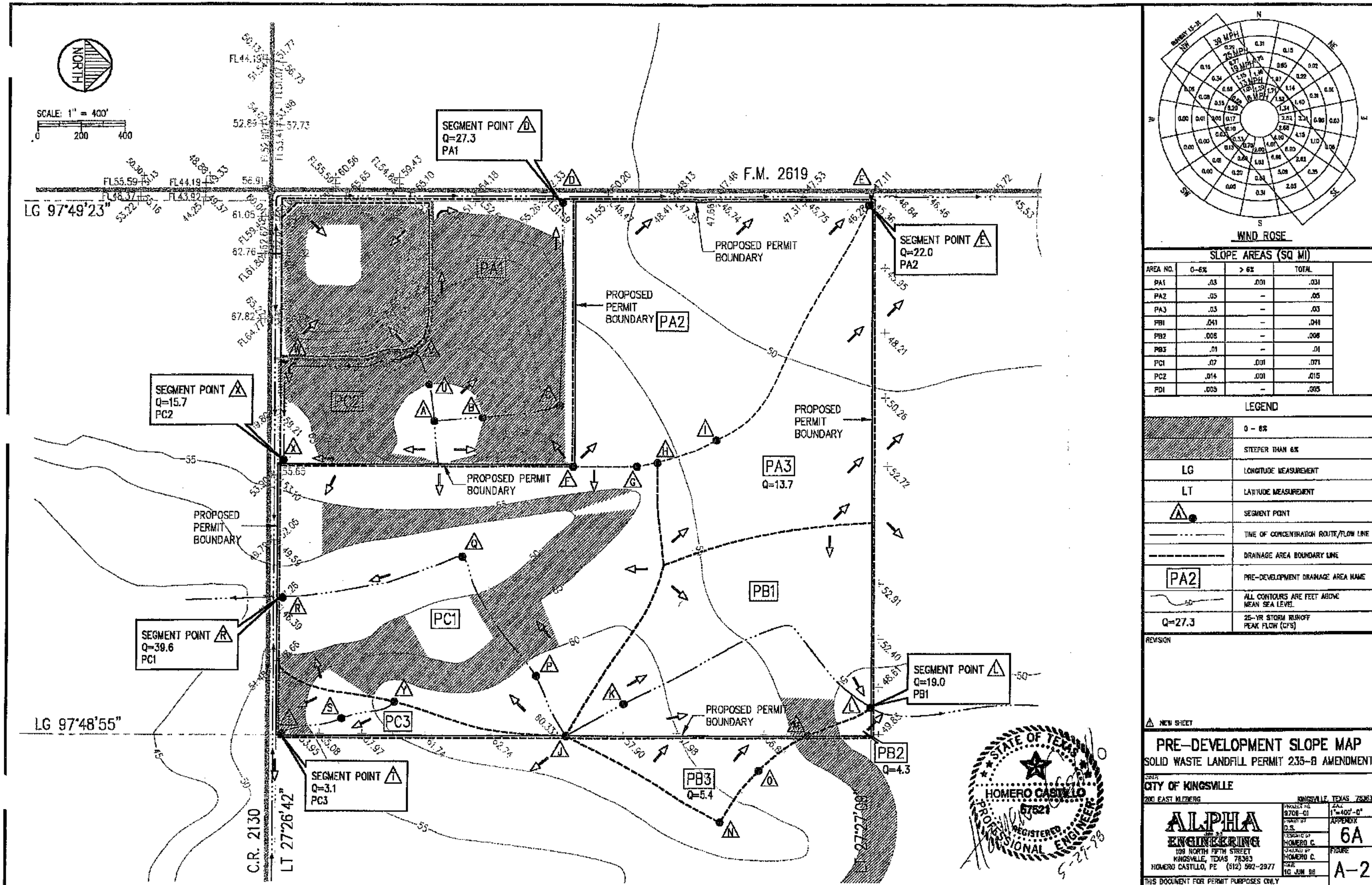
FOR PERMIT PURPOSES ONLY



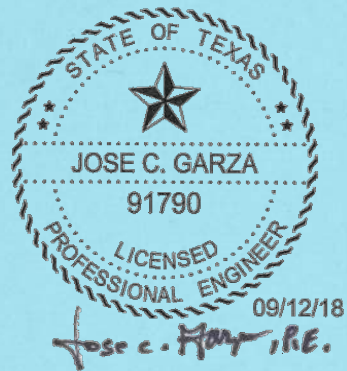
LEGEND	
LG	LONGITUDE MEASUREMENT
LT	LATITUDE MEASUREMENT
△	SEGMENT POINT
—	TIME OF CONCENTRATION ROUTE/FLOW LINE
---	DRAINAGE AREA BOUNDARY LINE
PA2	PRE-DEVELOPMENT DRAINAGE AREA NAME
50	ALL CONTOURS ARE FEET ABOVE MEAN SEA LEVEL
Q=27.3	25-YR STORM RUNOFF PEAK FLOW (CFD)
REVISION	
NEW SHEET	
<b>PRE-DEVELOPMENT DRAINAGE MAP</b>	
SOLID WASTE LANDFILL PERMIT 235-B AMENDMENT	
CITY OF KINGSVILLE	
200 EAST KILBERG KINGSVILLE, TEXAS 78363	
<b>ALPHA ENGINEERING</b>	PROJECT NO. 9708-01
100 NORTH FIFTH STREET	SCALE 1"=400'-0"
KINGSVILLE, TEXAS 78363	APPENDIX
HOMERO CASTILLO, P.E. (512) 582-2977	DESIGNED BY HOMERO C. CASTILLO
DATE 03 JAN 89	CHECKED BY HOMERO C. CASTILLO
	FIGURE 6A
	SHEET A-1

APPENDIX 6A.2.3  
PRE-DEVELOPMENT SLOPE MAP SOLID WASTE LANDFILL PERMIT  
235-B AMENDMENT FIGURE A-2

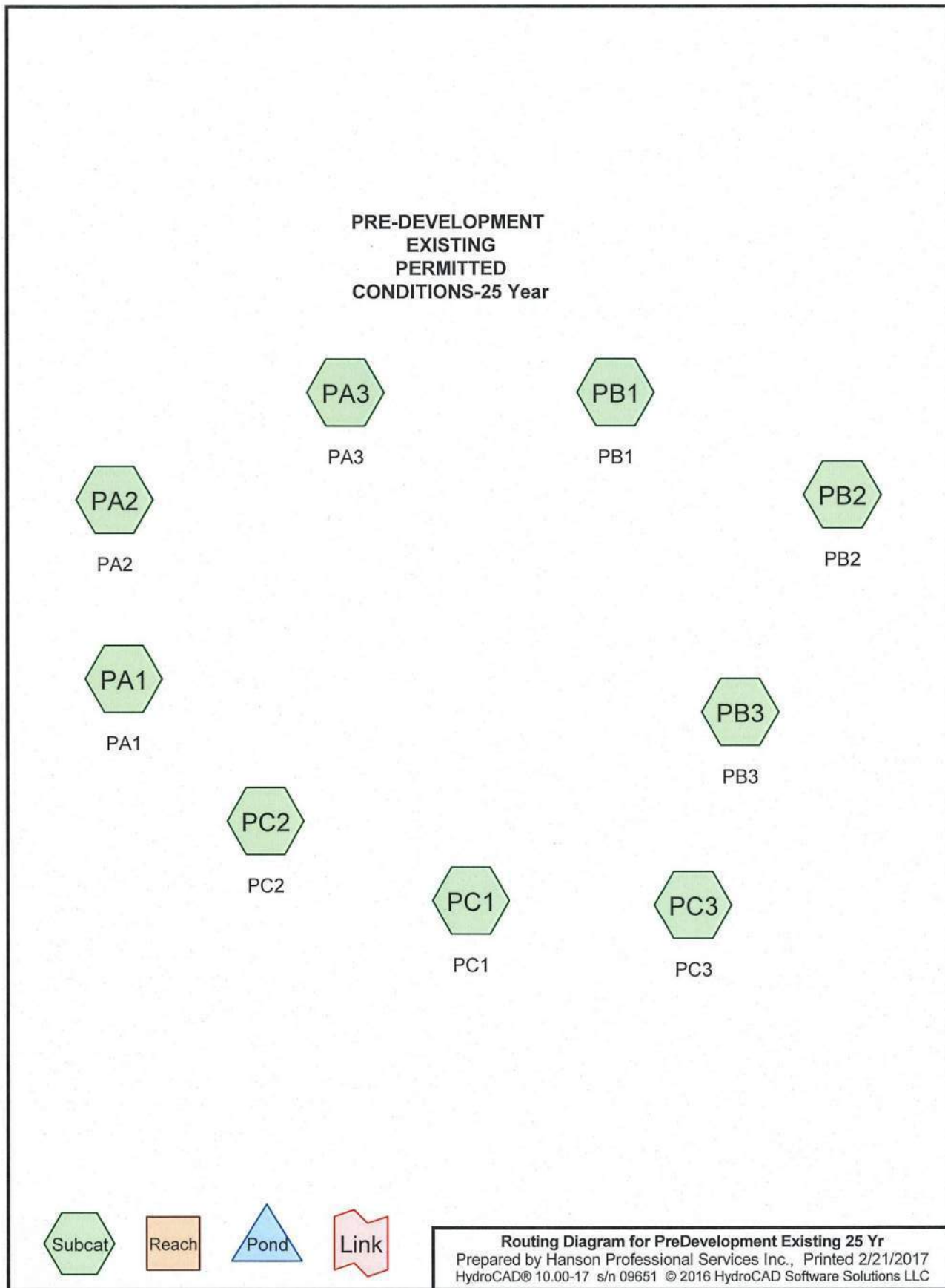




**APPENDIX 6A.2.4**  
**HYDROCAD MODEL PRE-DEVELOPMENT CONDITIONS 25 YEAR**  
**EXISTING PERMITTED CONDITIONS**







**PreDevelopment Existing 25 Yr**

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
19.840	46	(PA1)
83.840	40	(PA2, PA3, PB1, PB3)
49.280	42	(PB2, PC1)
9.600	47	(PC2)
3.200	41	(PC3)
<b>165.760</b>	<b>42</b>	<b>TOTAL AREA</b>

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
165.760	Other	PA1, PA2, PA3, PB1, PB2, PB3, PC1, PC2, PC3
<b>165.760</b>		<b>TOTAL AREA</b>

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.000	0.000	165.760	165.760		PA1, PA2, PA3, PB1, PB2, PB3, PC1, PC2, PC3
<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>165.760</b>	<b>165.760</b>	<b>TOTAL AREA</b>	

**PreDevelopment Existing 25 Yr**

*Type III 24-hr 25-Year Rainfall=8.70"*

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Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment PA1: PA1</b>	Runoff Area=19.840 ac 0.00% Impervious Runoff Depth=2.23" Tc=24.0 min CN=46 Runoff=28.74 cfs 3.688 af
<b>Subcatchment PA2: PA2</b>	Runoff Area=32.000 ac 0.00% Impervious Runoff Depth=1.57" Tc=41.4 min CN=40 Runoff=22.31 cfs 4.186 af
<b>Subcatchment PA3: PA3</b>	Runoff Area=19.200 ac 0.00% Impervious Runoff Depth=1.57" Tc=38.4 min CN=40 Runoff=13.91 cfs 2.511 af
<b>Subcatchment PB1: PB1</b>	Runoff Area=26.240 ac 0.00% Impervious Runoff Depth=1.57" Tc=36.6 min CN=40 Runoff=19.49 cfs 3.432 af
<b>Subcatchment PB2: PB2</b>	Runoff Area=3.840 ac 0.00% Impervious Runoff Depth=1.79" Tc=19.2 min CN=42 Runoff=4.48 cfs 0.571 af
<b>Subcatchment PB3: PB3</b>	Runoff Area=6.400 ac 0.00% Impervious Runoff Depth=1.57" Tc=26.4 min CN=40 Runoff=5.49 cfs 0.837 af
<b>Subcatchment PC1: PC1</b>	Runoff Area=45.440 ac 0.00% Impervious Runoff Depth=1.79" Tc=36.0 min CN=42 Runoff=40.94 cfs 6.761 af
<b>Subcatchment PC2: PC2</b>	Runoff Area=9.600 ac 0.00% Impervious Runoff Depth=2.34" Tc=16.8 min CN=47 Runoff=17.12 cfs 1.875 af
<b>Subcatchment PC3: PC3</b>	Runoff Area=3.200 ac 0.00% Impervious Runoff Depth=1.68" Tc=22.8 min CN=41 Runoff=3.20 cfs 0.447 af

**Total Runoff Area = 165.760 ac Runoff Volume = 24.309 af Average Runoff Depth = 1.76"**  
**100.00% Pervious = 165.760 ac 0.00% Impervious = 0.000 ac**

**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PA1: PA1**

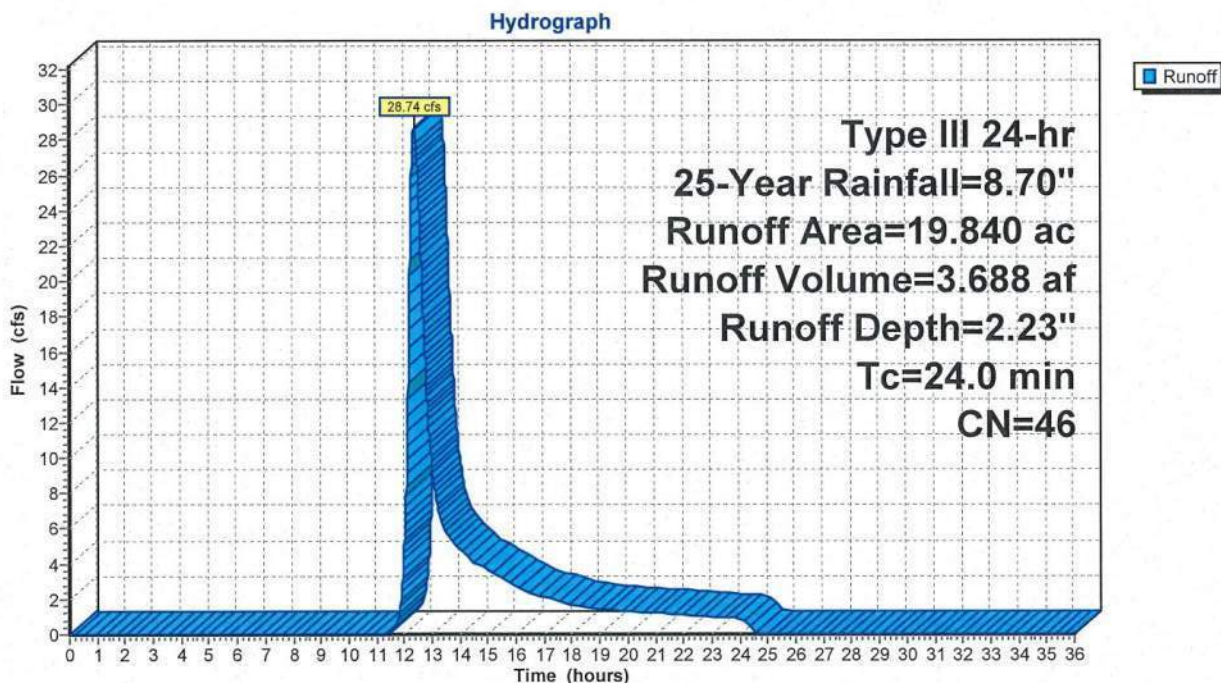
Runoff = 28.74 cfs @ 12.38 hrs, Volume= 3.688 af, Depth= 2.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 19.840	46	
19.840		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
24.0					Direct Entry,

**Subcatchment PA1: PA1**



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PA2: PA2**

Runoff = 22.31 cfs @ 12.69 hrs, Volume= 4.186 af, Depth= 1.57"

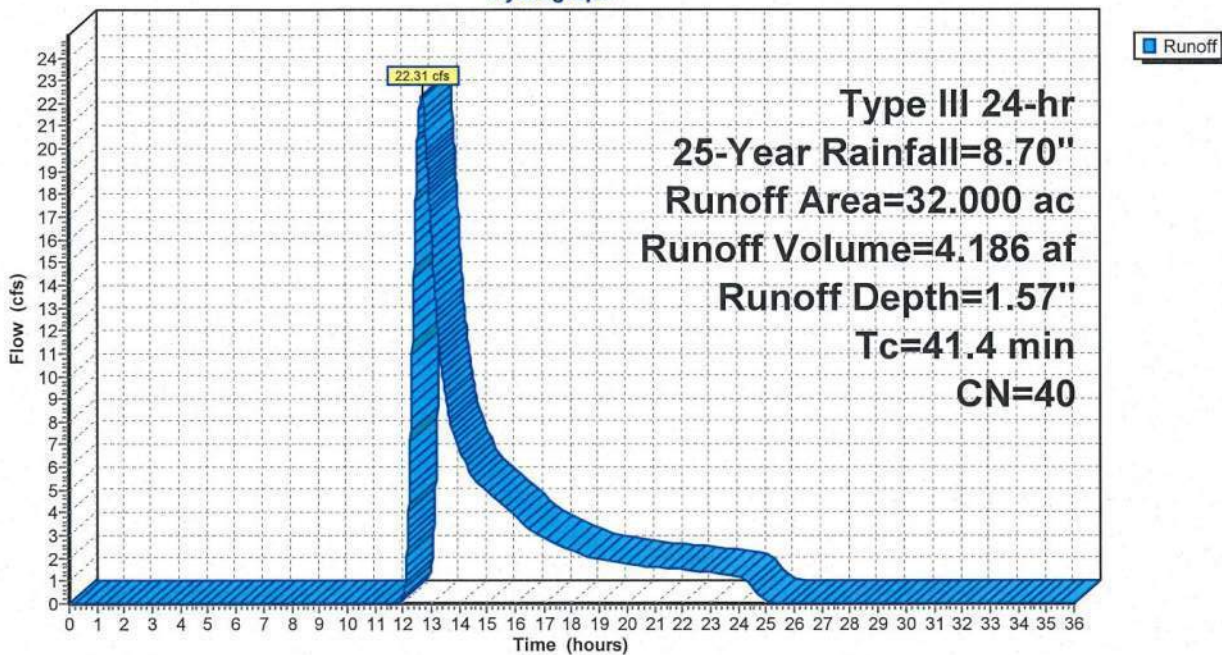
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 32.000	40	
32.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
41.4					Direct Entry,

**Subcatchment PA2: PA2**

Hydrograph



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PA3: PA3**

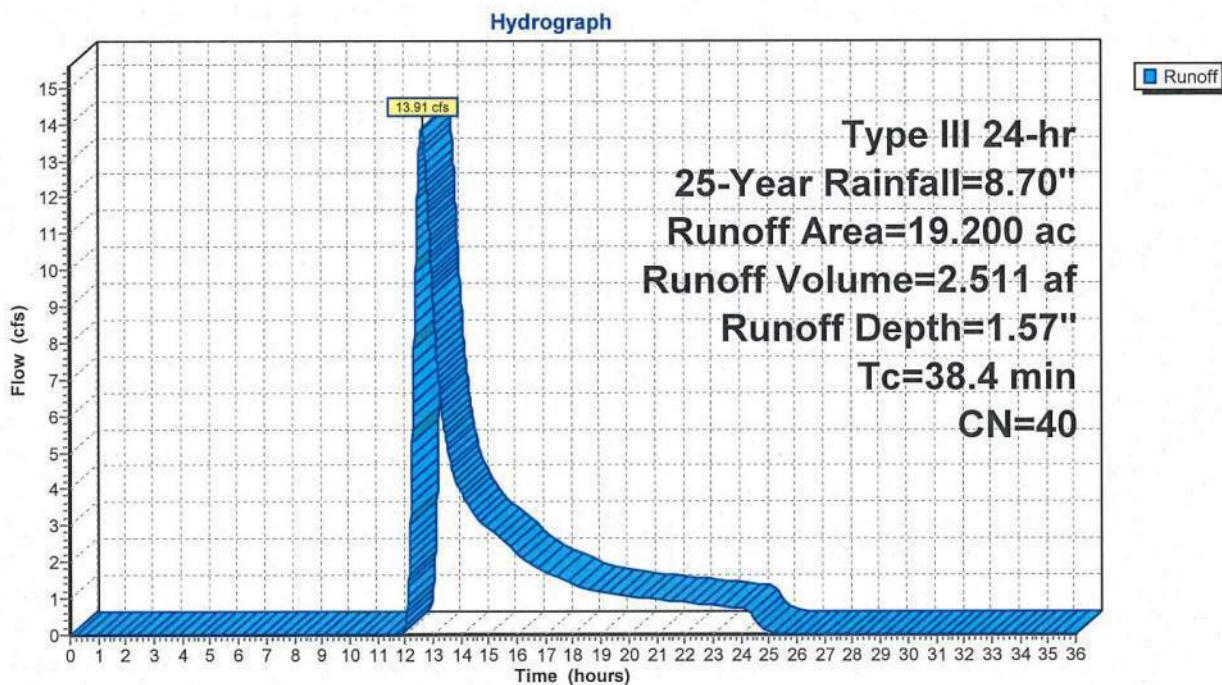
Runoff = 13.91 cfs @ 12.64 hrs, Volume= 2.511 af, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 19.200	40	
19.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
38.4					Direct Entry, Direct Entry

**Subcatchment PA3: PA3**





**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB1: PB1**

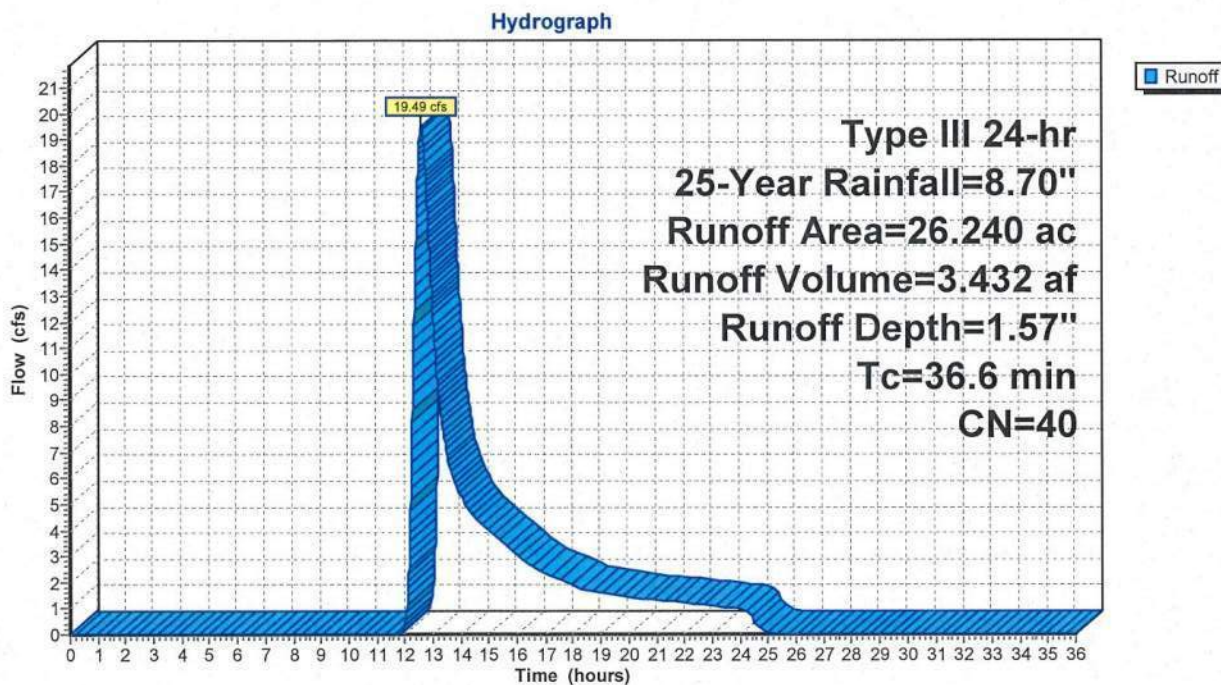
Runoff = 19.49 cfs @ 12.61 hrs, Volume= 3.432 af, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 26.240	40	
26.240		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
36.6					Direct Entry,

**Subcatchment PB1: PB1**



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB2: PB2**

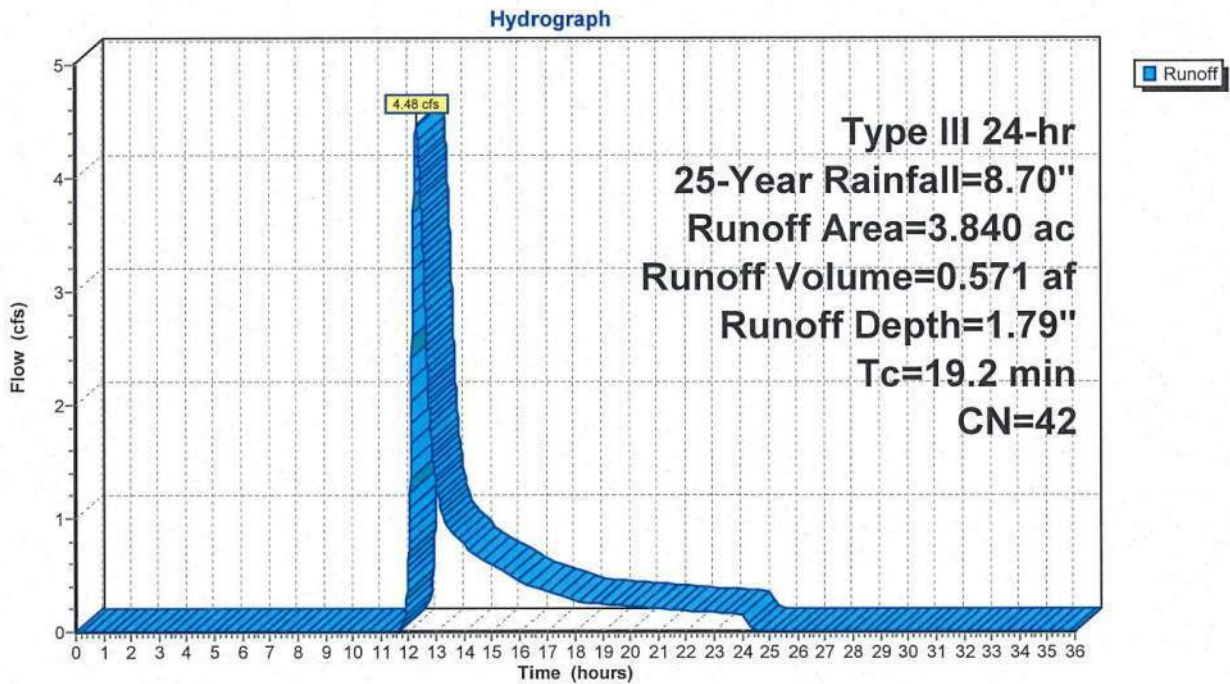
Runoff = 4.48 cfs @ 12.31 hrs, Volume= 0.571 af, Depth= 1.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 3.840	42	
3.840		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.2					Direct Entry,

**Subcatchment PB2: PB2**



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB3: PB3**

Runoff = 5.49 cfs @ 12.46 hrs, Volume= 0.837 af, Depth= 1.57"

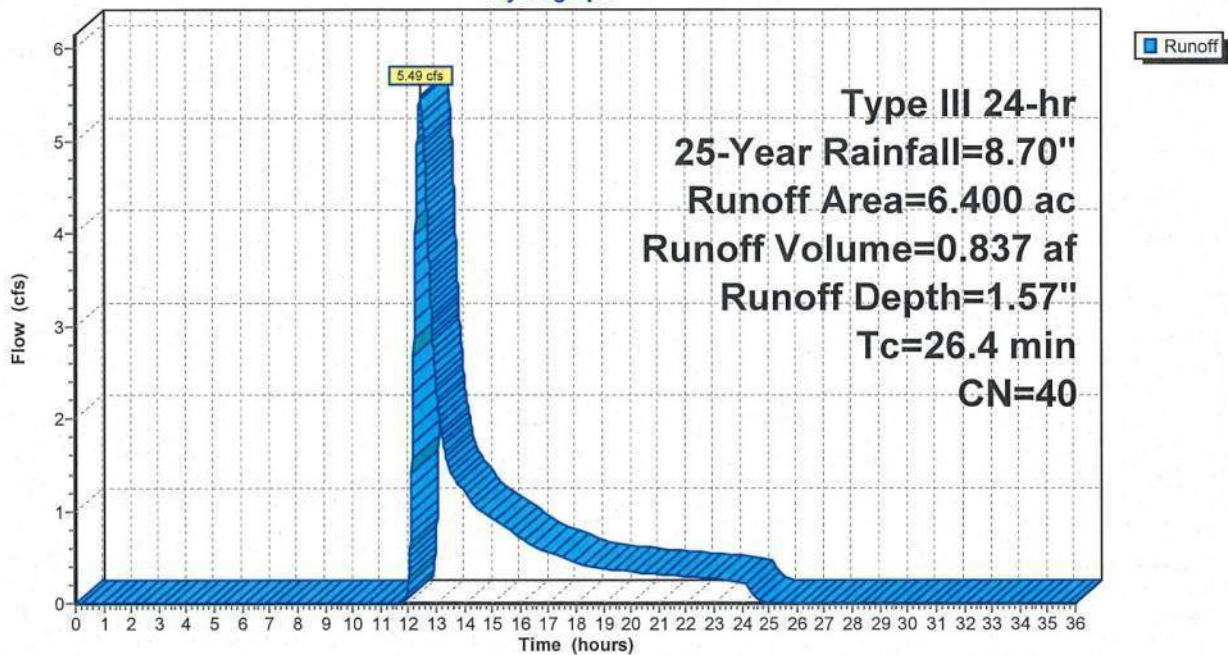
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 6.400	40	
6.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
26.4					Direct Entry,

**Subcatchment PB3: PB3**

Hydrograph



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC1: PC1**

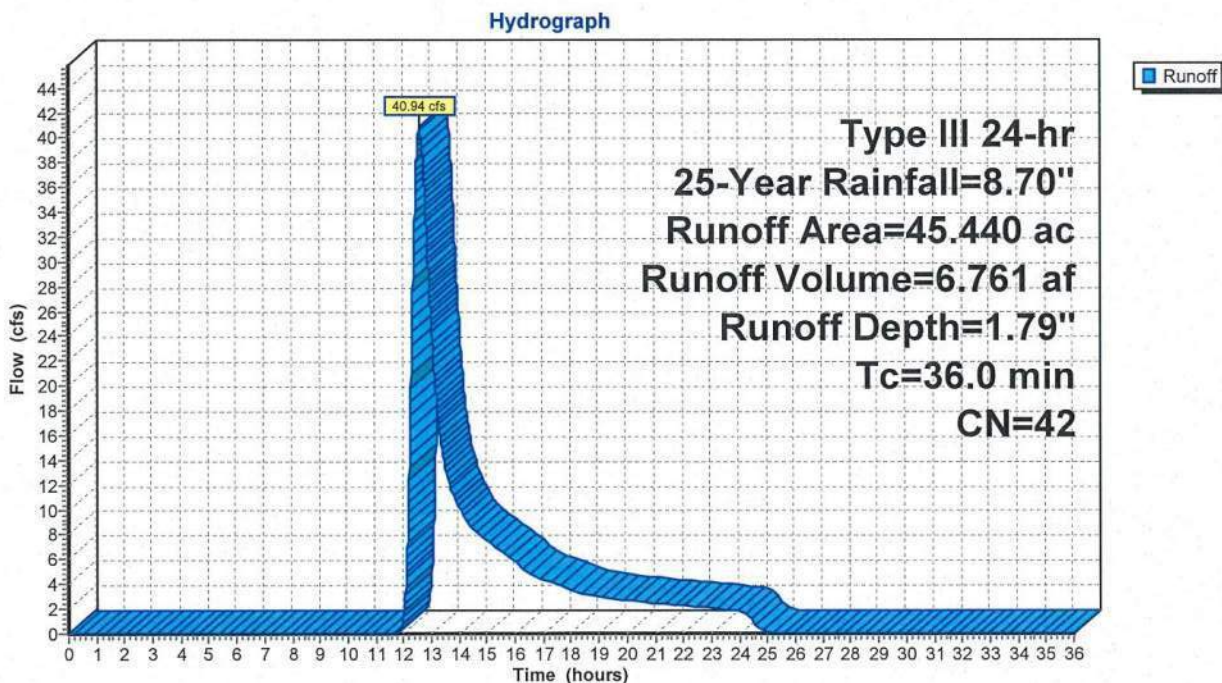
Runoff = 40.94 cfs @ 12.60 hrs, Volume= 6.761 af, Depth= 1.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 45.440	42	
45.440		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
36.0					Direct Entry,

**Subcatchment PC1: PC1**



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC2: PC2**

Runoff = 17.12 cfs @ 12.26 hrs, Volume= 1.875 af, Depth= 2.34"

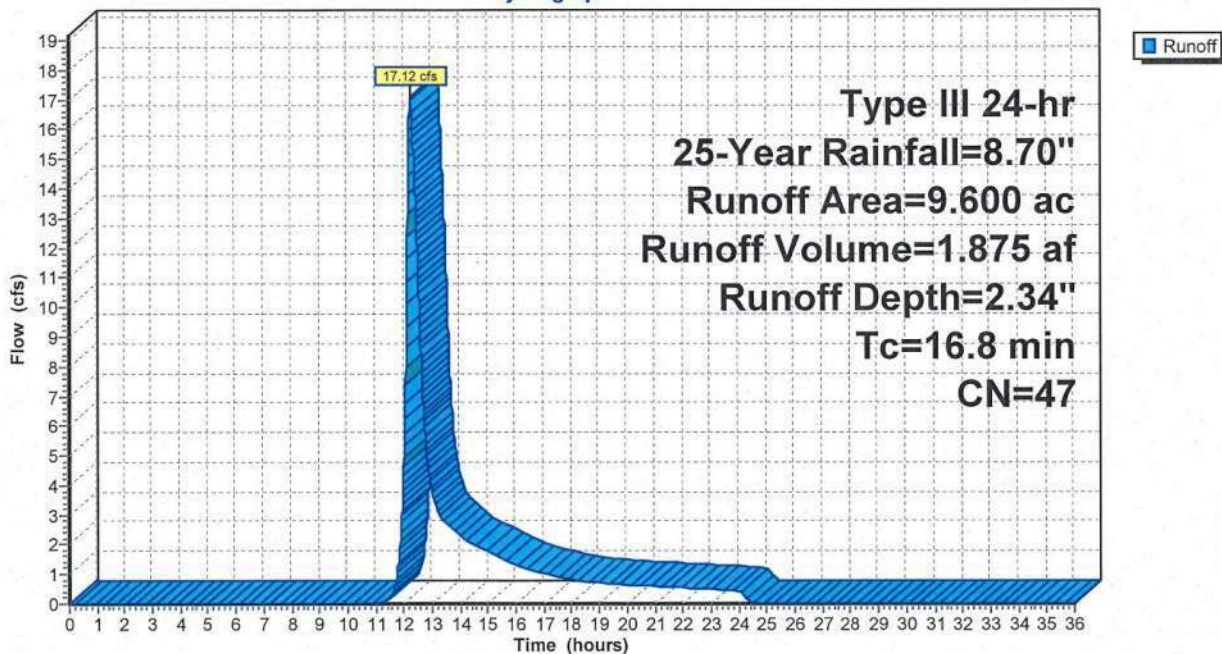
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 9.600	47	
9.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.8					Direct Entry,

**Subcatchment PC2: PC2**

Hydrograph



**PreDevelopment Existing 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC3: PC3**

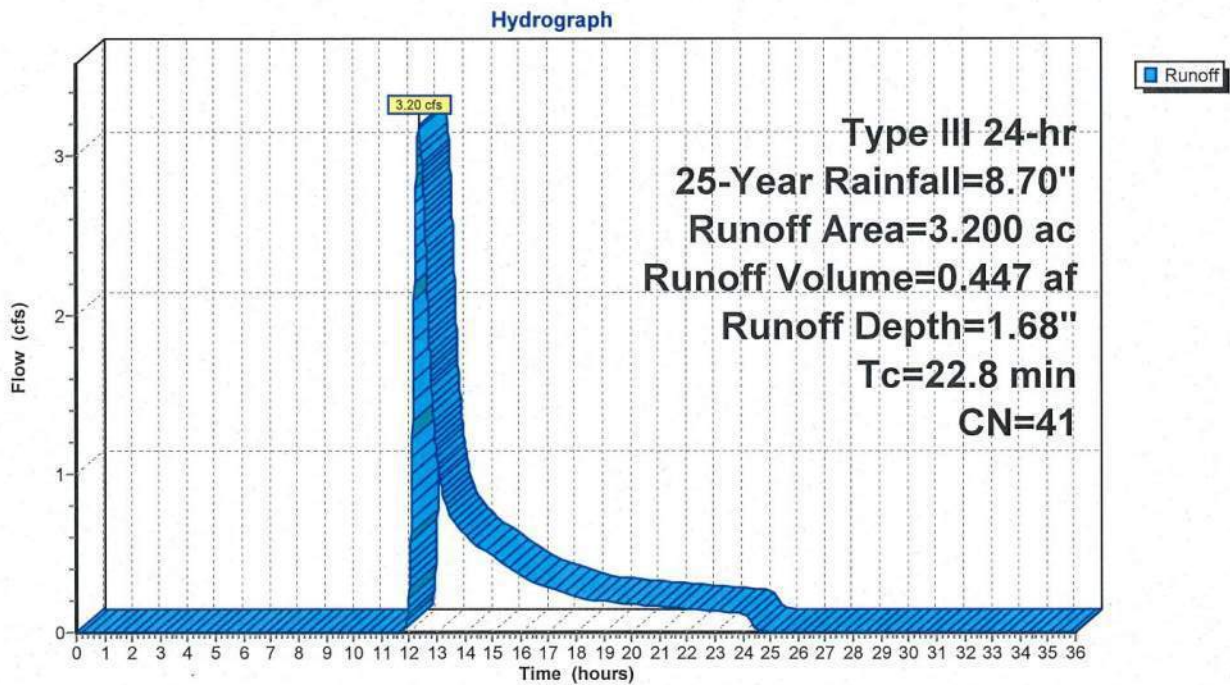
Runoff = 3.20 cfs @ 12.39 hrs, Volume= 0.447 af, Depth= 1.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

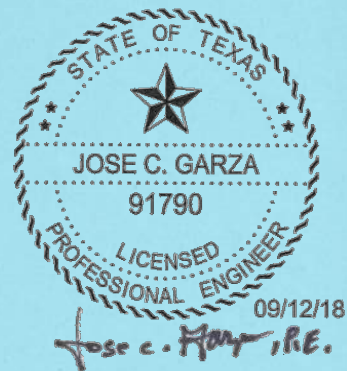
Area (ac)	CN	Description
* 3.200	41	
3.200		100.00% Pervious Area

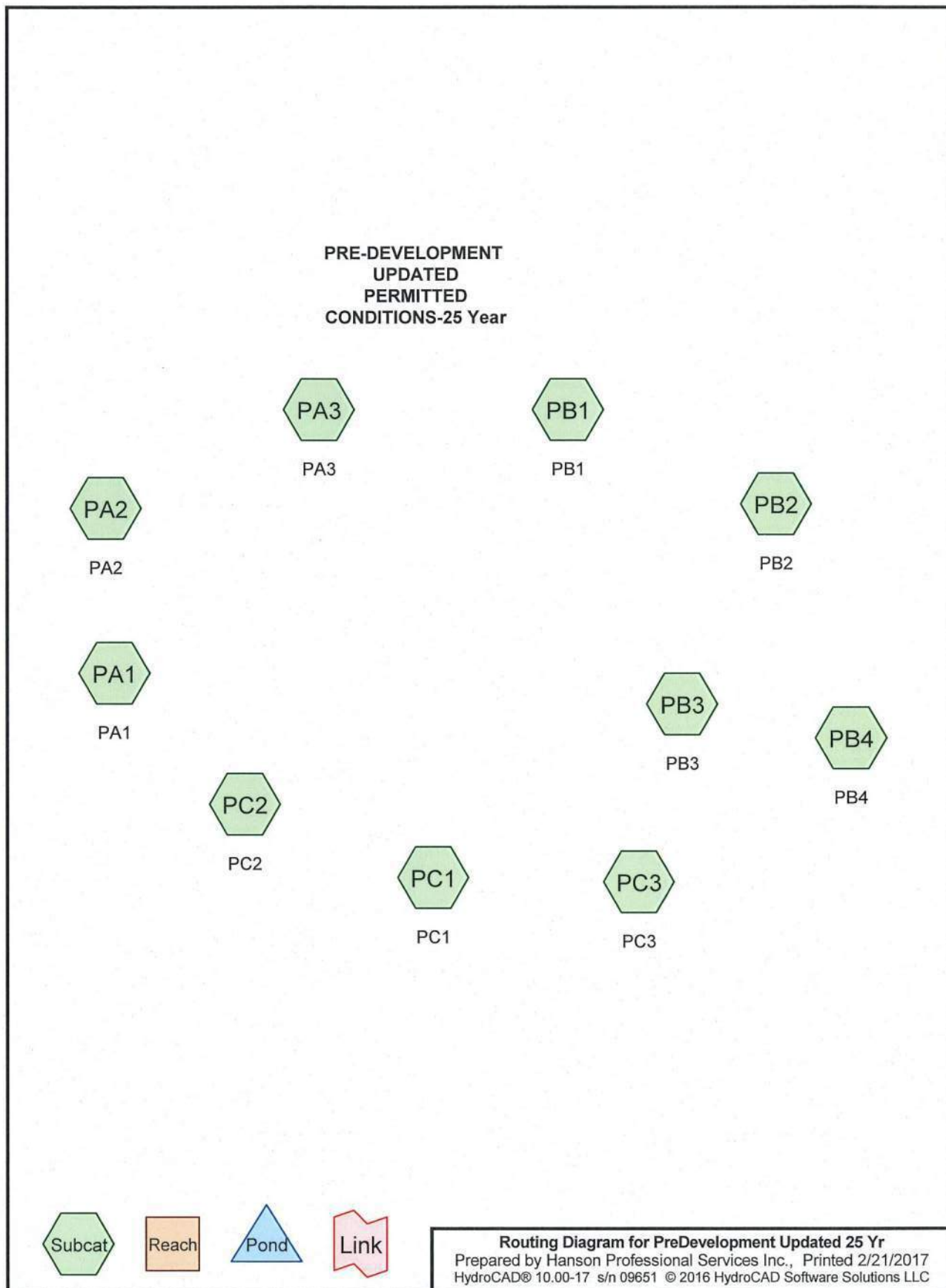
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
22.8					Direct Entry,

**Subcatchment PC3: PC3**



**APPENDIX 6A.2.5**  
**HYDROCAD MODEL PRE-DEVELOPMENT CONDITIONS 25 YEAR**  
**UPDATED PERMITTED CONDITIONS**







**PreDevelopment Updated 25 Yr**

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
19.840	46	(PA1)
97.220	40	(PA2, PA3, PB1, PB3, PB4)
49.280	42	(PB2, PC1)
9.600	47	(PC2)
3.200	41	(PC3)
<b>179.140</b>	<b>42</b>	<b>TOTAL AREA</b>

**PreDevelopment Updated 25 Yr**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
179.140	Other	PA1, PA2, PA3, PB1, PB2, PB3, PB4, PC1, PC2, PC3
<b>179.140</b>		<b>TOTAL AREA</b>

**PreDevelopment Updated 25 Yr**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.000	0.000	179.140	179.140		PA1, PA2, PA3, PB1, PB2, PB3, PB4, PC1, PC2, PC3
<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>0.000</b>	<b>179.140</b>	<b>179.140</b>	<b>TOTAL AREA</b>	

**PreDevelopment Updated 25 Yr**

*Type III 24-hr 25-Year Rainfall=8.70"*

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Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment PA1: PA1</b>	Runoff Area=19.840 ac 0.00% Impervious Runoff Depth=2.23" Tc=24.0 min CN=46 Runoff=28.74 cfs 3.688 af
<b>Subcatchment PA2: PA2</b>	Runoff Area=32.000 ac 0.00% Impervious Runoff Depth=1.57" Tc=41.4 min CN=40 Runoff=22.31 cfs 4.186 af
<b>Subcatchment PA3: PA3</b>	Runoff Area=19.200 ac 0.00% Impervious Runoff Depth=1.57" Tc=38.4 min CN=40 Runoff=13.91 cfs 2.511 af
<b>Subcatchment PB1: PB1</b>	Runoff Area=26.240 ac 0.00% Impervious Runoff Depth=1.57" Tc=36.6 min CN=40 Runoff=19.49 cfs 3.432 af
<b>Subcatchment PB2: PB2</b>	Runoff Area=3.840 ac 0.00% Impervious Runoff Depth=1.79" Tc=19.2 min CN=42 Runoff=4.48 cfs 0.571 af
<b>Subcatchment PB3: PB3</b>	Runoff Area=6.400 ac 0.00% Impervious Runoff Depth=1.57" Tc=26.4 min CN=40 Runoff=5.49 cfs 0.837 af
<b>Subcatchment PB4: PB4</b>	Runoff Area=13.380 ac 0.00% Impervious Runoff Depth=1.57" Tc=15.6 min CN=40 Runoff=13.85 cfs 1.750 af
<b>Subcatchment PC1: PC1</b>	Runoff Area=45.440 ac 0.00% Impervious Runoff Depth=1.79" Tc=36.0 min CN=42 Runoff=40.94 cfs 6.761 af
<b>Subcatchment PC2: PC2</b>	Runoff Area=9.600 ac 0.00% Impervious Runoff Depth=2.34" Tc=16.8 min CN=47 Runoff=17.12 cfs 1.875 af
<b>Subcatchment PC3: PC3</b>	Runoff Area=3.200 ac 0.00% Impervious Runoff Depth=1.68" Tc=22.8 min CN=41 Runoff=3.20 cfs 0.447 af

**Total Runoff Area = 179.140 ac Runoff Volume = 26.059 af Average Runoff Depth = 1.75"**  
**100.00% Pervious = 179.140 ac 0.00% Impervious = 0.000 ac**

**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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Page 6

**Summary for Subcatchment PA1: PA1**

Runoff = 28.74 cfs @ 12.38 hrs, Volume= 3.688 af, Depth= 2.23"

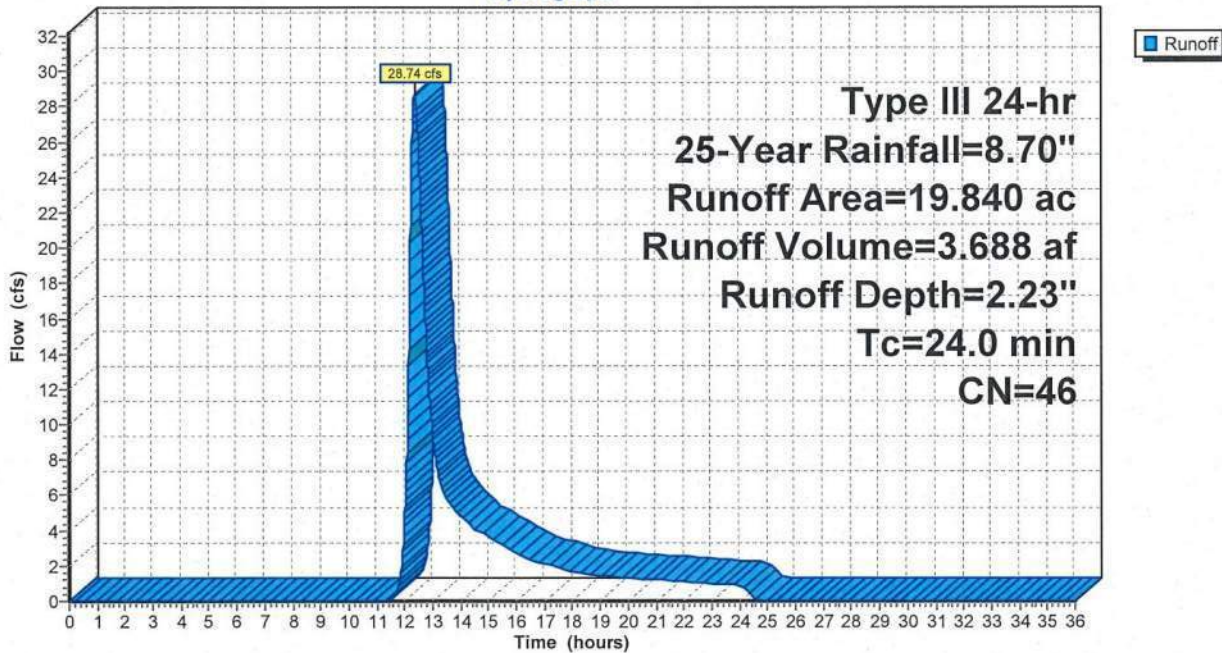
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 19.840	46	
19.840		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
24.0					Direct Entry,

**Subcatchment PA1: PA1**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PA2: PA2**

Runoff = 22.31 cfs @ 12.69 hrs, Volume= 4.186 af, Depth= 1.57"

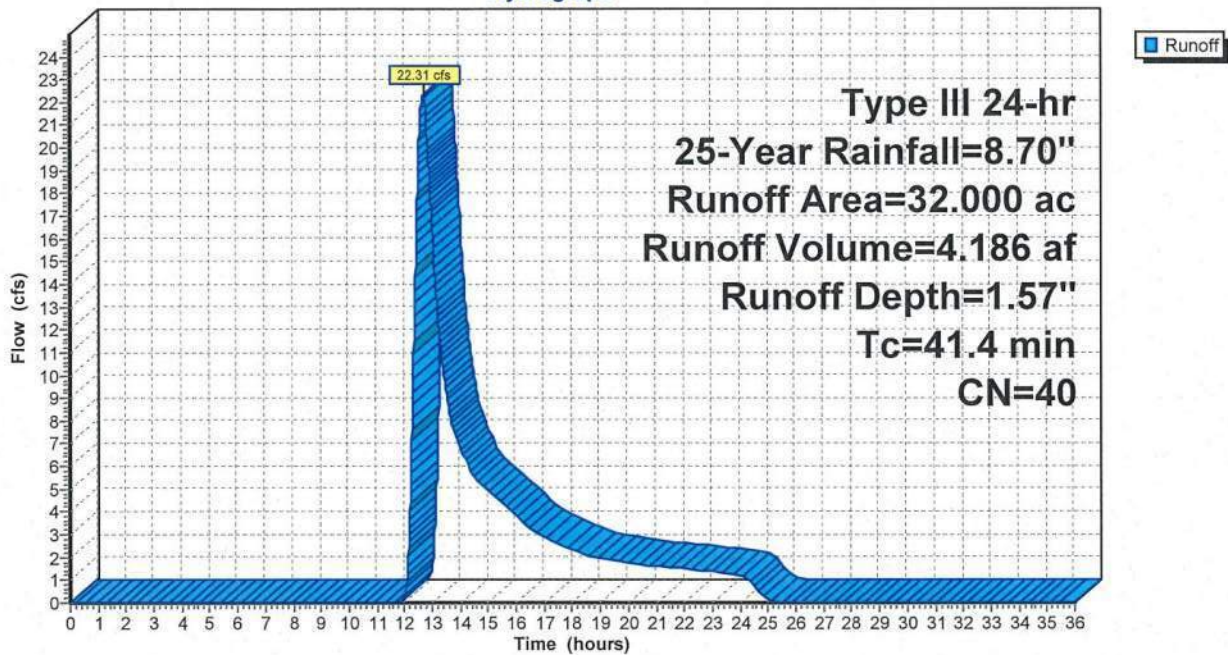
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 32.000	40	
32.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
41.4					Direct Entry,

**Subcatchment PA2: PA2**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PA3: PA3**

Runoff = 13.91 cfs @ 12.64 hrs, Volume= 2.511 af, Depth= 1.57"

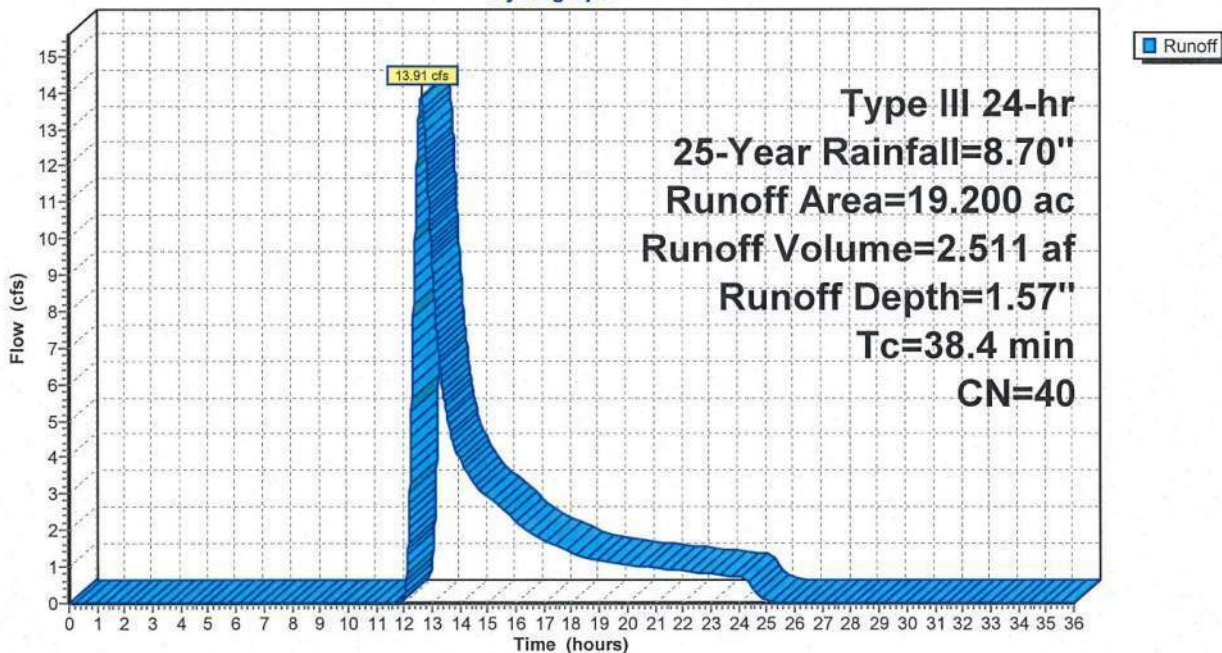
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 19.200	40	
19.200		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
38.4					Direct Entry, Direct Entry

**Subcatchment PA3: PA3**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB1: PB1**

Runoff = 19.49 cfs @ 12.61 hrs, Volume= 3.432 af, Depth= 1.57"

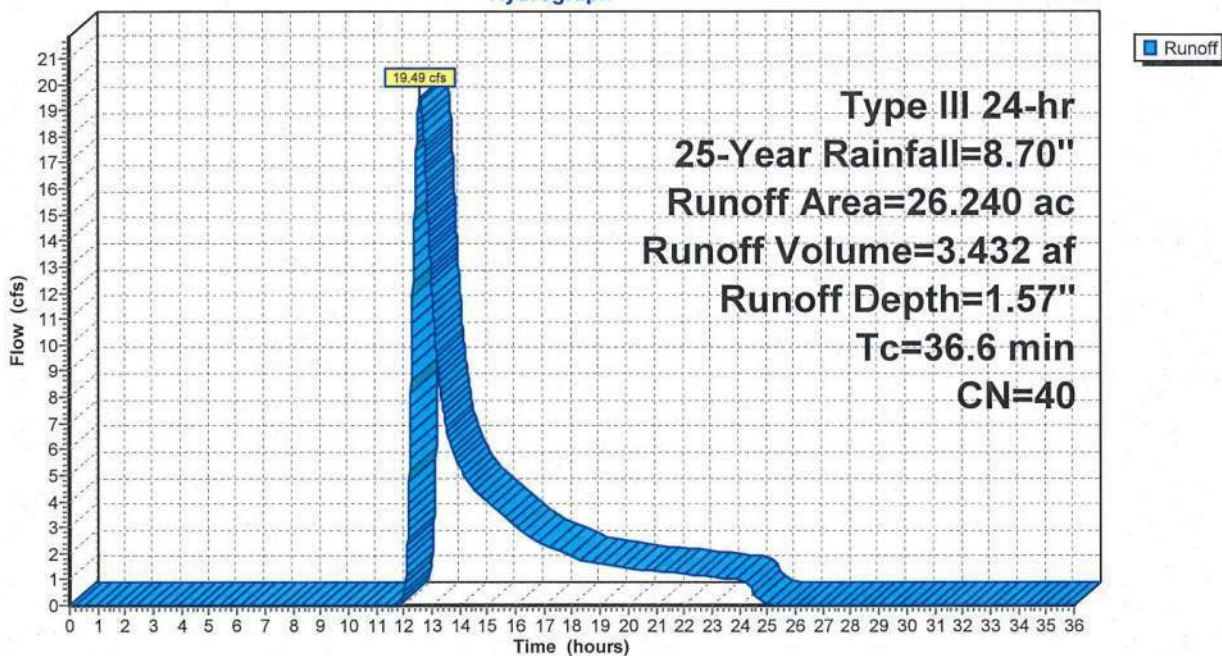
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 26.240	40	
26.240		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
36.6					Direct Entry,

**Subcatchment PB1: PB1**

Hydrograph





**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB2: PB2**

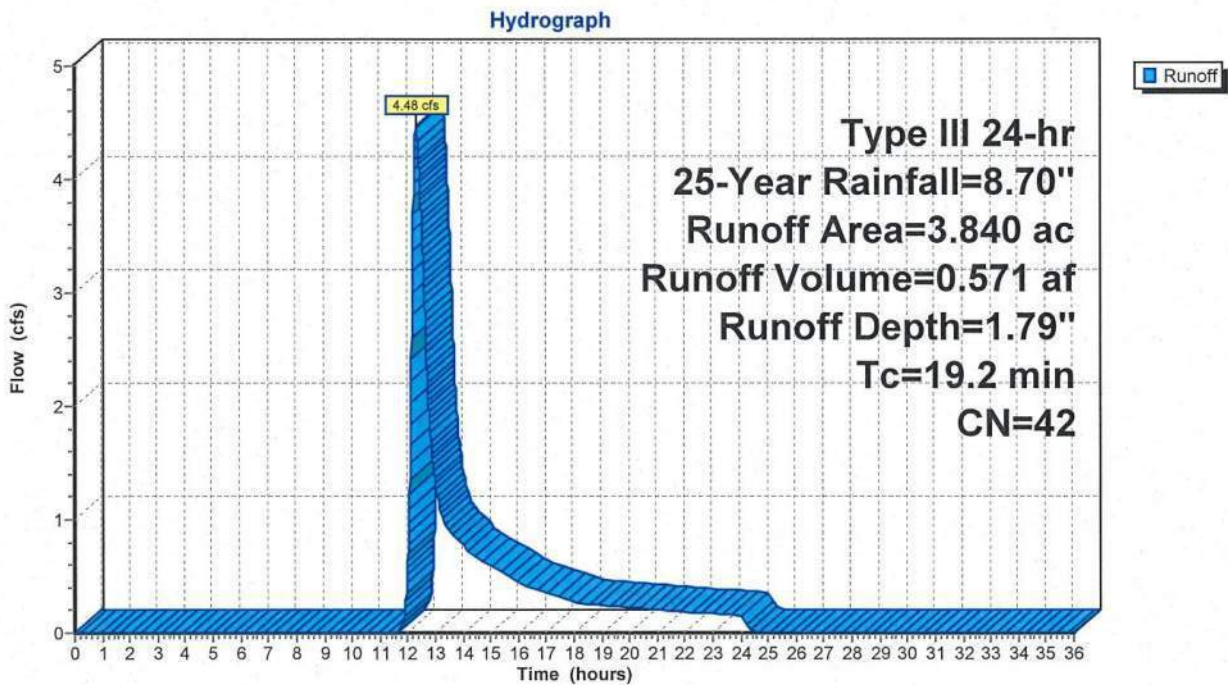
Runoff = 4.48 cfs @ 12.31 hrs, Volume= 0.571 af, Depth= 1.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 3.840	42	
3.840		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
19.2					Direct Entry,

**Subcatchment PB2: PB2**



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB3: PB3**

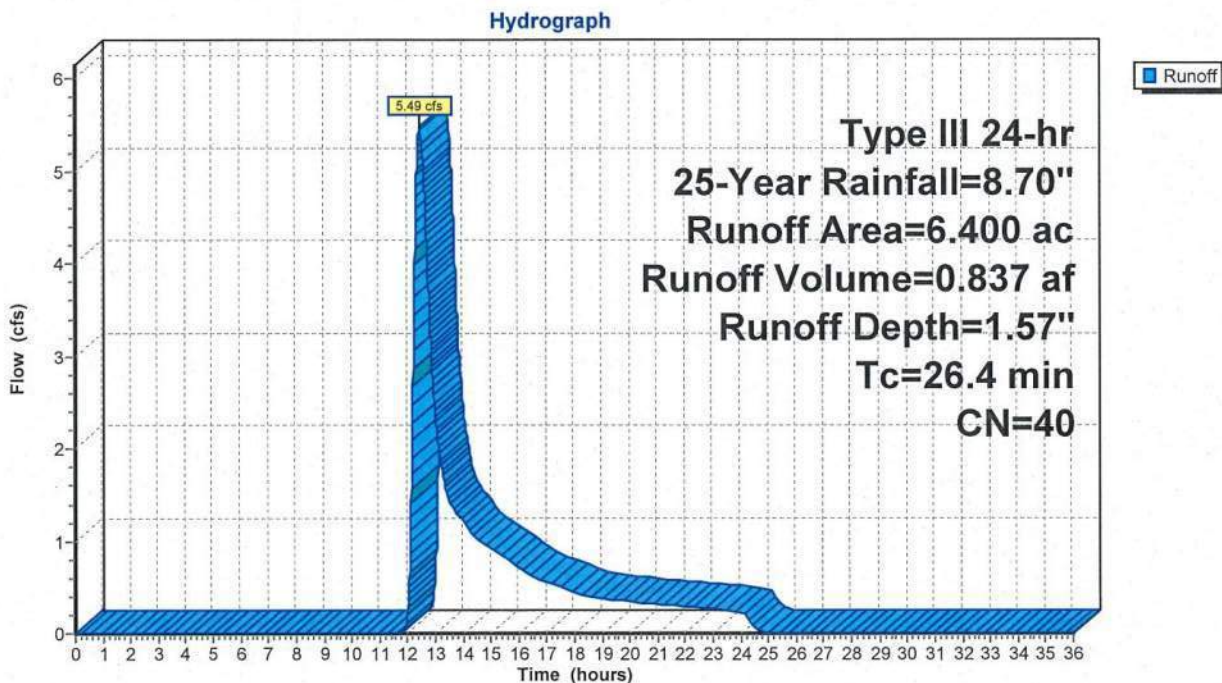
Runoff = 5.49 cfs @ 12.46 hrs, Volume= 0.837 af, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 6.400	40	
6.400		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
26.4					Direct Entry,

**Subcatchment PB3: PB3**



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PB4: PB4**

Runoff = 13.85 cfs @ 12.26 hrs, Volume= 1.750 af, Depth= 1.57"

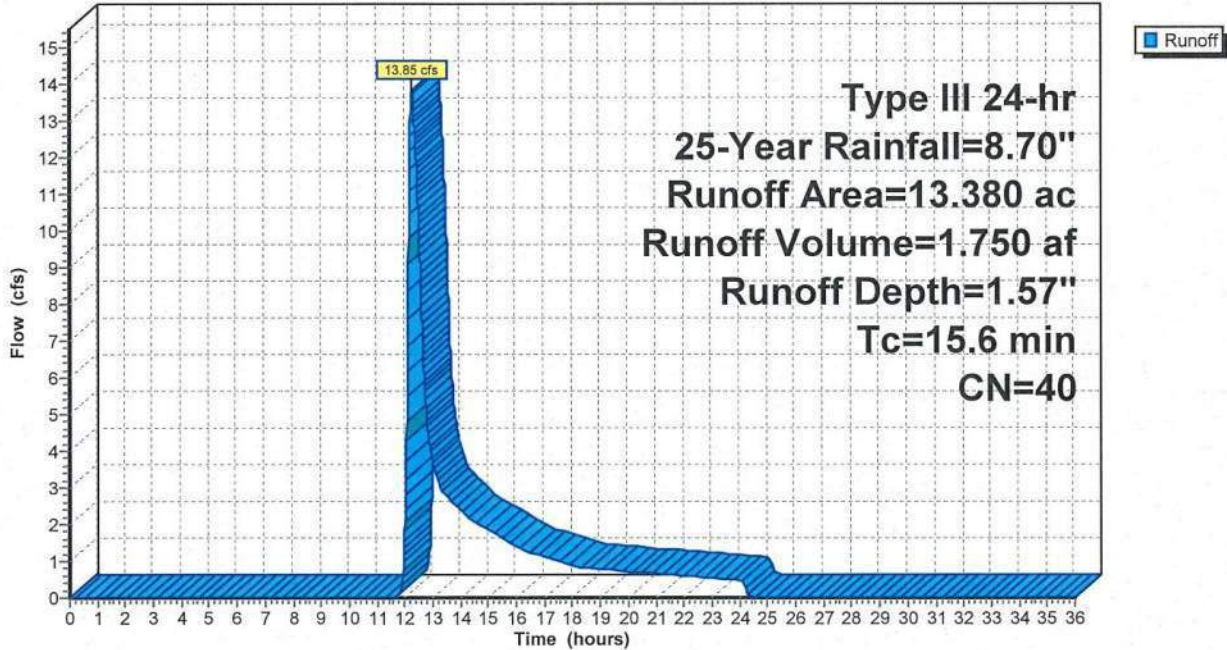
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 13.380	40	
13.380		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
15.6					Direct Entry,

**Subcatchment PB4: PB4**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC1: PC1**

Runoff = 40.94 cfs @ 12.60 hrs, Volume= 6.761 af, Depth= 1.79"

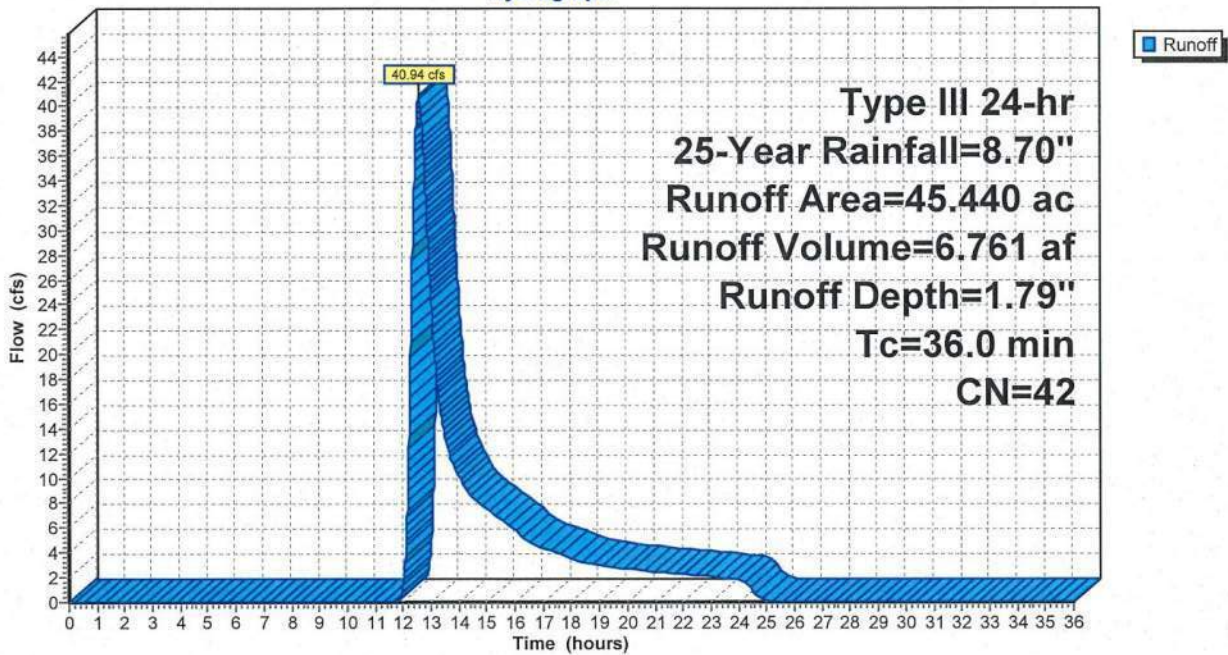
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 45.440	42	
45.440		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
36.0					Direct Entry,

**Subcatchment PC1: PC1**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC2: PC2**

Runoff = 17.12 cfs @ 12.26 hrs, Volume= 1.875 af, Depth= 2.34"

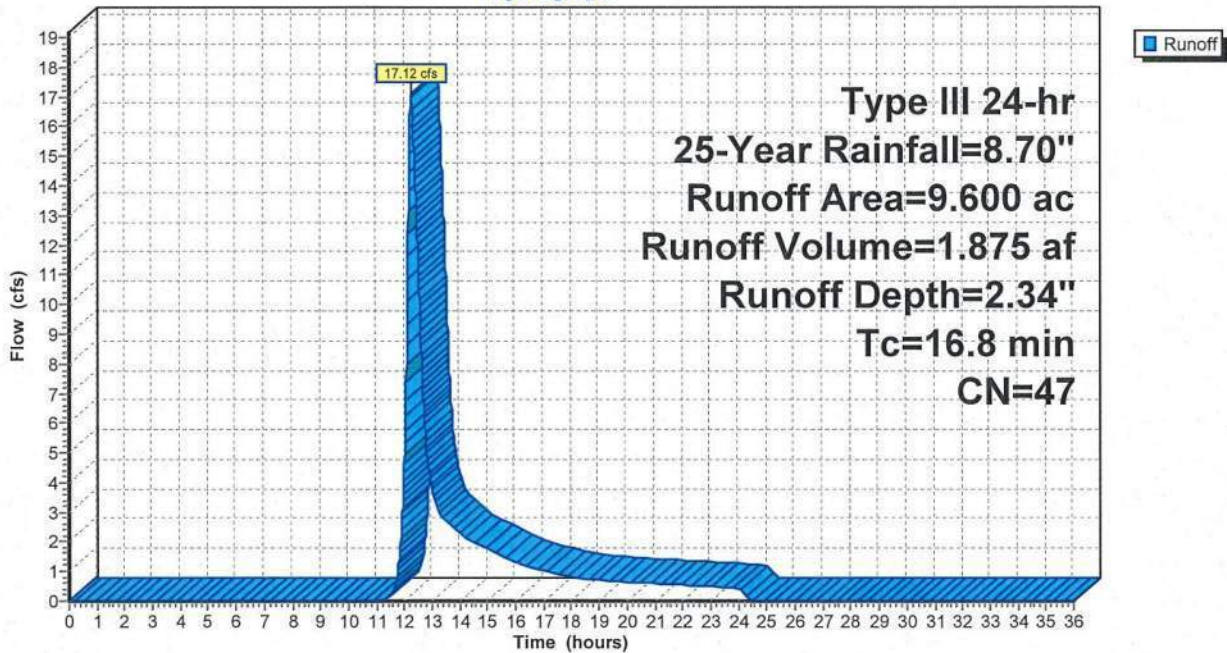
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 9.600	47	
9.600		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
16.8					Direct Entry,

**Subcatchment PC2: PC2**

Hydrograph



**PreDevelopment Updated 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PC3: PC3**

Runoff = 3.20 cfs @ 12.39 hrs, Volume= 0.447 af, Depth= 1.68"

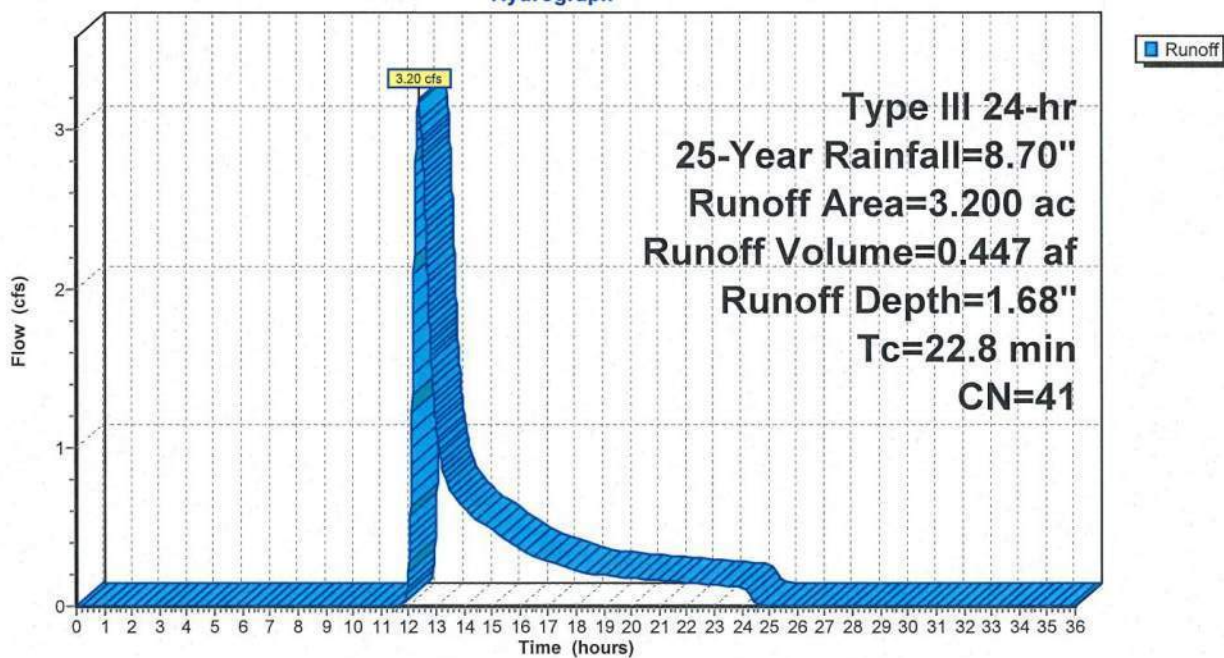
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
* 3.200	41	
3.200		100.00% Pervious Area

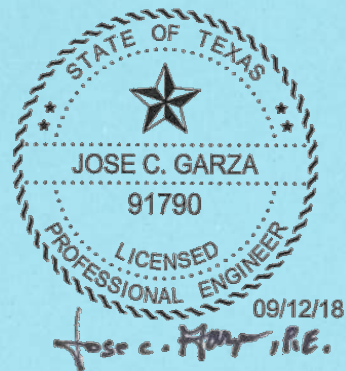
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
22.8					Direct Entry,

**Subcatchment PC3: PC3**

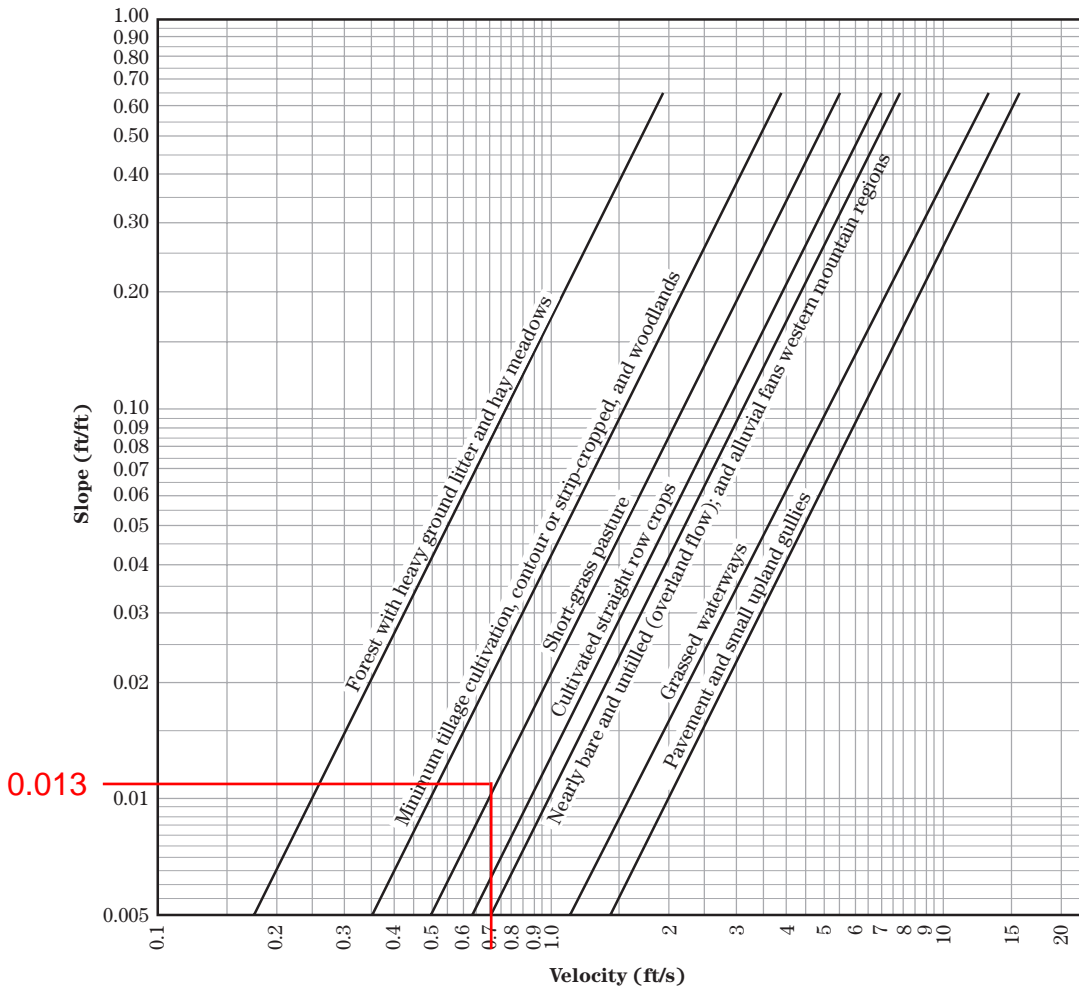
Hydrograph



APPENDIX 6A.2.6  
NATIONAL ENGINEERING HANDBOOK (NEH), CHAPTER 15, FIGURE  
15-4 VELOCITY VERSUS SLOPE FOR SHALLOW CONCENTRATED  
FLOW [ANNOTATED]



**Figure 15-4** Velocity versus slope for shallow concentrated flow



**PB4**

Elev 60 ft → Elev 50 ft  
 $s = 10 \text{ ft} / 750 \text{ ft} = 0.013$

**0.80**

$t_c = 750 \text{ ft} / 0.80 \text{ ft/sec} = 937.5 \text{ sec}$

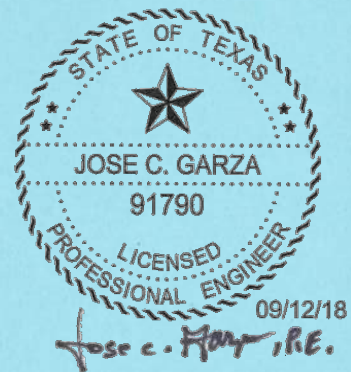
$t_c = 937.5 \text{ sec} / 60 \text{ sec/min} = 15.6 \text{ min}$

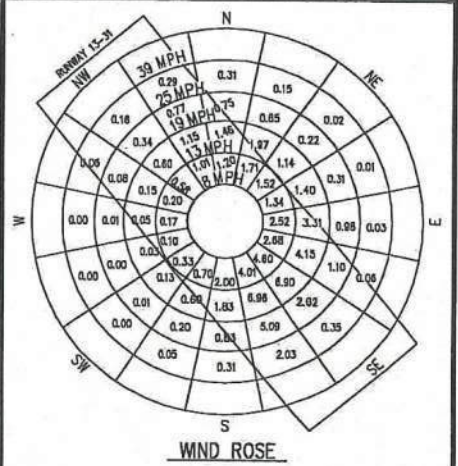
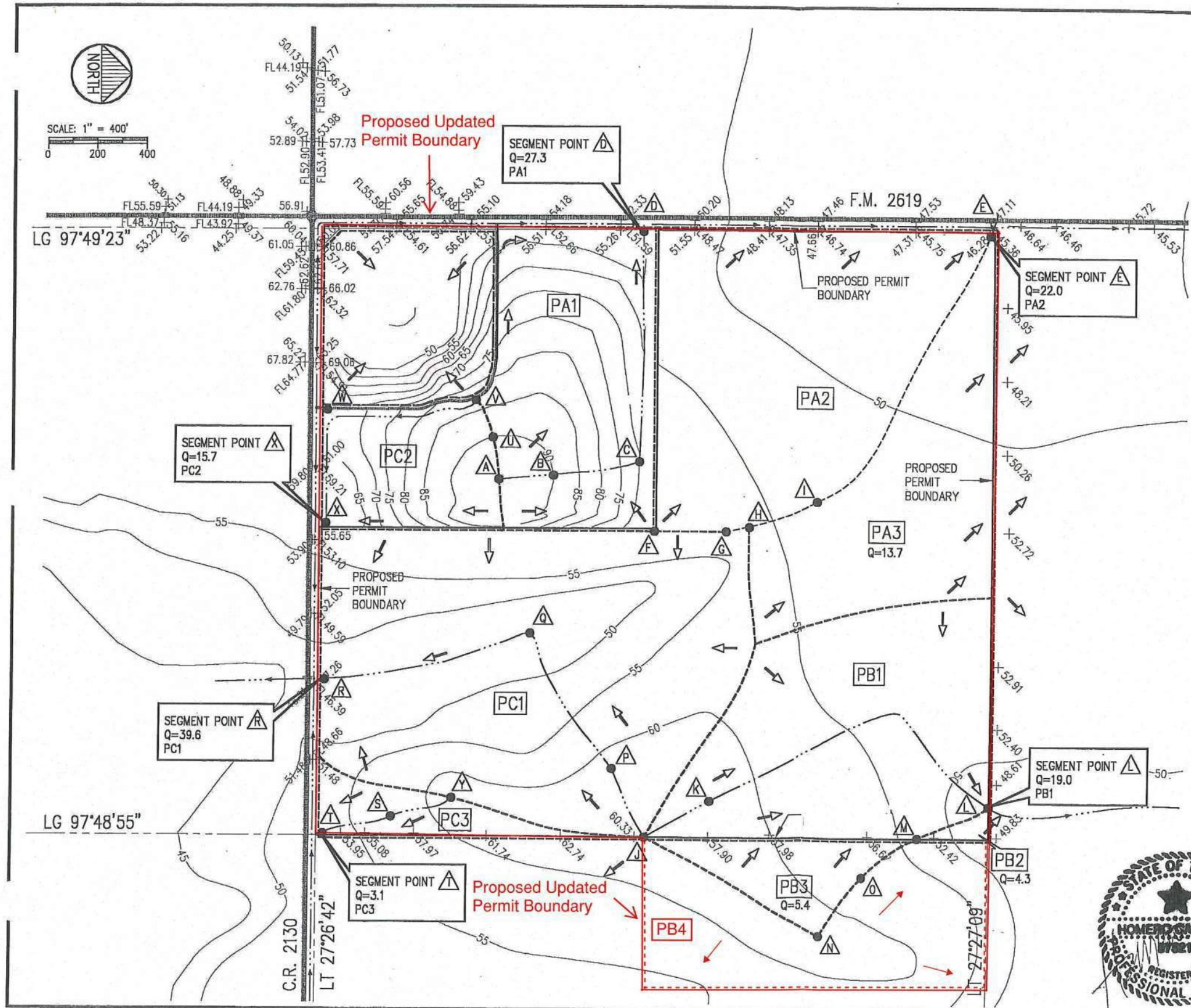
**Table 15-3** Equations and assumptions developed from figure 15-4

Flow type	Depth (ft)	Manning's <i>n</i>	Velocity equation (ft/s)
Pavement and small upland gullies	0.2	0.025	$V = 20.328(s)^{0.5}$
Grassed waterways	0.4	0.050	$V = 16.135(s)^{0.5}$
Nearly bare and untilled (overland flow); and alluvial fans in western mountain regions	0.2	0.051	$V = 9.965(s)^{0.5}$
Cultivated straight row crops	0.2	0.058	$V = 8.762(s)^{0.5}$
Short-grass pasture	0.2	0.073	$V = 6.962(s)^{0.5}$
Minimum tillage cultivation, contour or strip-cropped, and woodlands	0.2	0.101	$V = 5.032(s)^{0.5}$
Forest with heavy ground litter and hay meadows	0.2	0.202	$V = 2.516(s)^{0.5}$



**APPENDIX 6A.2.7**  
**PRE-DEVELOPMENT DRAINAGE MAP SOLID WASTE LANDFILL**  
**PERMIT 235-B AMENDMENT FIGURE A-1 (UPDATED PERMITTED**  
**CONDITIONS)**





**LEGEND**

LG	LONGITUDE MEASUREMENT
LT	LATITUDE MEASUREMENT
△	SEGMENT POINT
---	TIME OF CONCENTRATION ROUTE/FLOW LINE
---	DRAINAGE AREA BOUNDARY LINE
PA2	PRE-DEVELOPMENT DRAINAGE AREA NAME
50	ALL CONTOURS ARE FEET ABOVE MEAN SEA LEVEL
Q=27.3	25-YR STORM RUNOFF PEAK FLOW (CFS)

REVISION

NEW SHEET

**PRE-DEVELOPMENT DRAINAGE MAP**  
 SOLID WASTE LANDFILL PERMIT 235-B AMENDMENT

CITY OF KINGSVILLE  
 200 EAST KLEBERG

KINGSVILLE, TEXAS 78363

**ALPHA ENGINEERING**  
 109 NORTH FIFTH STREET  
 KINGSVILLE, TEXAS 78363  
 HOMERO CASTILLO, PE (512) 692-2977

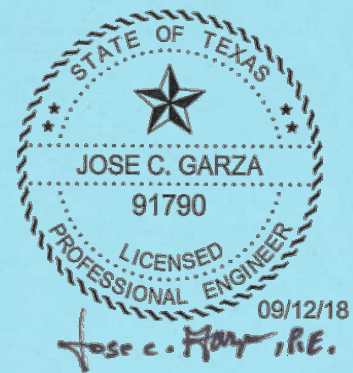
PROJECT NO. 9708-01  
 DRAWN BY D.S.  
 DESIGNED BY HOMERO C.  
 CHECKED BY HOMERO C.  
 DATE 05 JUN 98

SCALE: 1"=400'-0"  
 APPENDIX 6A  
 FIGURE A-1

THIS DOCUMENT FOR PERMIT PURPOSES ONLY

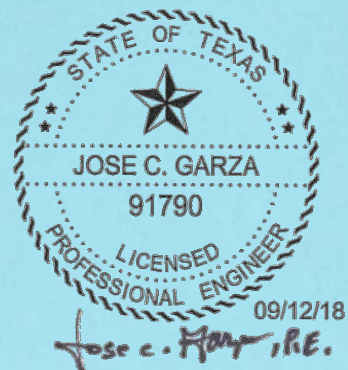


APPENDIX 6B  
SITE POST-DEVELOPMENT CONDITIONS



APPENDIX 6B.1

USGS ATLAS OF DEPTH-DURATION FREQUENCY OF  
PRECIPITATION ANNUAL MAXIMA FOR TEXAS-DEPTH OF  
PRECIPITATION FOR 25 YR-24 HR & 100 YR-24 HR [ANNOTATED]





**In cooperation with the Texas Department of Transportation**

# **Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas**



Scientific Investigations Report 2004–5041  
(TxDOT Implementation Report 5–1301–01–1)

**U.S. Department of the Interior  
U.S. Geological Survey**

Technical Report Documentation Page

1. Report No. FHWA/FX-04/5-1301-01-1		2. Government Accession No.		3. Recipient's Catalog No.	
4. Title and Subtitle ATLAS OF DEPTH-DURATION FREQUENCY OF PRECIPITATION ANNUAL MAXIMA FOR TEXAS				5. Report Date June 2004	
				6. Performing Organization Code	
7. Author(s) William H. Asquith and Meghan C. Rousset				8. Performing Organization Report No. SIR 2004-5041	
9. Performing Organization Name and Address U.S. Geological Survey Water Resources Division 8027 Exchange Drive Austin, Texas 78754				10. Work Unit No. (TRAIS)	
				11. Contract or Grant No. Project 5-1301	
12. Sponsoring Agency Name and Address Texas Department of Transportation Research and Technology Implementation Office 4000 Jackson Ave., Bldg. 1 P.O. Box 5080 Austin, TX 78731				13. Type of Report and Period Covered Research from 2003 to 2004	
				14. Sponsoring Agency Code	
15. Supplementary Notes Project conducted in cooperation with the Texas Department of Transportation and the Federal Highway Administration.					
16. Abstract Ninety-six maps depicting the spatial variation of the depth-duration frequency of precipitation annual maxima for Texas are presented. The recurrence intervals represented are 2, 5, 10, 25, 50, 100, 250, and 500 years. The storm durations represented are 15 and 30 minutes; 1, 2, 3, 6, and 12 hours; and 1, 2, 3, 5, and 7 days. The maps were derived using geographically referenced parameter maps of probability distributions used in previously published research by the U.S. Geological Survey to model the magnitude and frequency of precipitation annual maxima for Texas. The maps in this report apply that research and update depth-duration frequency of precipitation maps available in earlier studies performed by the National Weather Service.					
17. Key Words Precipitation, Depth duration frequency, Annual precipitation maxima, L-moments, Texas				18. Distribution Statement No restrictions.	
19. Security Classif. (of report) Unclassified		20. Security Classif. (of this page) Unclassified		21. No. of pages 106	22. Price \$4.00

Form DOT F 1700.7 (8-72)

Reproduction of completed page authorized

**Cover:**

West Sister Creek near Sisterdale, Texas, on FM 473, Kendall County, May 10, 2004.

# **Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas**

By William H. Asquith and Meghan C. Roussel

In cooperation with the Texas Department of Transportation

Scientific Investigations Report 2004-5041  
(TxDOT Implementation Report 5-1301-01-1)

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54 Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas

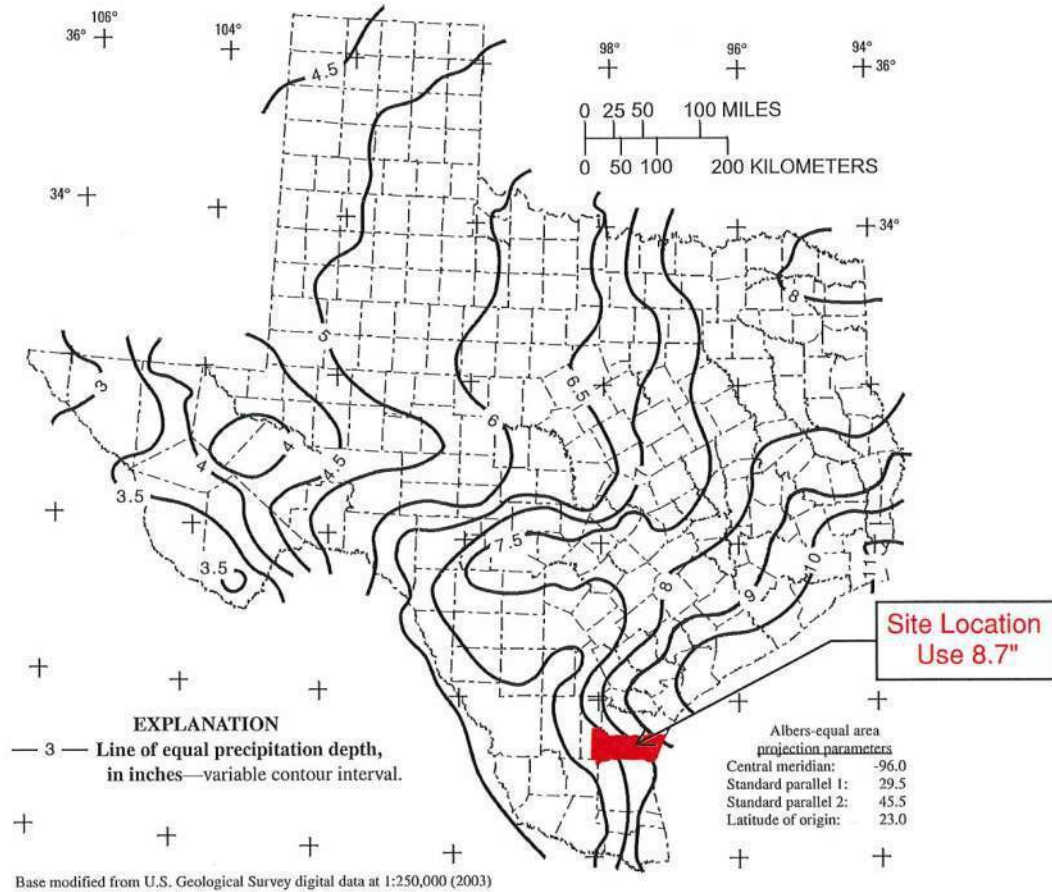


Figure 47. Depth of precipitation for 25-year storm for 1-day duration in Texas.

78 Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas

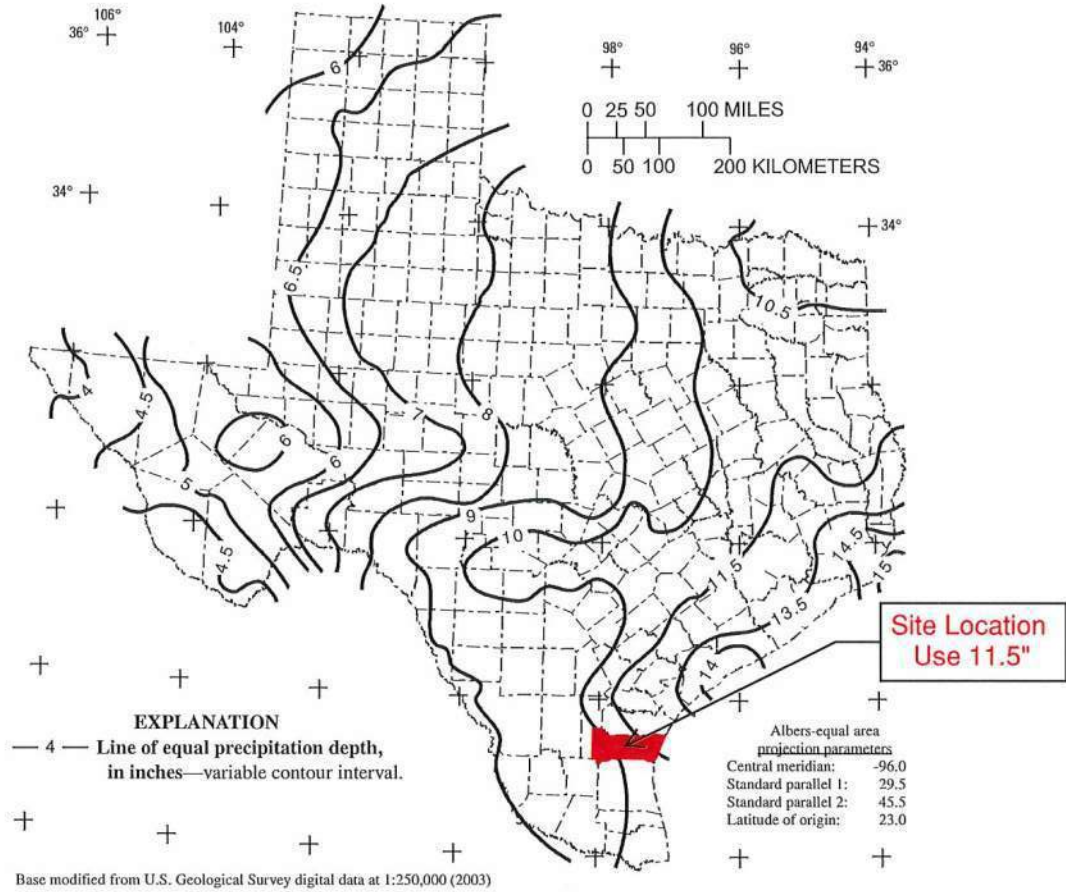


Figure 71. Depth of precipitation for 100-year storm for 1-day duration in Texas.

APPENDIX 6B.2

TABLE 6B-1 HYDROLOGIC SOIL GROUPS FOR ON-SITE SOILS  
(FROM NRCS, 2015) AND CITY OF KINGSVILLE MUNICIPAL SOLID  
WASTE LANDFILL FINAL DRAINAGE AREAS

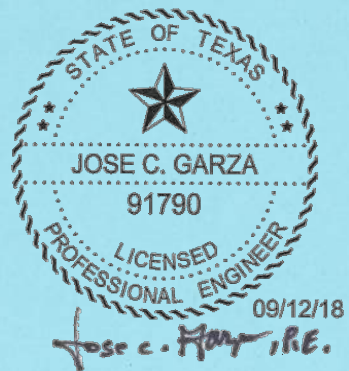


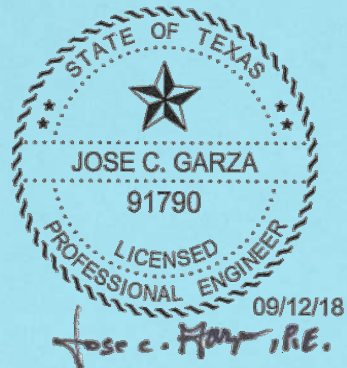
Table 6B-1. Hydrologic Soil Groups for On-Site Soils  
 (From NRCS, 2015)

Map Symbol and Soil Name	Percent of AOI	Pct of Map Unit	Slope Length (ft)	Hydrologic Soil Group	Kf	T Factor	Representative Value	
							% Sand	% Silt
CkA - Clareville Clay Loam 0 to 1 percent slopes	10.7	50	98	C	0.24	5	33.5	16.5
CmkA - Odintsa Fine Sandy Loam 0 to 1 percent slopes	9.3	50	98	B	0.2	5	66.1	19.9
BT - Pine Quarry	80.0	-	-	-	-	-	-	-

City of Kingsville Municipal Solid Waste Landfill Final Drainage Areas

Drainage Area Designation	Area (Acres)
A1T	7.425
A1S	8.009
A2T	5.120
A2S	12.241
A3T	7.488
A3S	10.760
B1T	7.499
B1S	14.894
B2T	4.309
B2S	8.806
C1T	6.252
C1S	11.506
C2T	5.249
C2S	10.038
C3	3.500
C4	9.500
C5	2.680
C6	3.982
1C	1.000
2C	1.480
3C	1.640
4C	0.910
5C	1.000
6C	1.000
7C	1.00
PAR	7.440
PBR	4.290
PCR	4.540
C1SN1	0.250
C1SN2	0.250
C1SS1	0.250
C1SS2	0.250
<b>Total</b>	<b>164.60</b>

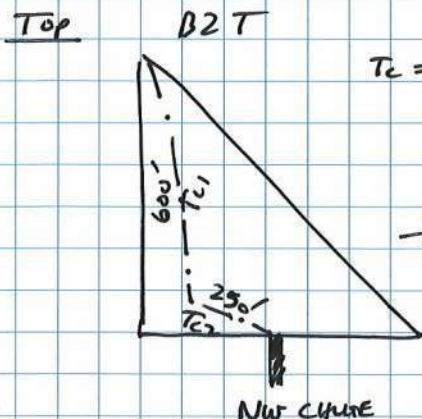
APPENDIX 6B.3  
PERMIT AMENDMENT-POST DEVELOPMENT-TOP DRAINAGE  
AREAS/SLOPES HYDROCAD (T<sub>c</sub>-TIME OF CONCENTRATION) INPUT  
DATA



FOR PERMIT PURPOSES ONLY



JOB NO. 8514-03 City of Kingsville Landfill	SHEET NO. 1 of 2
DESCRIPTION Permit Amendment - Post Development - Top Orange Area / Slopes	DATE 8/26/18
HydroCAD - T <sub>c</sub> (Time of Concentration) Input Data	BY JCG



$$T_c = \frac{T_{c1}}{1.3 \text{ ft/sec}} + \frac{T_{c2}}{0.7 \text{ ft/sec}} = 818.68 \text{ sec}$$

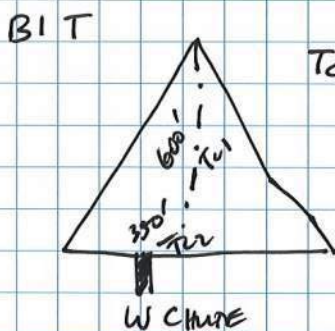
$$461.54 \text{ sec} + 357.14 \text{ sec} \Rightarrow \frac{818.68 \text{ sec}}{60 \text{ sec/min}} \Rightarrow 13.64 \text{ min}$$

→ Overland flow @ 4% Slope  
 TO DIVERSION BERM @ 1% Slope  
 TO CHAURE

Slopes

B2S USE CONSERVATIVE  
 VALUE OF T<sub>c</sub> = 10min

→ WATER BEING DIVERTED  
 TO CHAURES BY  
 DIVERSION BERMS



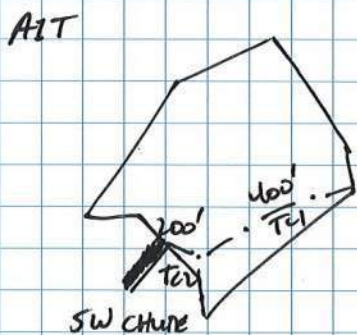
$$T_c = \frac{T_{c1}}{1.3 \text{ ft/sec}} + \frac{T_{c2}}{0.7 \text{ ft/sec}} = 961.54 \text{ sec}$$

$$461.54 \text{ sec} + 500 \text{ sec} \Rightarrow \frac{961.54 \text{ sec}}{60 \text{ sec/min}} \Rightarrow 16.02 \text{ min}$$

→ Overland Flow @ 4% Slope TO  
 DIVERSION BERM @ 1% Slope TO CHAURE

B1S USE CONSERVATIVE  
 VALUE OF T<sub>c</sub> = 10min

→ WATER BEING  
 DIVERTED TO  
 CHAURES BY  
 DIVERSION BERMS



$$T_c = \frac{400 \text{ ft}}{1.3 \text{ ft/sec}} + \frac{200 \text{ ft}}{0.7 \text{ ft/sec}} \Rightarrow 593 \text{ sec}$$

$$307.7 \text{ sec} + 285.7 \text{ sec} \Rightarrow \frac{593 \text{ sec}}{60 \text{ sec/min}} \Rightarrow 9.89 \text{ min}$$

USE 10min  
 → Overland Flow @ 4% Slope  
 TO DIVERSION BERM @ 1% Slope TO CHAURE

A1S USE CONSERVATIVE  
 VALUE OF T<sub>c</sub> = 10min

→ WATER BEING  
 DIVERTED  
 TO CHAURES  
 BY DIVERSION  
 BERMS.

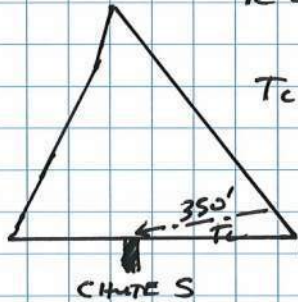
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JOB NO. 8514-03 City of Kingsville Landfill	SHEET NO. 2 of 2
DESCRIPTION Permit Amendment - Post Development - Top Drainage Areas / Slopes	DATE 8/26/18
HydroCAD - Tc (Time of Concentration) Input DATA	BY JLG

TOP

A2T



$$T_c = \frac{350 \text{ ft}}{0.7 \text{ ft/sec}} \Rightarrow 500 \text{ SEC}$$

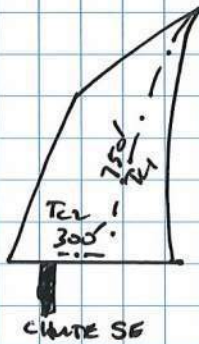
$$T_c = \frac{500 \text{ sec}}{60 \frac{\text{sec}}{\text{min}}} \Rightarrow 8.3 \text{ min}$$

USE 10 min  
 → FLOW @ 1% Slope TO CHUTE

SLOPES

A2S USE CONSERVATIVE VALUE OF  $T_c = 10 \text{ min}$ ,  
 → WATER BEING DIVERTED TO CHUTES BY DIVERSION BERMS.

A3T



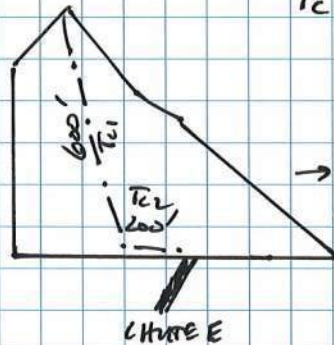
$$T_c = \frac{T_{c1}}{1.3 \text{ ft/sec}} + \frac{T_{c2}}{0.7 \text{ ft/sec}} \Rightarrow 1005.48 \text{ SEC}$$

$$T_c = 576.92 + 428.57 \Rightarrow 1005.49 \text{ SEC} \Rightarrow 16.76 \text{ min}$$

→ OVERLAND FLOW @ 4% Slope TO DIVERSION BERM @ 1% TO CHUTE

A3S USE CONSERVATIVE VALUE OF  $T_c = 10 \text{ min}$   
 → WATER BEING DIVERTED TO CHUTES BY DIVERSION BERMS

C1T



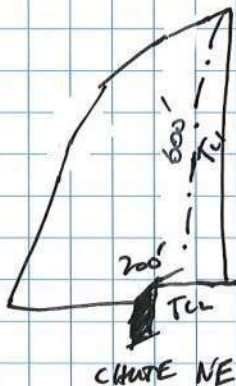
$$T_c = \frac{T_{c1}}{1.3 \text{ ft/sec}} + \frac{T_{c2}}{0.7 \text{ ft/sec}} \Rightarrow 747.25 \text{ SEC}$$

$$461.54 \text{ sec} + 285.71 \text{ sec} \Rightarrow 747.25 \text{ SEC} \Rightarrow 12.45 \text{ min}$$

→ OVERLAND FLOW @ 4% Slope TO DIVERSION BERM @ 1% TO CHUTE

C1S USE CONSERVATIVE VALUE OF  $T_c = 10 \text{ min}$   
 → WATER BEING DIVERTED TO CHUTES BY DIVERSION BERMS.

C2T



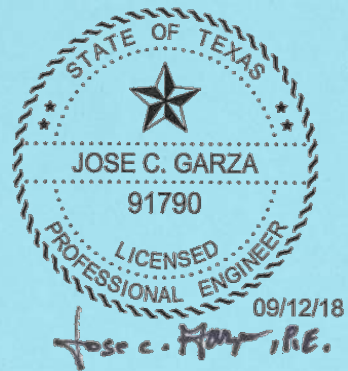
$$T_c = \frac{T_{c1}}{1.3 \text{ ft/sec}} + \frac{T_{c2}}{0.7 \text{ ft/sec}} \Rightarrow 747.25 \text{ SEC}$$

$$461.54 \text{ sec} + 285.71 \text{ sec} \Rightarrow 747.25 \text{ SEC} \Rightarrow 12.45 \text{ min}$$

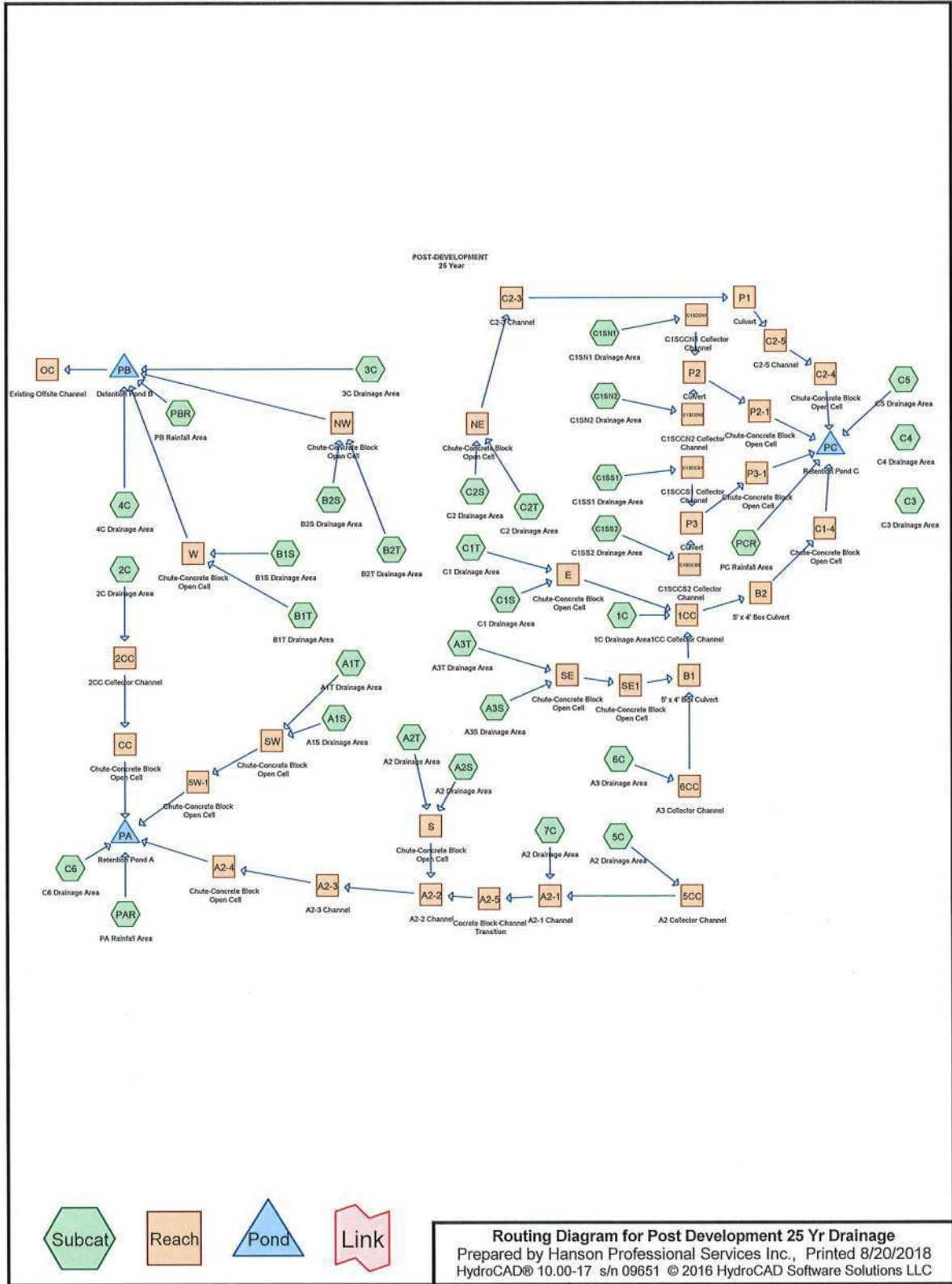
→ OVERLAND FLOW @ 4% Slope TO DIVERSION BERM @ 1% Slope TO CHUTE

C2S USE CONSERVATIVE VALUE OF  $T_c = 10 \text{ min}$   
 → WATER BEING DIVERTED TO CHUTES BY DIVERSION BERMS.

APPENDIX 6B.4  
HYDROCAD MODEL POST DEVELOPMENT-25 YEAR







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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
128.657	79	50-75% Grass cover, Fair, HSG C (1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T)
19.672	86	<50% Grass cover, Poor, HSG C (C3, C4, C5, C6)
16.270	98	Water Surface, 0% imp, HSG C (PAR, PBR, PCR)
<b>164.599</b>	<b>82</b>	<b>TOTAL AREA</b>

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
164.599	HSG C	1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T, C3, C4, C5, C6, PAR, PBR, PCR
0.000	HSG D	
0.000	Other	
<b>164.599</b>		<b>TOTAL AREA</b>

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	128.657	0.000	0.000	128.657	50-75% Grass cover, Fair	1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T
0.000	0.000	19.672	0.000	0.000	19.672	<50% Grass cover, Poor	C3, C4, C5, C6
0.000	0.000	16.270	0.000	0.000	16.270	Water Surface, 0% imp	PAR, PBR, PCR
<b>0.000</b>	<b>0.000</b>	<b>164.599</b>	<b>0.000</b>	<b>0.000</b>	<b>164.599</b>	<b>TOTAL AREA</b>	

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**Pipe Listing (all nodes)**

Line#	Node Number	In-invert (feet)	Out-invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	B1	56.54	53.89	464.0	0.0057	0.013	60.0	48.0	0.0
2	B2	53.45	49.80	200.0	0.0183	0.013	60.0	48.0	0.0
3	P1	51.75	51.11	64.0	0.0100	0.011	48.0	0.0	0.0
4	P2	54.39	53.31	72.0	0.0150	0.011	18.0	0.0	0.0
5	P3	55.41	54.33	72.0	0.0150	0.011	18.0	0.0	0.0
6	PB	47.00	46.75	128.0	0.0020	0.013	21.0	0.0	0.0
7	PB	47.00	46.75	128.0	0.0020	0.013	21.0	0.0	0.0

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*Type III 24-hr 25-Year Rainfall=8.70"*

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Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment 1C: 1C Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=6.22 cfs 0.514 af
<b>Subcatchment 2C: 2C Drainage Area</b>	Runoff Area=1.480 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=9.20 cfs 0.760 af
<b>Subcatchment 3C: 3C Drainage Area</b>	Runoff Area=1.640 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=10.20 cfs 0.842 af
<b>Subcatchment 4C: 4C Drainage Area</b>	Runoff Area=0.910 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=5.66 cfs 0.467 af
<b>Subcatchment 5C: A2 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=6.22 cfs 0.514 af
<b>Subcatchment 6C: A3 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=6.22 cfs 0.514 af
<b>Subcatchment 7C: A2 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=6.22 cfs 0.514 af
<b>Subcatchment A1S: A1S Drainage Area</b>	Runoff Area=8.009 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=49.80 cfs 4.113 af
<b>Subcatchment A1T: A1T Drainage Area</b>	Runoff Area=7.425 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=46.16 cfs 3.813 af
<b>Subcatchment A2S: A2 Drainage Area</b>	Runoff Area=12.241 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=76.11 cfs 6.287 af
<b>Subcatchment A2T: A2 Drainage Area</b>	Runoff Area=5.120 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=31.83 cfs 2.629 af
<b>Subcatchment A3S: A3S Drainage Area</b>	Runoff Area=10.760 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=66.90 cfs 5.526 af
<b>Subcatchment A3T: A3T Drainage Area</b>	Runoff Area=7.489 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=1,050' Tc=16.7 min CN=79 Runoff=38.81 cfs 3.846 af
<b>Subcatchment B1S: B1S Drainage Area</b>	Runoff Area=14.884 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=92.54 cfs 7.644 af
<b>Subcatchment B1T: B1T Drainage Area</b>	Runoff Area=7.499 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=950' Tc=16.0 min CN=79 Runoff=39.52 cfs 3.851 af
<b>Subcatchment B2S: B2S Drainage Area</b>	Runoff Area=8.806 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=54.75 cfs 4.522 af

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<b>Subcatchment B2T: B2T Drainage Area</b>	Runoff Area=4.309 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=850' Tc=13.7 min CN=79 Runoff=24.07 cfs 2.213 af
<b>Subcatchment C1S: C1 Drainage Area</b>	Runoff Area=11.506 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=71.54 cfs 5.909 af
<b>Subcatchment C1SN1: C1SN1 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=1.55 cfs 0.128 af
<b>Subcatchment C1SN2: C1SN2 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=1.55 cfs 0.128 af
<b>Subcatchment C1SS1: C1SS1 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=1.55 cfs 0.128 af
<b>Subcatchment C1SS2: C1SS2 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=1.55 cfs 0.128 af
<b>Subcatchment C1T: C1 Drainage Area</b>	Runoff Area=6.292 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=800' Tc=12.5 min CN=79 Runoff=36.29 cfs 3.231 af
<b>Subcatchment C2S: C2 Drainage Area</b>	Runoff Area=10.038 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=62.41 cfs 5.155 af
<b>Subcatchment C2T: C2 Drainage Area</b>	Runoff Area=5.249 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=800' Tc=12.5 min CN=79 Runoff=30.27 cfs 2.696 af
<b>Subcatchment C3: C3 Drainage Area</b>	Runoff Area=3.500 ac 0.00% Impervious Runoff Depth=7.01" Tc=10.0 min CN=86 Runoff=24.05 cfs 2.045 af
<b>Subcatchment C4: C4 Drainage Area</b>	Runoff Area=9.500 ac 0.00% Impervious Runoff Depth=7.01" Tc=10.0 min CN=86 Runoff=65.28 cfs 5.551 af
<b>Subcatchment C5: C5 Drainage Area</b>	Runoff Area=2.690 ac 0.00% Impervious Runoff Depth=7.01" Tc=10.0 min CN=86 Runoff=18.49 cfs 1.572 af
<b>Subcatchment C6: C6 Drainage Area</b>	Runoff Area=3.982 ac 0.00% Impervious Runoff Depth=7.01" Tc=10.0 min CN=86 Runoff=27.36 cfs 2.327 af
<b>Subcatchment PAR: PA Rainfall Area</b>	Runoff Area=7.440 ac 0.00% Impervious Runoff Depth=8.46" Tc=0.0 min CN=98 Runoff=77.55 cfs 5.245 af
<b>Subcatchment PBR: PB Rainfall Area</b>	Runoff Area=4.290 ac 0.00% Impervious Runoff Depth=8.46" Tc=0.0 min CN=98 Runoff=44.71 cfs 3.024 af
<b>Subcatchment PCR: PC Rainfall Area</b>	Runoff Area=4.540 ac 0.00% Impervious Runoff Depth=8.46" Tc=0.0 min CN=98 Runoff=47.32 cfs 3.201 af
<b>Reach 1CC: 1CC Collector Channel</b>	Avg. Flow Depth=4.52' Max Vel=3.89 fps Inflow=213.11 cfs 19.540 af n=0.030 L=222.0' S=0.0020 1' Capacity=2,157.50 cfs Outflow=211.91 cfs 19.540 af

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<b>Reach 2CC: 2CC Collector Channel</b>	Avg. Flow Depth=1.28' Max Vel=1.58 fps Inflow=9.20 cfs 0.760 af n=0.030 L=650.0' S=0.0020 '/ Capacity=46.53 cfs Outflow=7.72 cfs 0.760 af
<b>Reach 5CC: A2 Collector Channel</b>	Avg. Flow Depth=0.97' Max Vel=1.36 fps Inflow=6.22 cfs 0.514 af n=0.030 L=595.0' S=0.0015 '/ Capacity=68.72 cfs Outflow=5.17 cfs 0.514 af
<b>Reach 6CC: A3 Collector Channel</b>	Avg. Flow Depth=0.77' Max Vel=1.97 fps Inflow=6.22 cfs 0.514 af n=0.030 L=740.0' S=0.0040 '/ Capacity=50.02 cfs Outflow=5.34 cfs 0.514 af
<b>Reach A2-1: A2-1 Channel</b>	Avg. Flow Depth=1.24' Max Vel=1.57 fps Inflow=8.74 cfs 1.027 af n=0.030 L=250.5' S=0.0015 '/ Capacity=83.47 cfs Outflow=8.70 cfs 1.027 af
<b>Reach A2-2: A2-2 Channel</b>	Avg. Flow Depth=2.53' Max Vel=3.72 fps Inflow=114.51 cfs 9.943 af n=0.025 L=257.0' S=0.0020 '/ Capacity=338.68 cfs Outflow=113.50 cfs 9.943 af
<b>Reach A2-3: A2-3 Channel</b>	Avg. Flow Depth=2.57' Max Vel=3.19 fps Inflow=113.50 cfs 9.943 af n=0.030 L=582.0' S=0.0020 '/ Capacity=532.10 cfs Outflow=108.05 cfs 9.943 af
<b>Reach A2-4: Chute-Concrete Block</b>	Avg. Flow Depth=0.75' Max Vel=11.15 fps Inflow=108.05 cfs 9.943 af n=0.025 L=250.0' S=0.0697 '/ Capacity=692.98 cfs Outflow=107.90 cfs 9.943 af
<b>Reach A2-5: Concrete Block-Channel</b>	Avg. Flow Depth=0.30' Max Vel=11.21 fps Inflow=8.70 cfs 1.027 af n=0.025 L=5.6' S=0.2482 '/ Capacity=903.50 cfs Outflow=8.70 cfs 1.027 af
<b>Reach B1: 5' x 4' Box Culvert</b>	Avg. Flow Depth=2.17' Max Vel=9.54 fps Inflow=103.76 cfs 9.886 af 60.0" x 48.0" Box Pipe n=0.013 L=464.0' S=0.0057 '/ Capacity=185.34 cfs Outflow=103.38 cfs 9.886 af
<b>Reach B2: 5' x 4' Box Culvert</b>	Avg. Flow Depth=2.40' Max Vel=17.67 fps Inflow=211.91 cfs 19.540 af 60.0" x 48.0" Box Pipe n=0.013 L=200.0' S=0.0183 '/ Capacity=331.32 cfs Outflow=211.71 cfs 19.540 af
<b>Reach C1-4: Chute-Concrete Block</b>	Avg. Flow Depth=1.01' Max Vel=23.03 fps Inflow=211.71 cfs 19.540 af n=0.025 L=76.0' S=0.2474 '/ Capacity=672.67 cfs Outflow=211.66 cfs 19.540 af
<b>Reach C1SCCN1: C1SCCN1 Collector</b>	Avg. Flow Depth=0.33' Max Vel=1.19 fps Inflow=1.55 cfs 0.128 af n=0.030 L=285.0' S=0.0033 '/ Capacity=24.47 cfs Outflow=1.44 cfs 0.128 af
<b>Reach C1SCCN2: C1SCCN2 Collector</b>	Avg. Flow Depth=0.33' Max Vel=1.19 fps Inflow=1.55 cfs 0.128 af n=0.030 L=287.5' S=0.0033 '/ Capacity=24.36 cfs Outflow=1.44 cfs 0.128 af
<b>Reach C1SCCS1: C1SCCS1 Collector</b>	Avg. Flow Depth=0.33' Max Vel=1.19 fps Inflow=1.55 cfs 0.128 af n=0.030 L=280.0' S=0.0033 '/ Capacity=24.30 cfs Outflow=1.44 cfs 0.128 af
<b>Reach C1SCCS2: C1SCCS2 Collector</b>	Avg. Flow Depth=0.33' Max Vel=1.19 fps Inflow=1.55 cfs 0.128 af n=0.030 L=280.0' S=0.0033 '/ Capacity=24.30 cfs Outflow=1.44 cfs 0.128 af
<b>Reach C2-3: C2-3 Channel</b>	Avg. Flow Depth=2.82' Max Vel=3.06 fps Inflow=91.74 cfs 7.851 af n=0.030 L=882.0' S=0.0020 '/ Capacity=178.76 cfs Outflow=82.99 cfs 7.851 af
<b>Reach C2-4: Chute-Concrete Block</b>	Avg. Flow Depth=0.58' Max Vel=19.49 fps Inflow=82.89 cfs 7.851 af n=0.025 L=52.0' S=0.3269 '/ Capacity=1,003.23 cfs Outflow=82.88 cfs 7.851 af



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<b>Reach C2-5: C2-5 Channel</b>	Avg. Flow Depth=1.08'	Max Vel=8.22 fps	Inflow=82.96 cfs	7.851 af
	n=0.025 L=106.0'	S=0.0293 '/'	Capacity=492.25 cfs	Outflow=82.89 cfs 7.851 af
<b>Reach CC: Chute-Concrete Block Open</b>	Avg. Flow Depth=0.21'	Max Vel=6.18 fps	Inflow=7.72 cfs	0.760 af
	n=0.025 L=160.0'	S=0.1028 '/'	Capacity=562.60 cfs	Outflow=7.71 cfs 0.760 af
<b>Reach E: Chute-Concrete Block</b>	Avg. Flow Depth=0.71'	Max Vel=19.11 fps	Inflow=106.93 cfs	9.140 af
	n=0.025 L=462.0'	S=0.2511 '/'	Capacity=879.20 cfs	Outflow=106.72 cfs 9.140 af
<b>Reach NE: Chute-Concrete Block</b>	Avg. Flow Depth=0.66'	Max Vel=18.27 fps	Inflow=91.93 cfs	7.851 af
	n=0.025 L=464.0'	S=0.2500 '/'	Capacity=877.30 cfs	Outflow=91.74 cfs 7.851 af
<b>Reach NW: Chute-Concrete Block</b>	Avg. Flow Depth=0.60'	Max Vel=17.38 fps	Inflow=77.52 cfs	6.735 af
	n=0.025 L=464.0'	S=0.2500 '/'	Capacity=877.30 cfs	Outflow=77.39 cfs 6.735 af
<b>Reach OC: Existing Offsite Channel</b>	Avg. Flow Depth=1.82'	Max Vel=1.72 fps	Inflow=33.70 cfs	21.821 af
	n=0.030 L=2,800.0'	S=0.0010 '/'	Capacity=44.23 cfs	Outflow=32.78 cfs 21.722 af
<b>Reach P1: Culvert</b>	Avg. Flow Depth=1.97'	Max Vel=13.43 fps	Inflow=82.99 cfs	7.851 af
48.0" Round Pipe	n=0.011 L=64.0'	S=0.0100 '/'	Capacity=169.76 cfs	Outflow=82.96 cfs 7.851 af
<b>Reach P2: Culvert</b>	Avg. Flow Depth=0.44'	Max Vel=6.62 fps	Inflow=2.88 cfs	0.257 af
18.0" Round Pipe	n=0.011 L=72.0'	S=0.0150 '/'	Capacity=15.20 cfs	Outflow=2.88 cfs 0.257 af
<b>Reach P2-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.14'	Max Vel=8.63 fps	Inflow=2.88 cfs	0.257 af
	n=0.025 L=60.0'	S=0.3718 '/'	Capacity=316.81 cfs	Outflow=2.88 cfs 0.257 af
<b>Reach P3: Culvert</b>	Avg. Flow Depth=0.44'	Max Vel=6.62 fps	Inflow=2.89 cfs	0.257 af
18.0" Round Pipe	n=0.011 L=72.0'	S=0.0150 '/'	Capacity=15.20 cfs	Outflow=2.89 cfs 0.257 af
<b>Reach P3-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.14'	Max Vel=8.81 fps	Inflow=2.89 cfs	0.257 af
	n=0.025 L=60.0'	S=0.3942 '/'	Capacity=326.18 cfs	Outflow=2.89 cfs 0.257 af
<b>Reach S: Chute-Concrete Block</b>	Avg. Flow Depth=0.72'	Max Vel=19.13 fps	Inflow=107.94 cfs	8.916 af
	n=0.025 L=459.0'	S=0.2500 '/'	Capacity=877.30 cfs	Outflow=107.70 cfs 8.916 af
<b>Reach SE: Chute-Concrete Block</b>	Avg. Flow Depth=0.69'	Max Vel=18.76 fps	Inflow=100.71 cfs	9.372 af
	n=0.025 L=450.0'	S=0.2499 '/'	Capacity=877.14 cfs	Outflow=100.58 cfs 9.372 af
<b>Reach SE1: Chute-Concrete Block</b>	Avg. Flow Depth=0.92'	Max Vel=12.50 fps	Inflow=100.58 cfs	9.372 af
	n=0.025 L=62.0'	S=0.0806 '/'	Capacity=498.27 cfs	Outflow=100.54 cfs 9.372 af
<b>Reach SW: Chute-Concrete Block</b>	Avg. Flow Depth=0.67'	Max Vel=18.50 fps	Inflow=95.96 cfs	7.926 af
	n=0.025 L=404.0'	S=0.2500 '/'	Capacity=877.30 cfs	Outflow=95.76 cfs 7.926 af
<b>Reach SW-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.80'	Max Vel=14.51 fps	Inflow=95.76 cfs	7.926 af
	n=0.025 L=266.0'	S=0.1269 '/'	Capacity=624.99 cfs	Outflow=95.59 cfs 7.926 af
<b>Reach W: Chute-Concrete Block</b>	Avg. Flow Depth=0.76'	Max Vel=20.06 fps	Inflow=127.46 cfs	11.495 af
	n=0.025 L=464.0'	S=0.2500 '/'	Capacity=877.30 cfs	Outflow=127.27 cfs 11.495 af

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<b>Pond PA: Retention Pond A</b>	Peak Elev=47.33'	Storage=26.200 af	Inflow=225.75 cfs	26.201 af	Outflow=0.00 cfs	0.000 af
<b>Pond PB: Detention Pond B</b>	Peak Elev=50.87'	Storage=11.562 af	Inflow=235.89 cfs	22.565 af	Outflow=33.70 cfs	21.821 af
<b>Pond PC: Retention Pond C</b>	Peak Elev=42.36'	Storage=32.676 af	Inflow=313.19 cfs	32.676 af	Outflow=0.00 cfs	0.000 af

**Total Runoff Area = 164.599 ac Runoff Volume = 89.038 af Average Runoff Depth = 6.49"**  
**100.00% Pervious = 164.599 ac 0.00% Impervious = 0.000 ac**

**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 1C: 1C Drainage Area**

Use Conservative Value of Tc=10 min

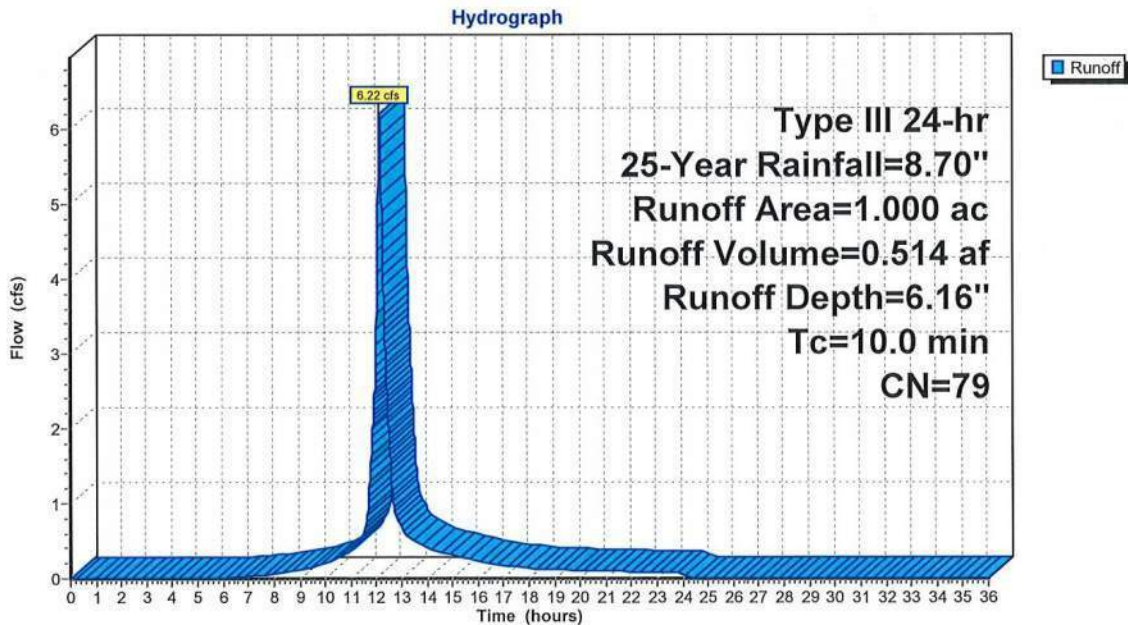
Runoff = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 1C: 1C Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 2C: 2C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 9.20 cfs @ 12.14 hrs, Volume= 0.760 af, Depth= 6.16"

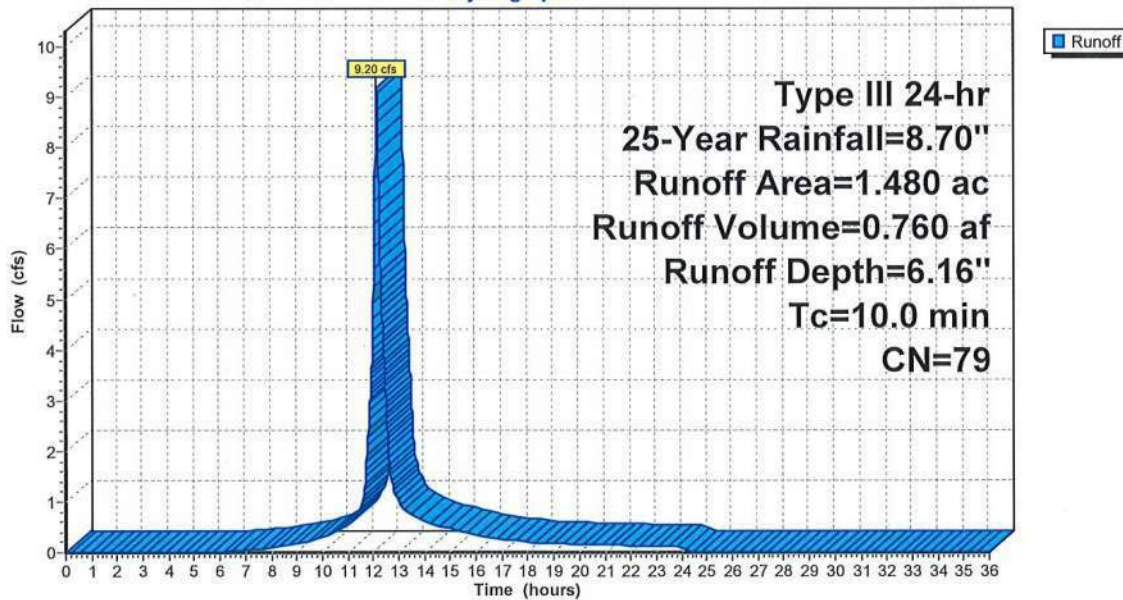
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.480	79	50-75% Grass cover, Fair, HSG C
1.480		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 2C: 2C Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 3C: 3C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 10.20 cfs @ 12.14 hrs, Volume= 0.842 af, Depth= 6.16"

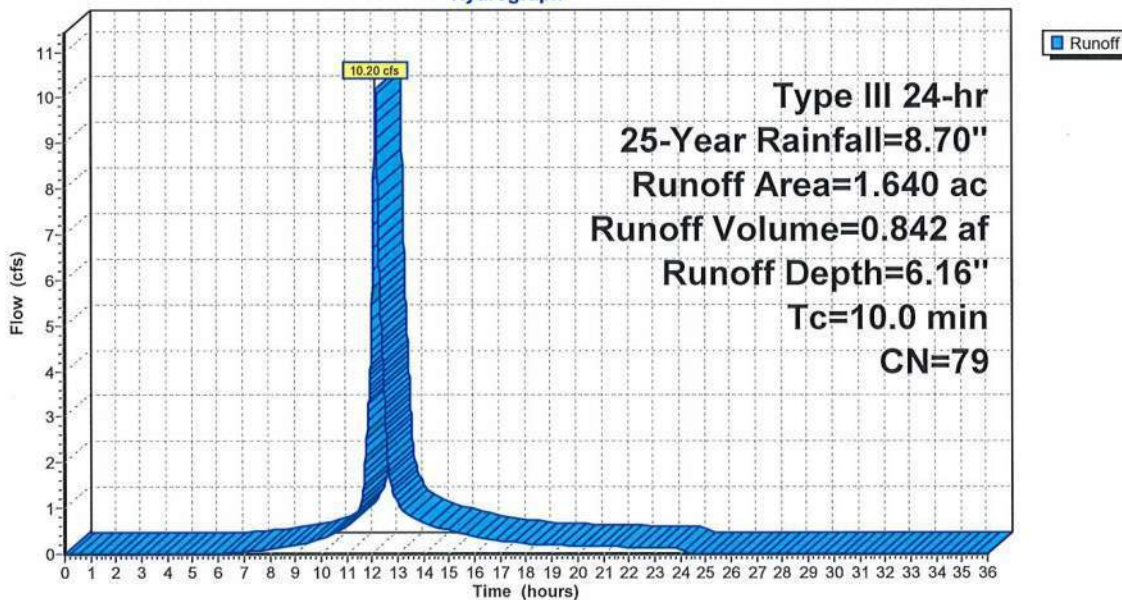
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.640	79	50-75% Grass cover, Fair, HSG C
1.640		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Surface Drainage to Pond B

**Subcatchment 3C: 3C Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 4C: 4C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 5.66 cfs @ 12.14 hrs, Volume= 0.467 af, Depth= 6.16"

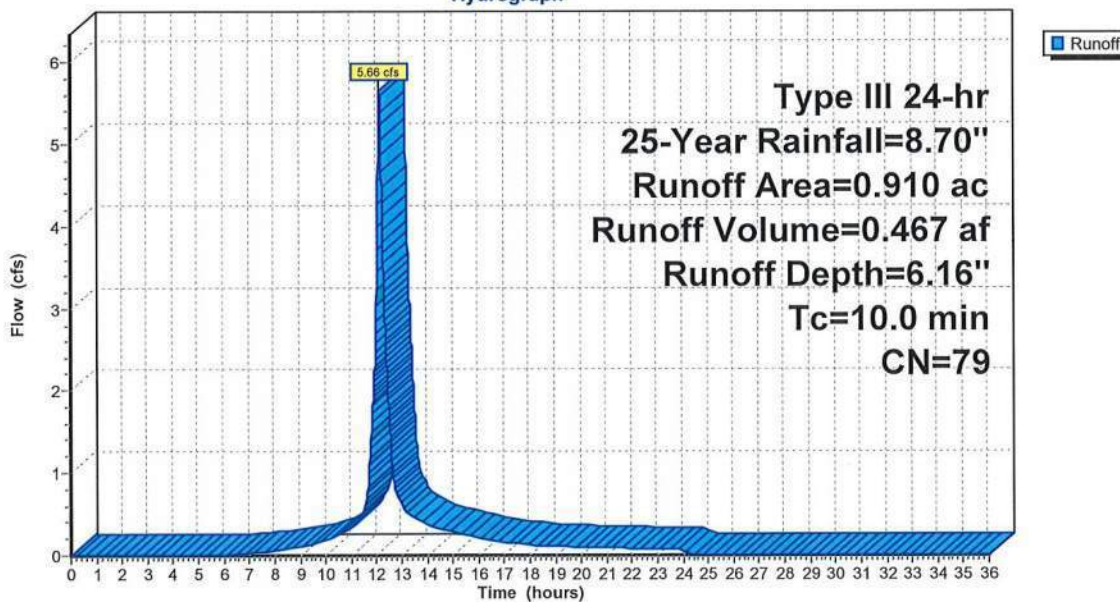
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
0.910	79	50-75% Grass cover, Fair, HSG C
0.910		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Surface Drainage to Pond B

**Subcatchment 4C: 4C Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 5C: A2 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af, Depth= 6.16"

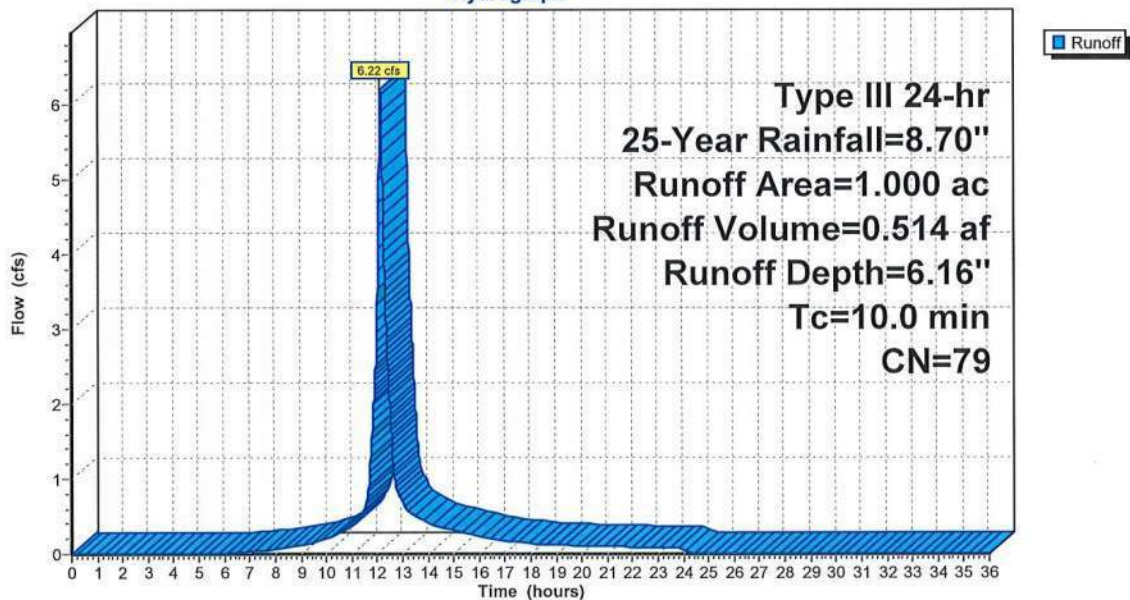
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 5C: A2 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 6C: A3 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af, Depth= 6.16"

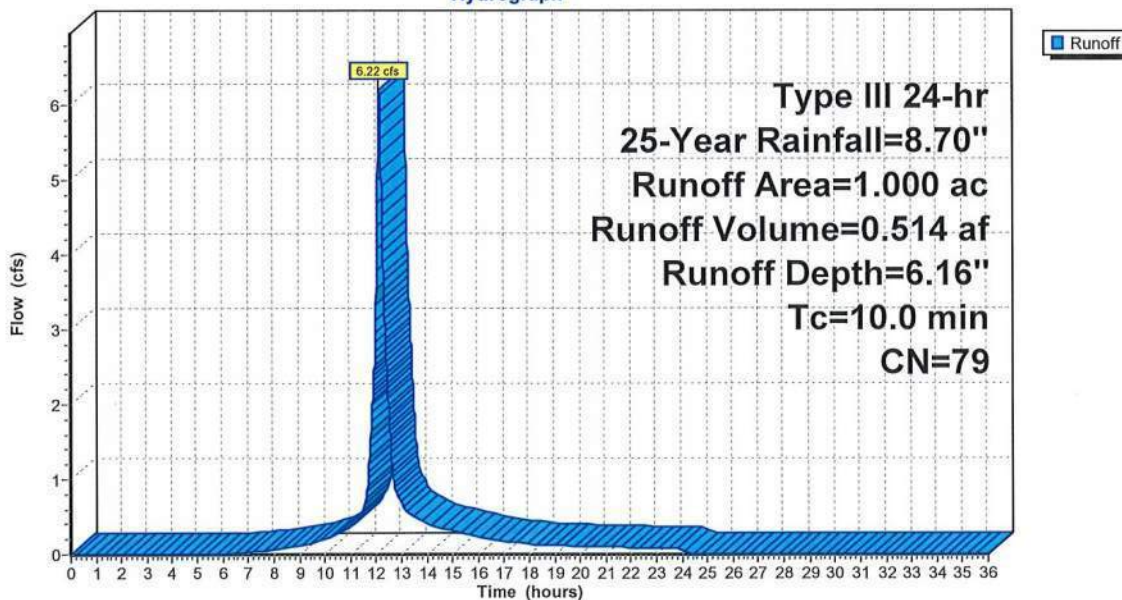
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 6C: A3 Drainage Area**

Hydrograph





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment 7C: A2 Drainage Area**

Use Conservative Value of Tc=10 min

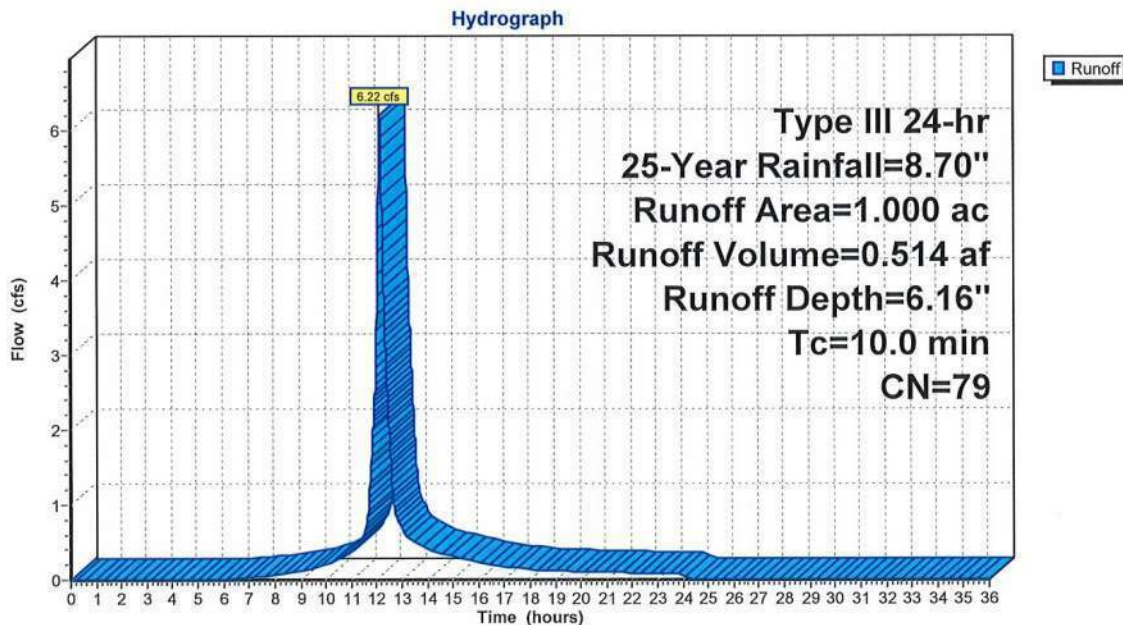
Runoff = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 7C: A2 Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A1S: A1S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 49.80 cfs @ 12.14 hrs, Volume= 4.113 af, Depth= 6.16"

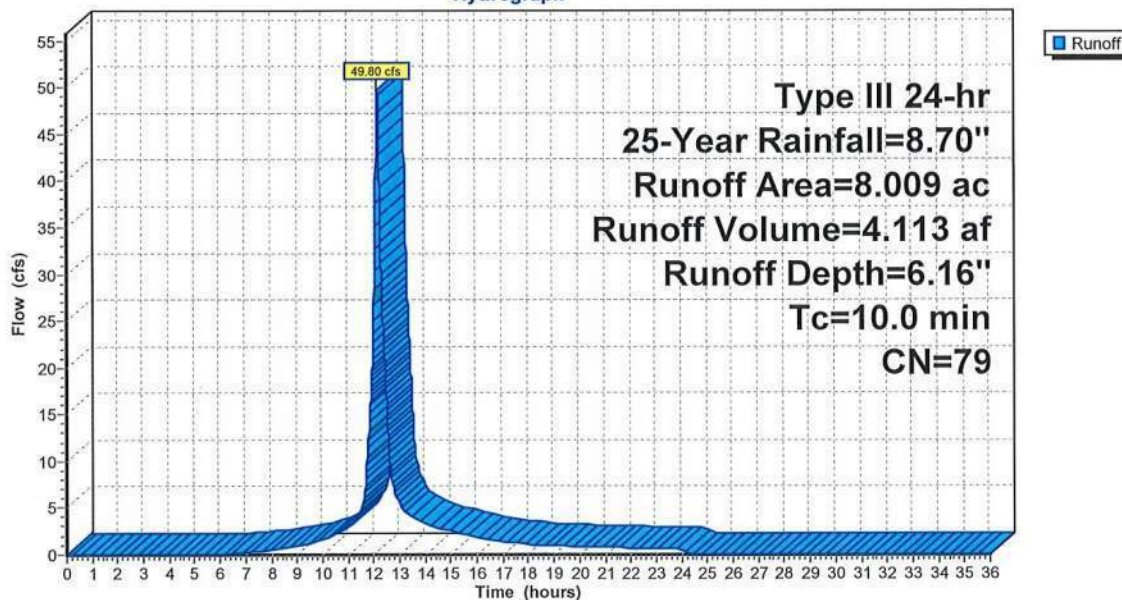
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
8.009	79	50-75% Grass cover, Fair, HSG C
8.009		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1S-Chute Flow Evaluation

**Subcatchment A1S: A1S Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A1T: A1T Drainage Area**

Runoff = 46.16 cfs @ 12.14 hrs, Volume= 3.813 af, Depth= 6.16"

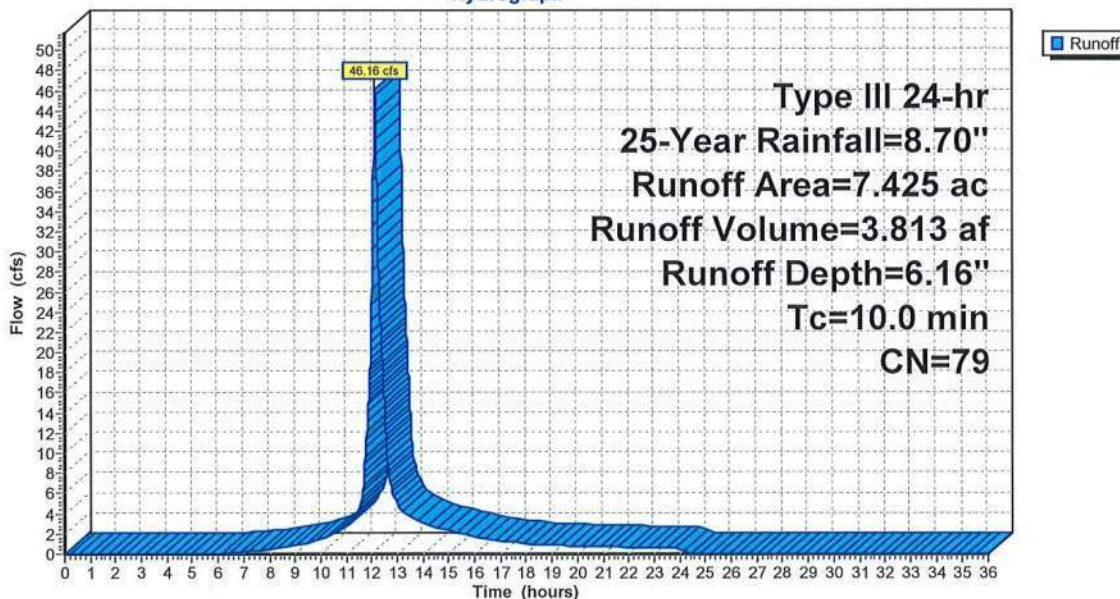
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
7.425	79	50-75% Grass cover, Fair, HSG C
7.425		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1T-Chute Flow Evaluation

**Subcatchment A1T: A1T Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A2S: A2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 76.11 cfs @ 12.14 hrs, Volume= 6.287 af, Depth= 6.16"

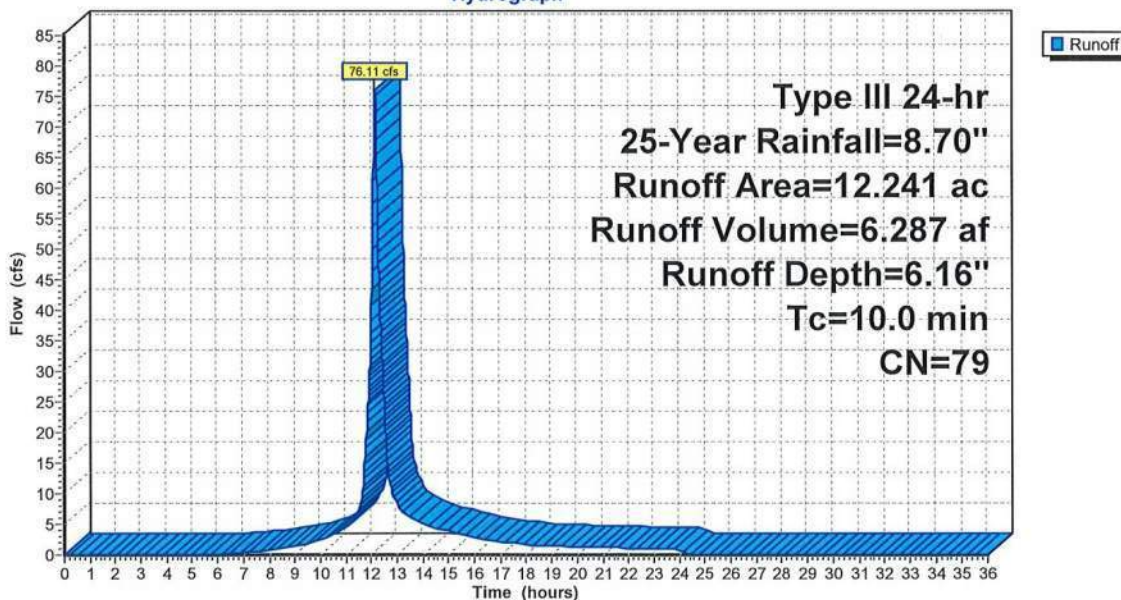
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
12.241	79	50-75% Grass cover, Fair, HSG C
12.241		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2S: A2 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A2T: A2 Drainage Area**

Runoff = 31.83 cfs @ 12.14 hrs, Volume= 2.629 af, Depth= 6.16"

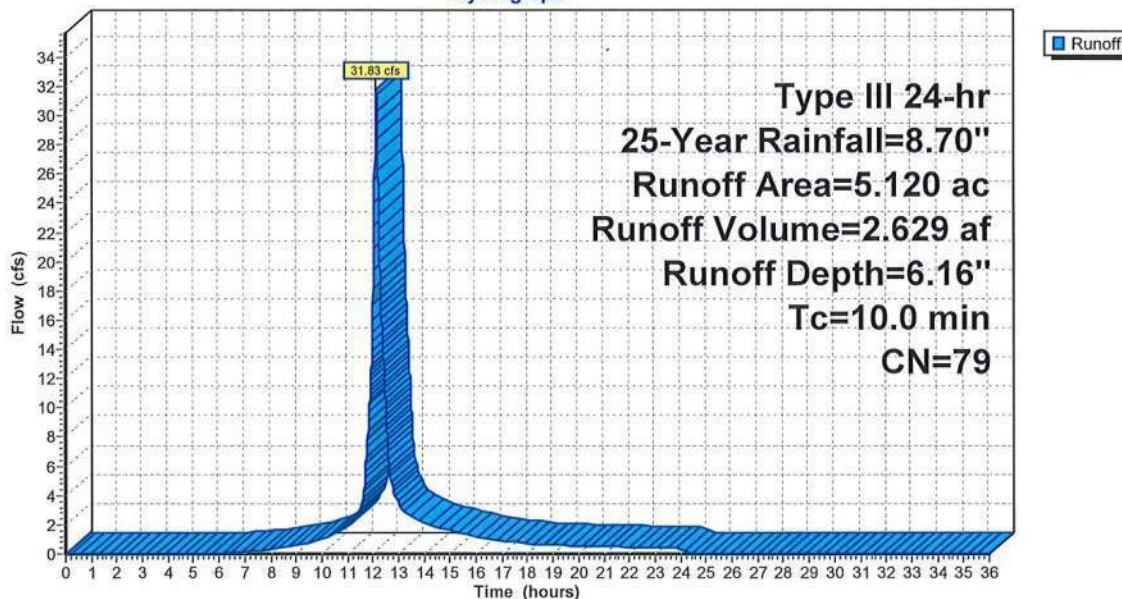
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
5.120	79	50-75% Grass cover, Fair, HSG C
5.120		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2T: A2 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A3S: A3S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 66.90 cfs @ 12.14 hrs, Volume= 5.526 af, Depth= 6.16"

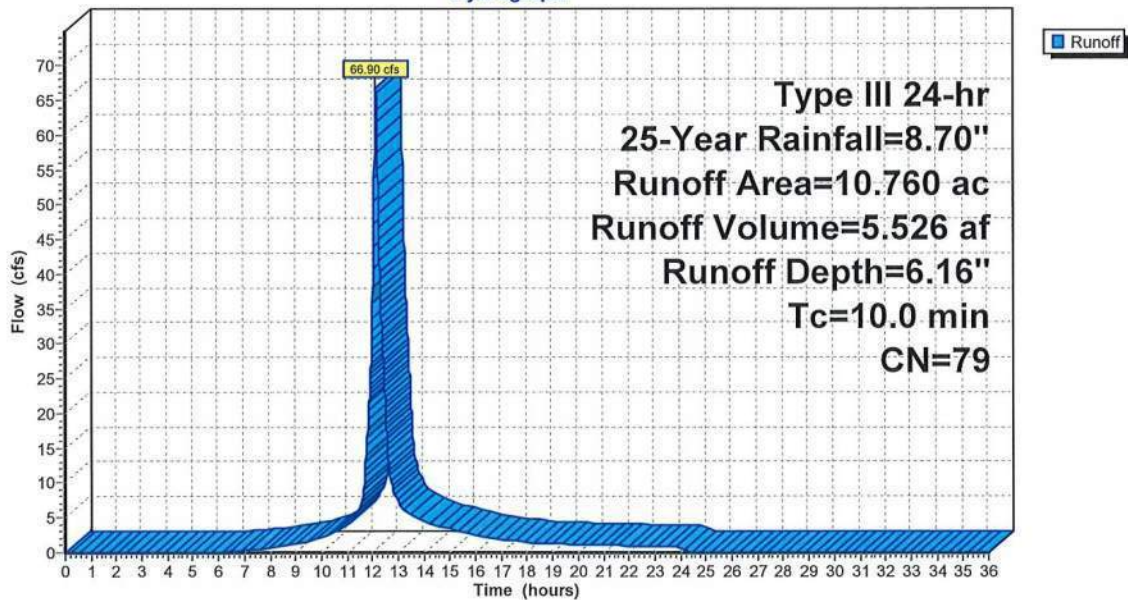
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
10.760	79	50-75% Grass cover, Fair, HSG C
10.760		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A3S-Chute Flow Evaluation

**Subcatchment A3S: A3S Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A3T: A3T Drainage Area**

Runoff = 38.81 cfs @ 12.23 hrs, Volume= 3.846 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

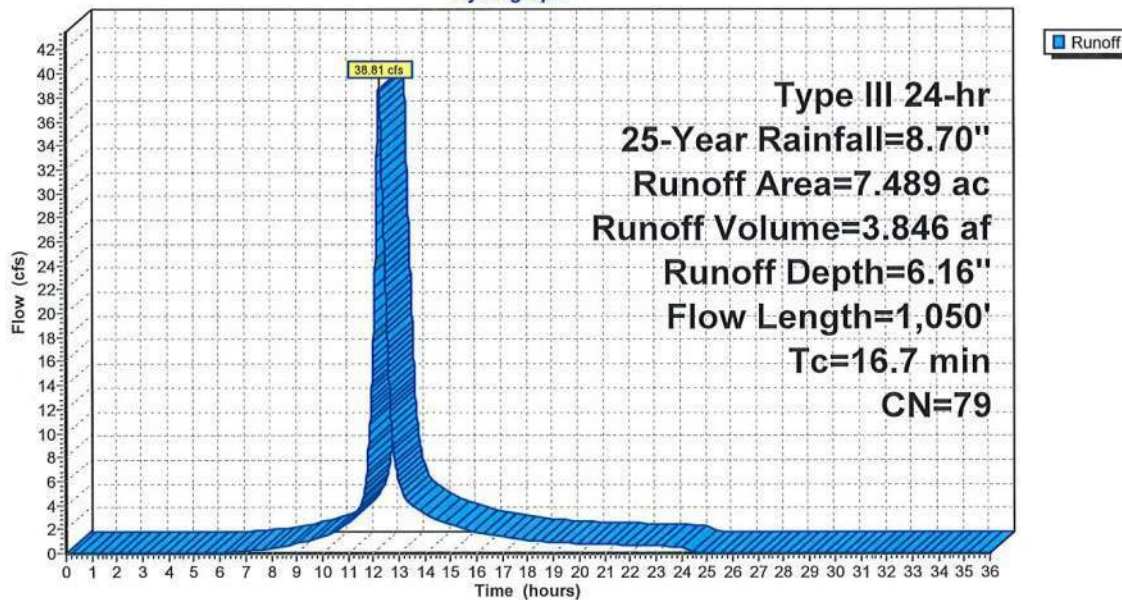
Area (ac)	CN	Description
7.489	79	50-75% Grass cover, Fair, HSG C
7.489		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.6	750		1.30		Direct Entry, A3T-Chute Flow Evaluation
7.1	300		0.70		Direct Entry,
16.7	1,050	Total			

**Subcatchment A3T: A3T Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B1S: B1S Drainage Area**

Use Conservative Value of Tc= 10 min.

Runoff = 92.54 cfs @ 12.14 hrs, Volume= 7.644 af, Depth= 6.16"

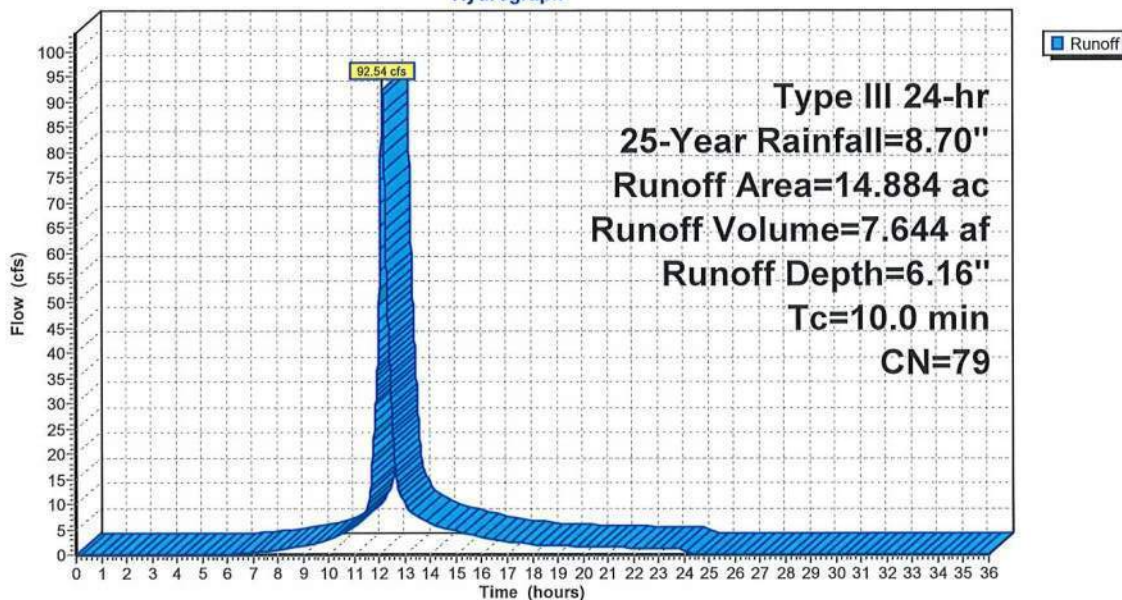
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
14.884	79	50-75% Grass cover, Fair, HSG C
14.884		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B1S-Chute Flow Evaluation

**Subcatchment B1S: B1S Drainage Area**

Hydrograph





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B1T: B1T Drainage Area**

Runoff = 39.52 cfs @ 12.21 hrs, Volume= 3.851 af, Depth= 6.16"

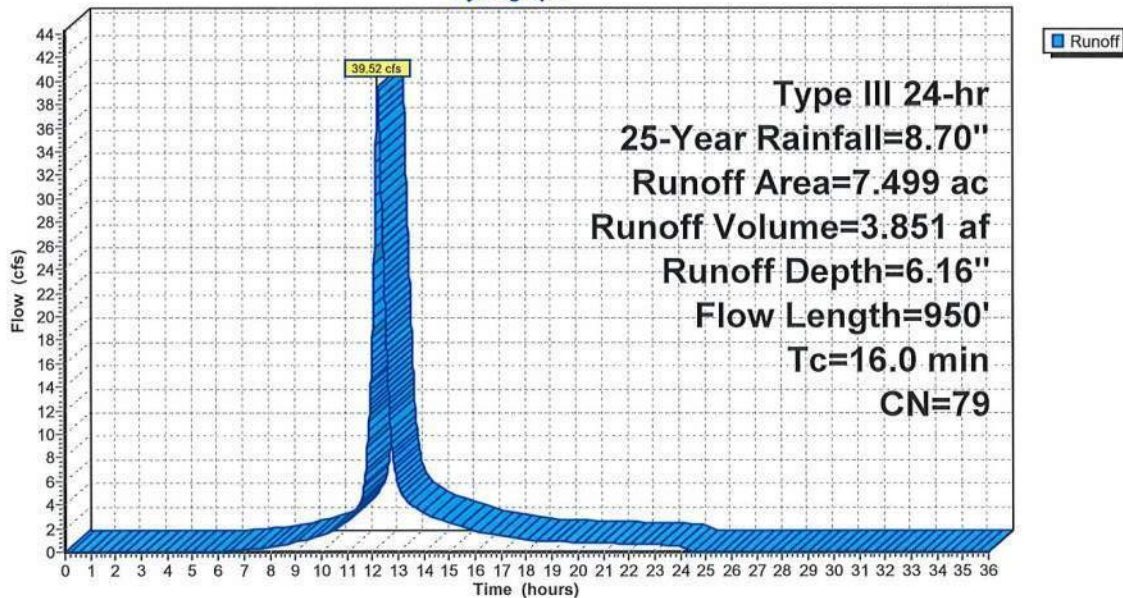
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
7.499	79	50-75% Grass cover, Fair, HSG C
7.499		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B1T-Chute Flow Evaluation
8.3	350		0.70		Direct Entry,
16.0	950	Total			

**Subcatchment B1T: B1T Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B2S: B2S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 54.75 cfs @ 12.14 hrs, Volume= 4.522 af, Depth= 6.16"

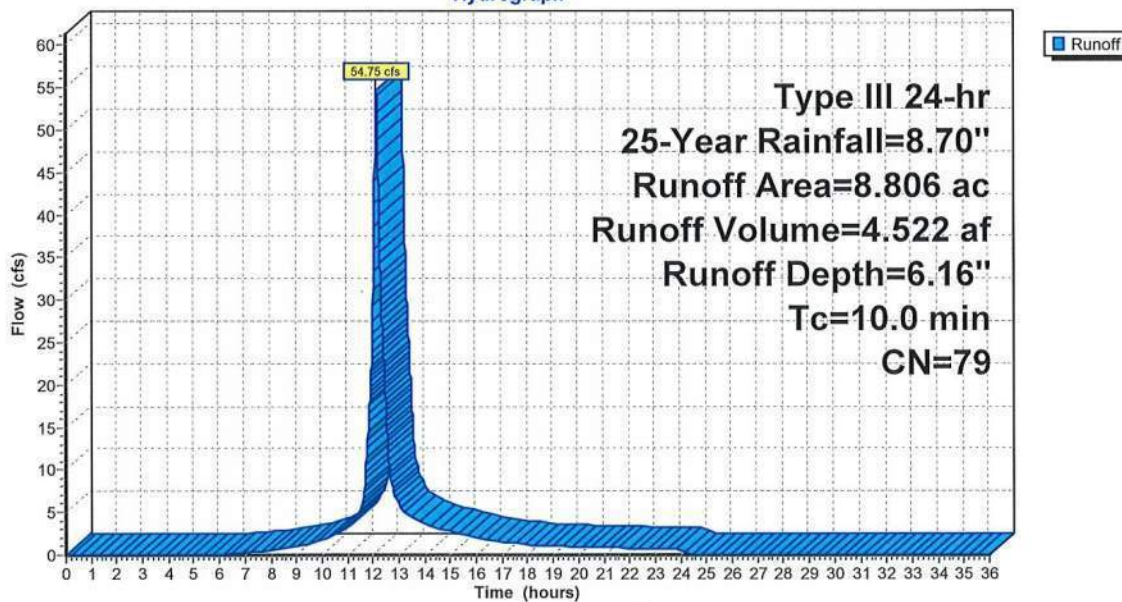
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
8.806	79	50-75% Grass cover, Fair, HSG C
8.806		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B2S-Chute Flow Evaluation

**Subcatchment B2S: B2S Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B2T: B2T Drainage Area**

Runoff = 24.07 cfs @ 12.19 hrs, Volume= 2.213 af, Depth= 6.16"

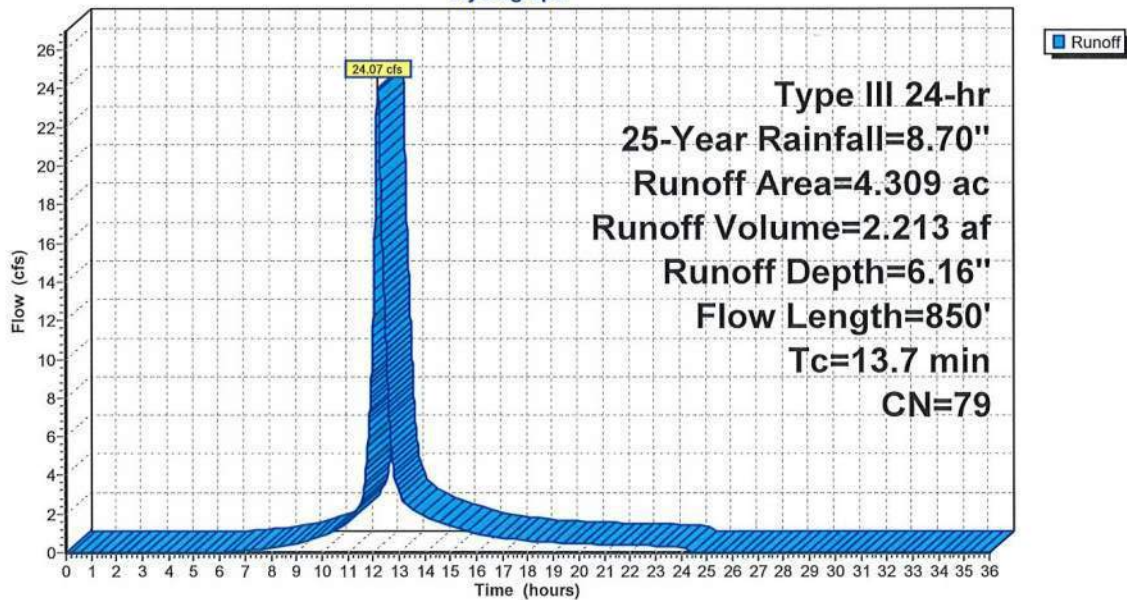
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
4.309	79	50-75% Grass cover, Fair, HSG C
4.309		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B2T-Chute Flow Evaluation
6.0	250		0.70		Direct Entry,
13.7	850	Total			

**Subcatchment B2T: B2T Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1S: C1 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 71.54 cfs @ 12.14 hrs, Volume= 5.909 af, Depth= 6.16"

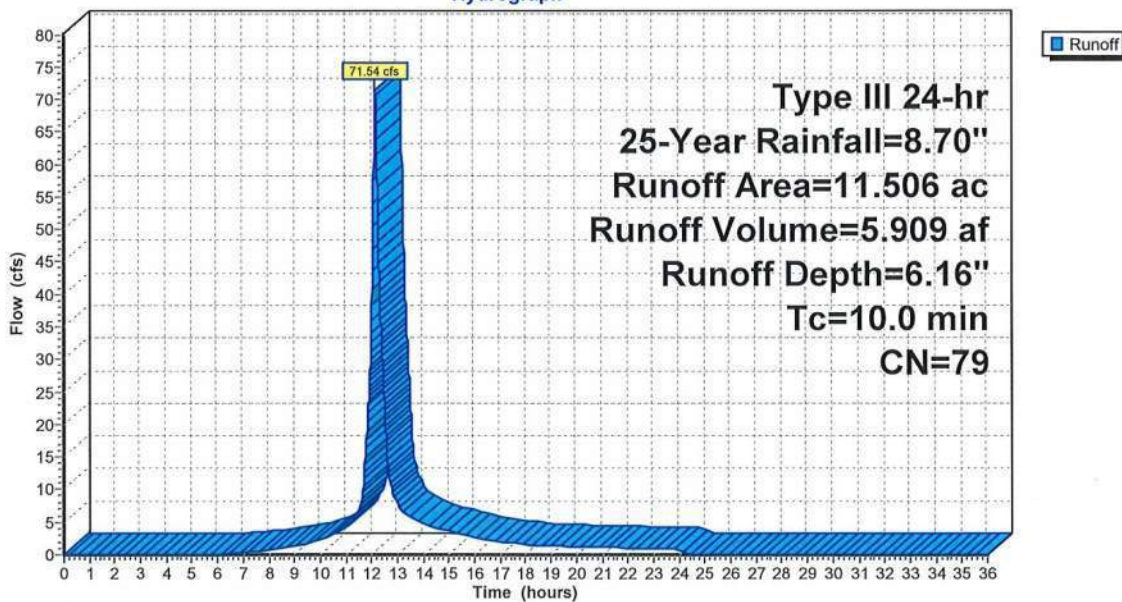
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
11.506	79	50-75% Grass cover, Fair, HSG C
11.506		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C1 Drainage Area

**Subcatchment C1S: C1 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1SN1: C1SN1 Drainage Area**

Use Conservative Value of Tc=10 min

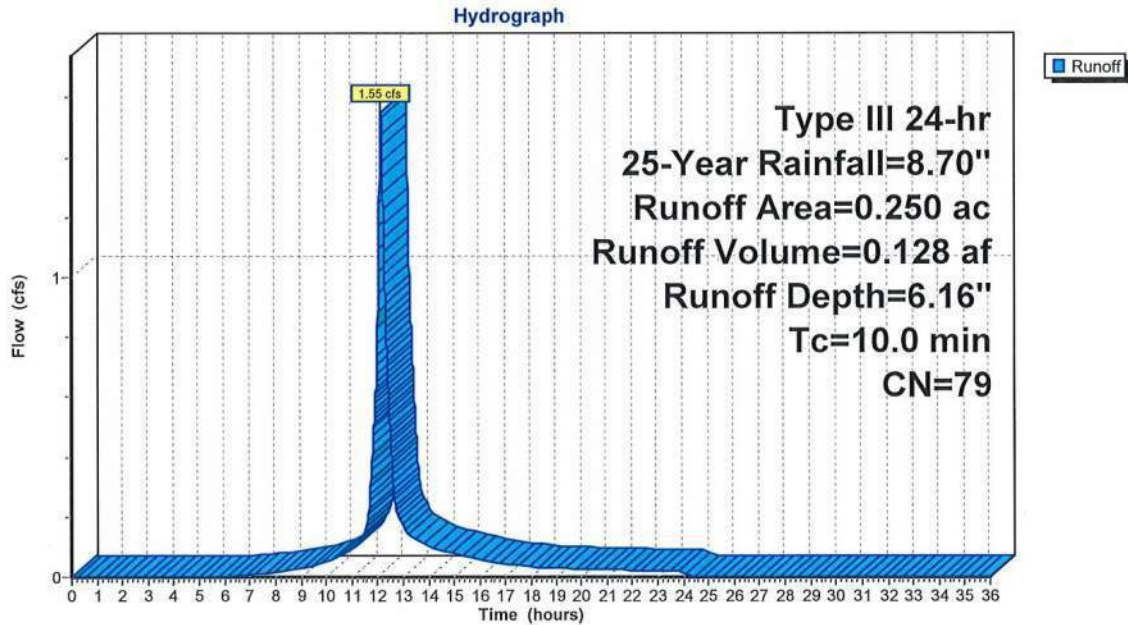
Runoff = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SN1: C1SN1 Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1SN2: C1SN2 Drainage Area**

Use Conservative Value of Tc=10 min

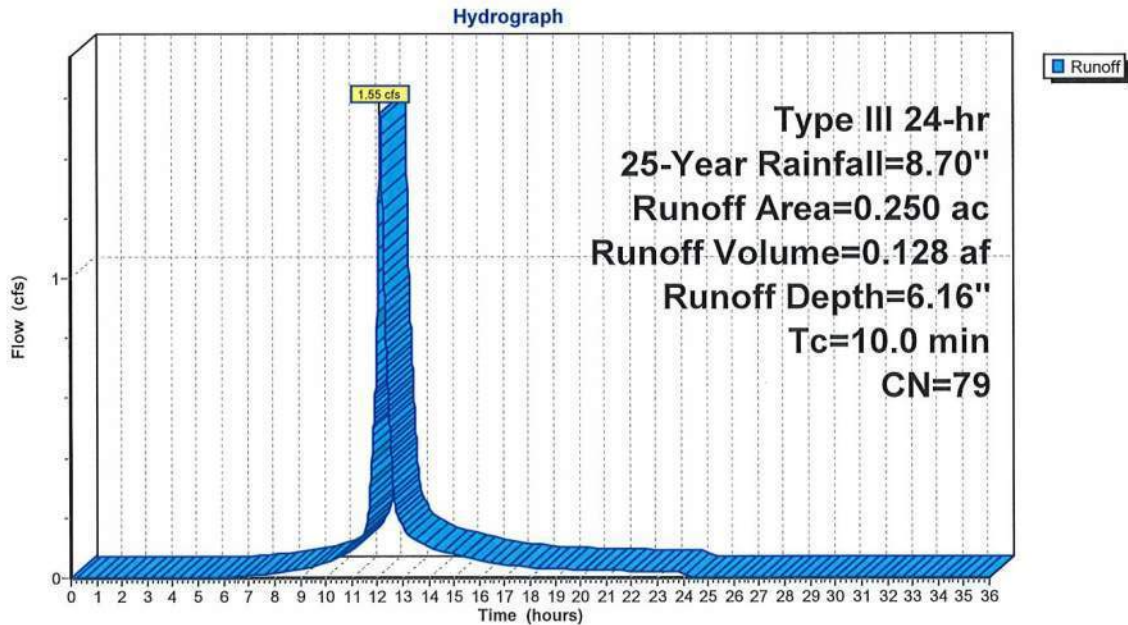
Runoff = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SN2: C1SN2 Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1SS1: C1SS1 Drainage Area**

Use Conservative Value of Tc=10 min

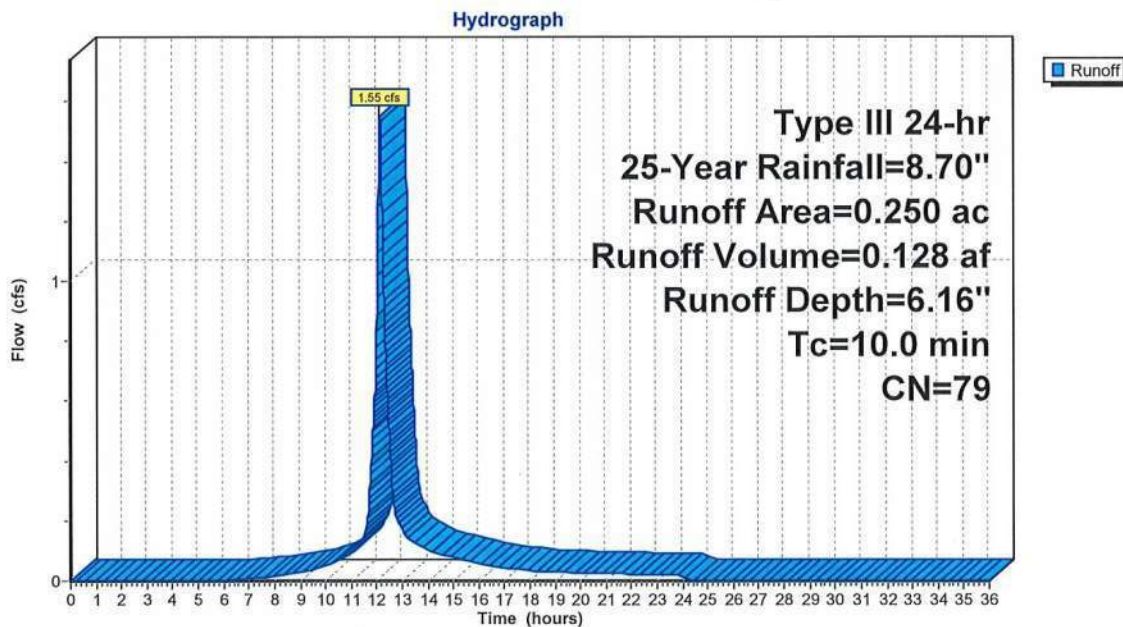
Runoff = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SS1: C1SS1 Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1SS2: C1SS2 Drainage Area**

Use Conservative Value of Tc=10 min

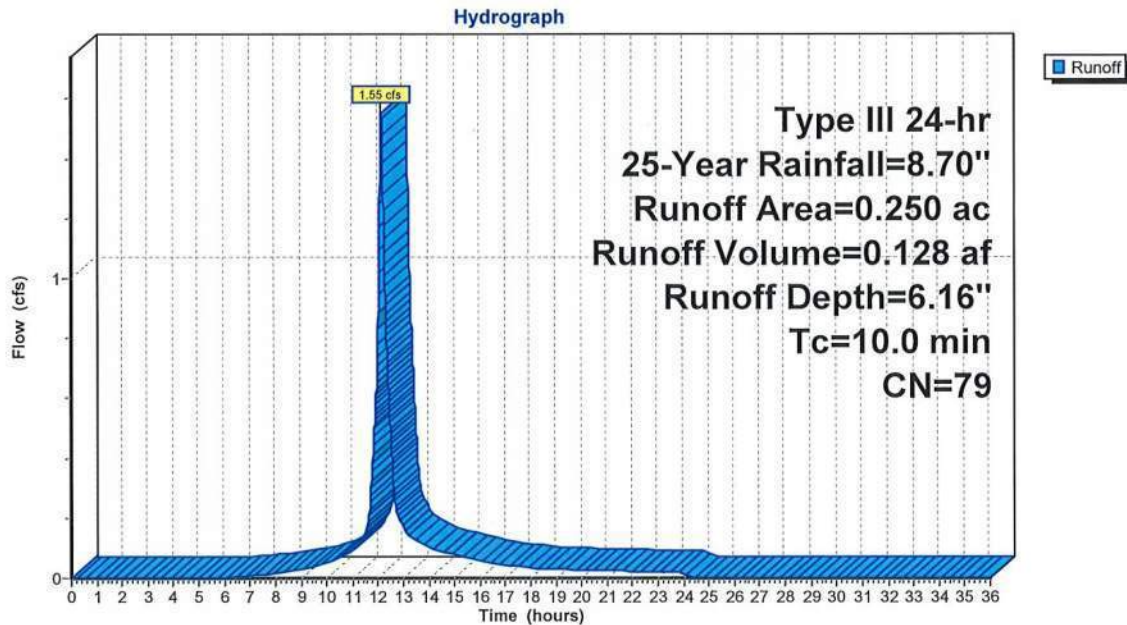
Runoff = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SS2: C1SS2 Drainage Area**





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1T: C1 Drainage Area**

Runoff = 36.29 cfs @ 12.17 hrs, Volume= 3.231 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

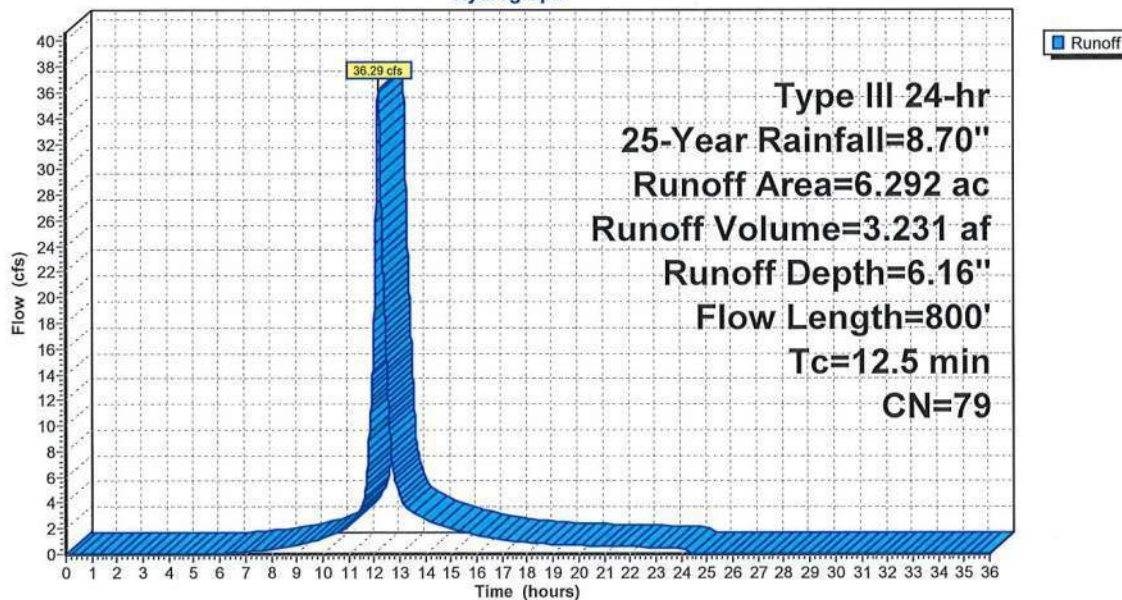
Area (ac)	CN	Description
6.292	79	50-75% Grass cover, Fair, HSG C
6.292		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C1 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800	Total			

**Subcatchment C1T: C1 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C2S: C2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 62.41 cfs @ 12.14 hrs, Volume= 5.155 af, Depth= 6.16"

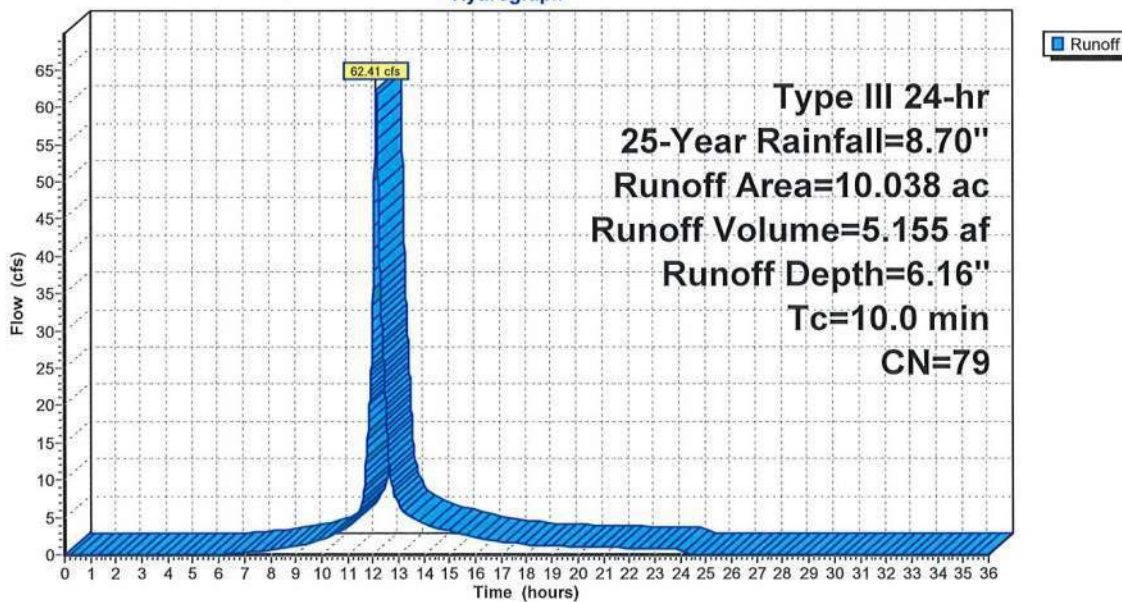
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
10.038	79	50-75% Grass cover, Fair, HSG C
10.038		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C2 Drainage Area

**Subcatchment C2S: C2 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C2T: C2 Drainage Area**

Runoff = 30.27 cfs @ 12.17 hrs, Volume= 2.696 af, Depth= 6.16"

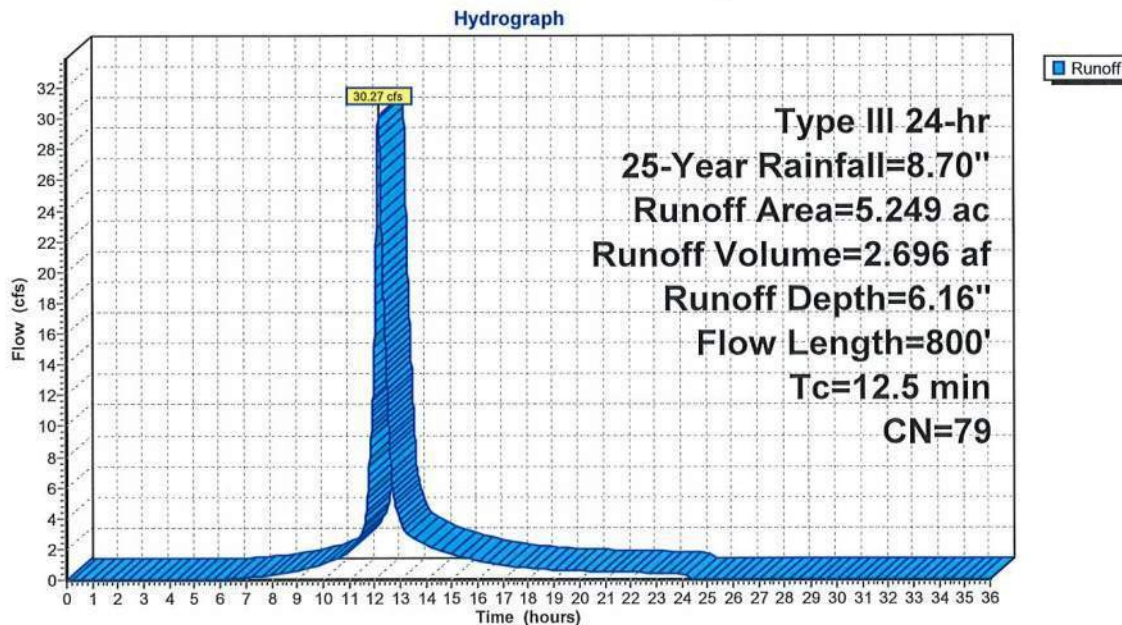
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
5.249	79	50-75% Grass cover, Fair, HSG C
5.249		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C2 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800	Total			

**Subcatchment C2T: C2 Drainage Area**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C3: C3 Drainage Area**

Existing Drainage Area Surface Drains to the North, Into Existing Low-Lying Excavated Pit C4 Drainage Area.

Runoff = 24.05 cfs @ 12.14 hrs, Volume= 2.045 af, Depth= 7.01"

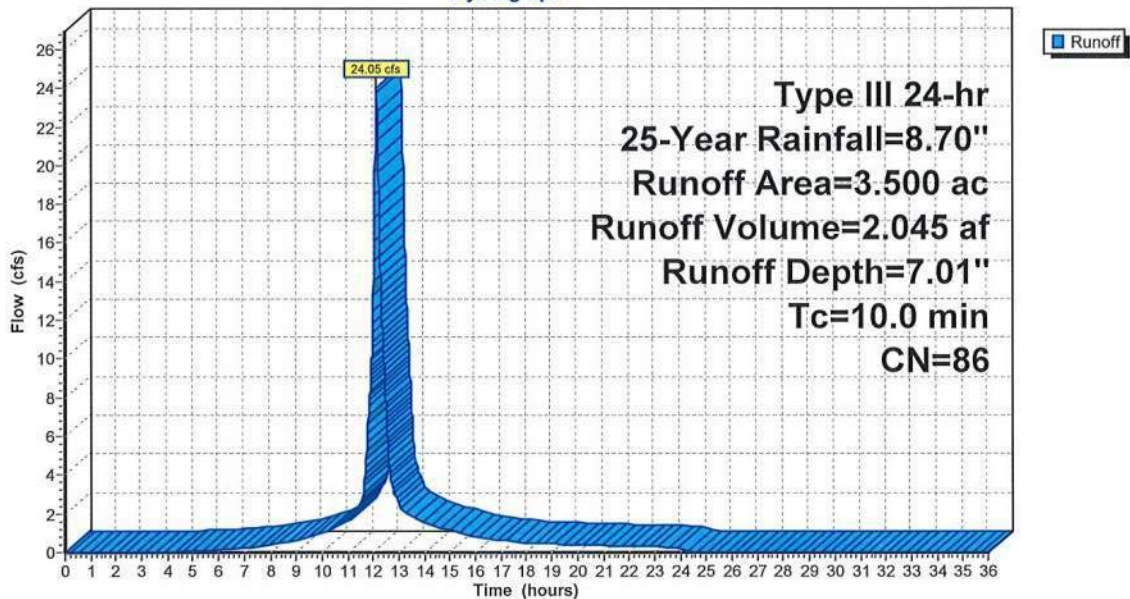
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
3.500	86	<50% Grass cover, Poor, HSG C
3.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C3 Drainage Area

**Subcatchment C3: C3 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C4: C4 Drainage Area**

Existing Low-Lying Excavated Pit Area. Infiltration and Evaporation Occur Here.

Runoff = 65.28 cfs @ 12.14 hrs, Volume= 5.551 af, Depth= 7.01"

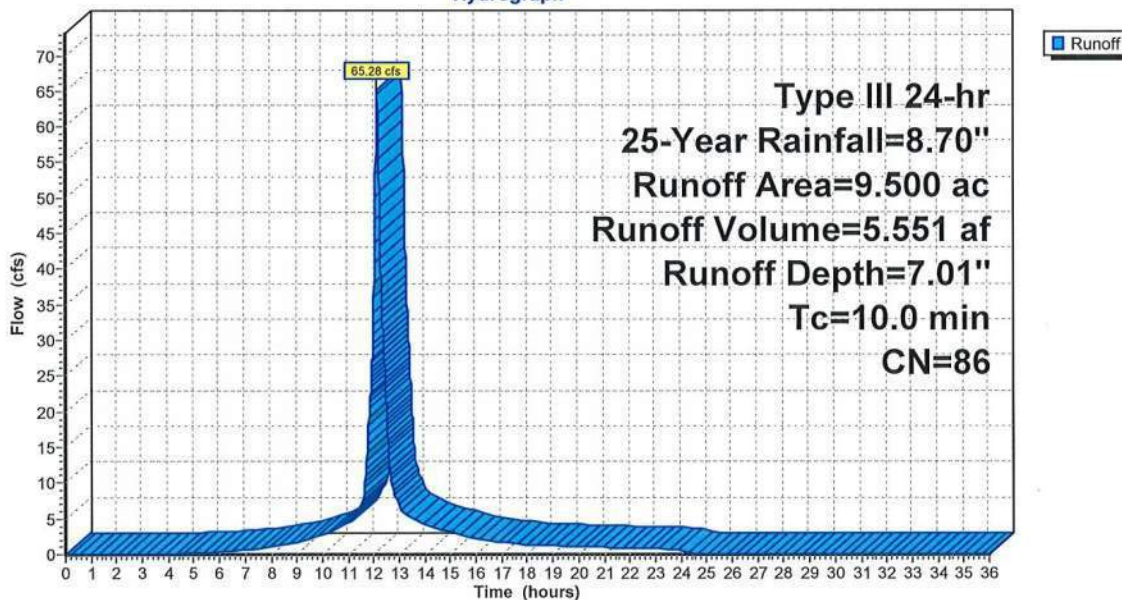
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
9.500	86	<50% Grass cover, Poor, HSG C
9.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C4 Drainage Area

**Subcatchment C4: C4 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C5: C5 Drainage Area**

Side Slope Drainage Area that Flows Into Pond C.

Runoff = 18.49 cfs @ 12.14 hrs, Volume= 1.572 af, Depth= 7.01"

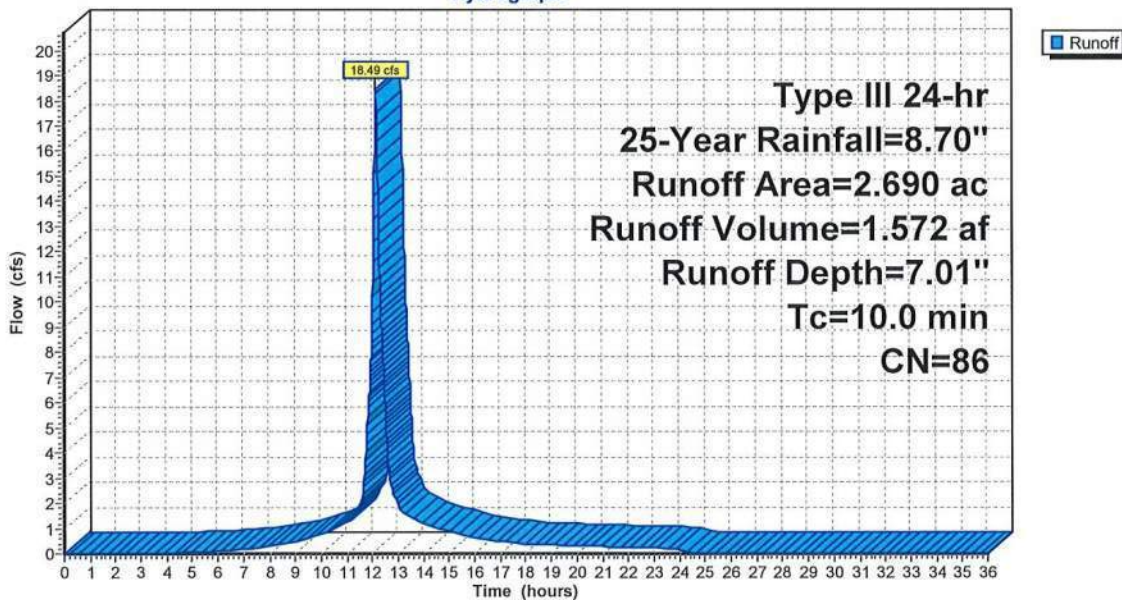
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
2.690	86	<50% Grass cover, Poor, HSG C
2.690		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C5 Drainage Area

**Subcatchment C5: C5 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C6: C6 Drainage Area**

Surrounding Drainage Area that Flows Into Pond A.

Runoff = 27.36 cfs @ 12.14 hrs, Volume= 2.327 af, Depth= 7.01"

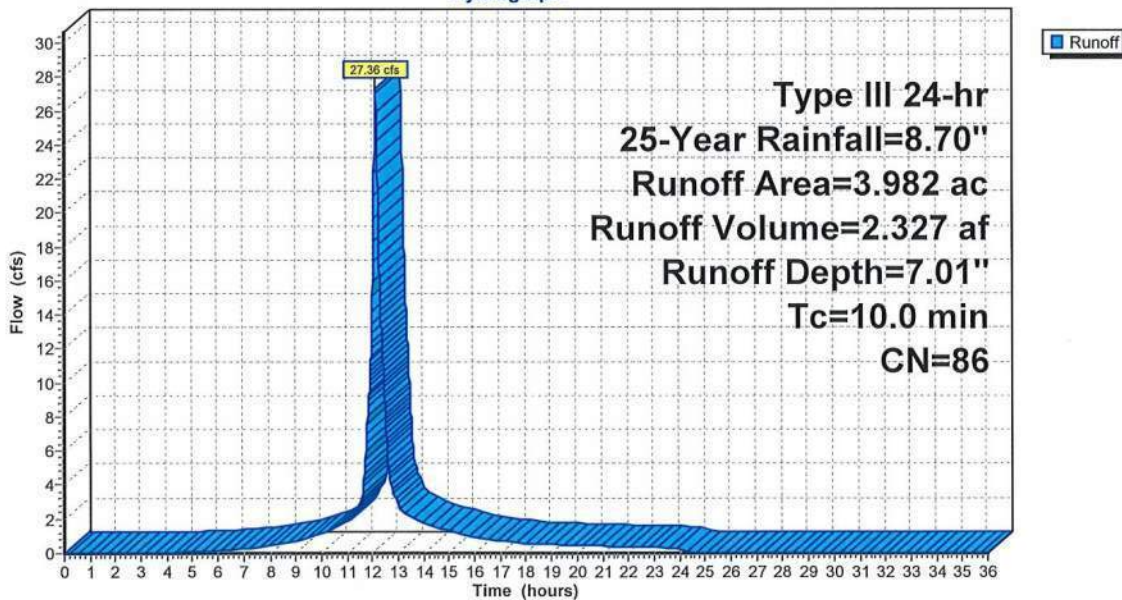
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
3.982	86	<50% Grass cover, Poor, HSG C
3.982		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C6 Drainage Area

**Subcatchment C6: C6 Drainage Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PAR: PA Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 77.55 cfs @ 12.00 hrs, Volume= 5.245 af, Depth= 8.46"

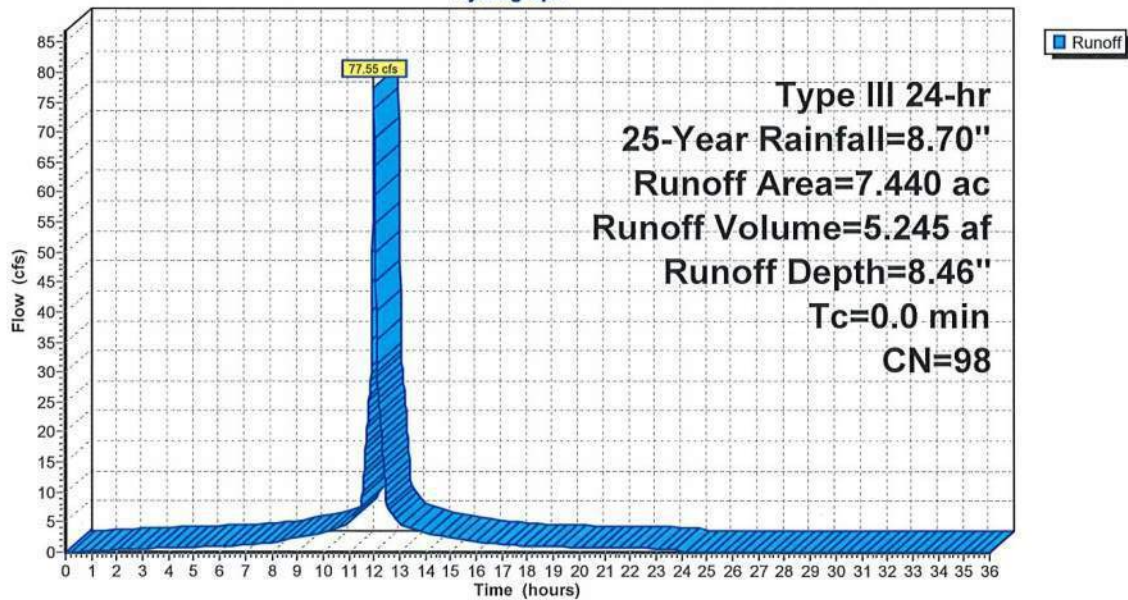
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
7.440	98	Water Surface, 0% imp, HSG C
7.440		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond A

**Subcatchment PAR: PA Rainfall Area**

Hydrograph





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PBR: PB Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 44.71 cfs @ 12.00 hrs, Volume= 3.024 af, Depth= 8.46"

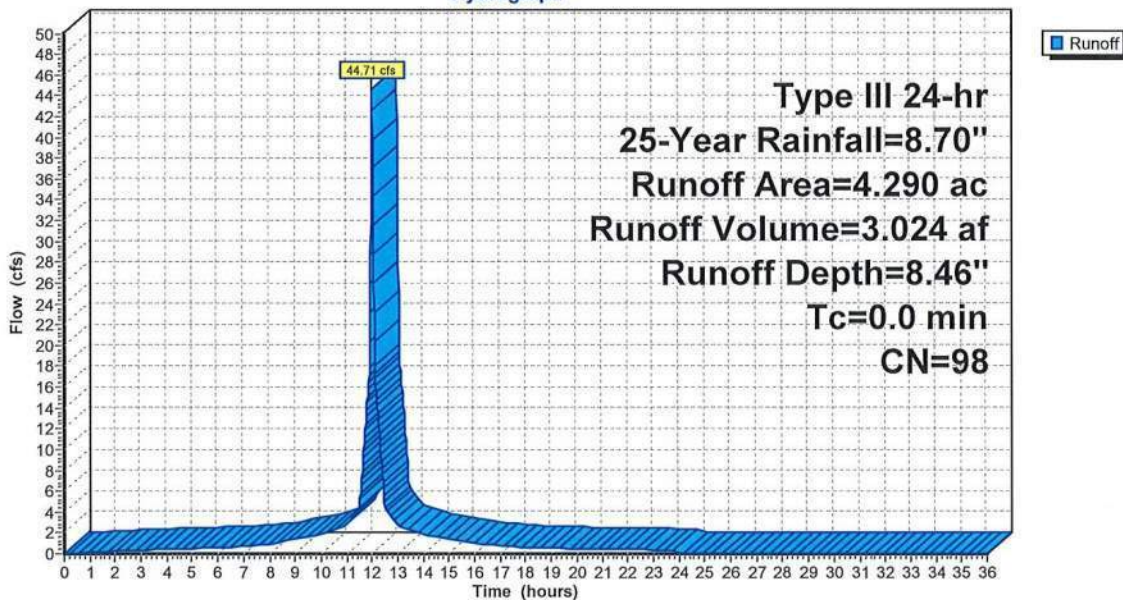
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
4.290	98	Water Surface, 0% imp, HSG C
4.290		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond B

**Subcatchment PBR: PB Rainfall Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment PCR: PC Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 47.32 cfs @ 12.00 hrs, Volume= 3.201 af, Depth= 8.46"

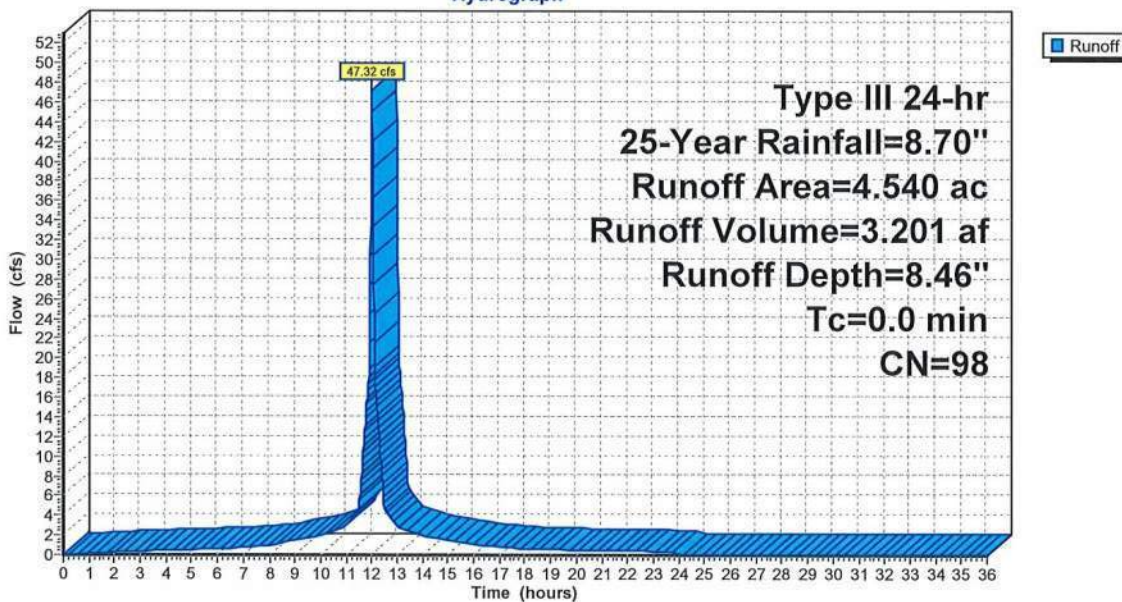
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
4.540	98	Water Surface, 0% imp, HSG C
4.540		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond C

**Subcatchment PCR: PC Rainfall Area**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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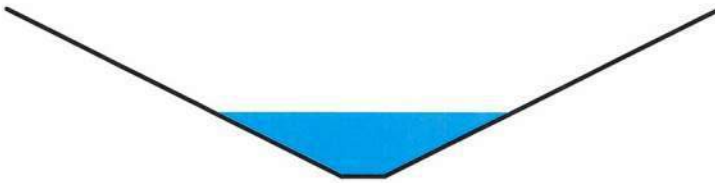
**Summary for Reach 1CC: 1CC Collector Channel**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 213.11 cfs @ 12.17 hrs, Volume= 19.540 af  
 Outflow = 211.91 cfs @ 12.20 hrs, Volume= 19.540 af, Atten= 1%, Lag= 1.7 min

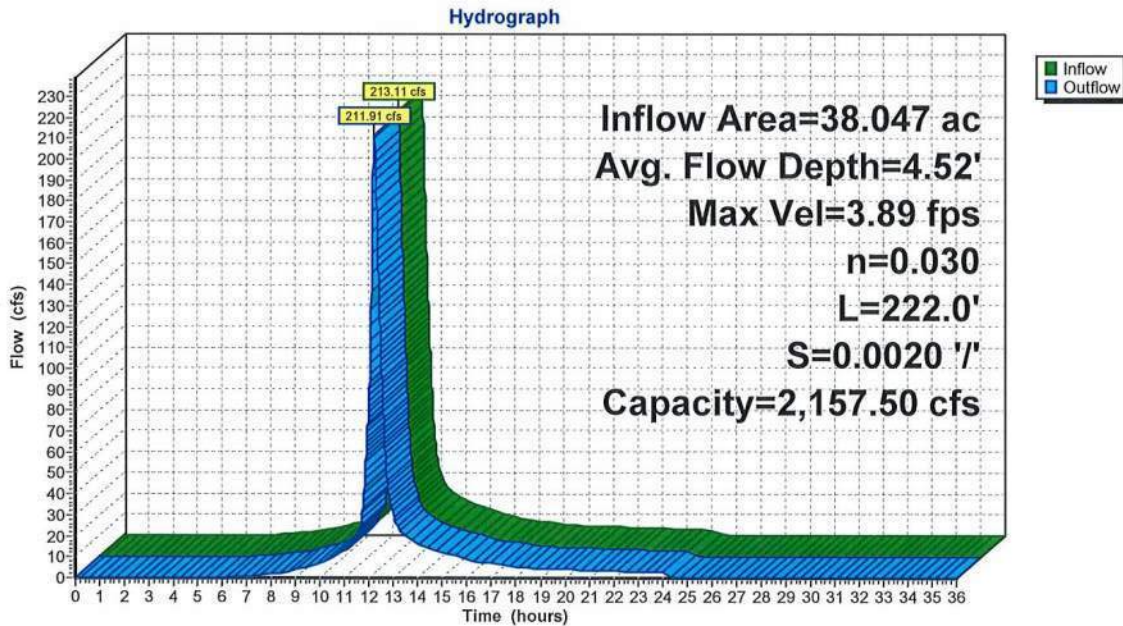
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.89 fps, Min. Travel Time= 1.0 min  
 Avg. Velocity = 1.32 fps, Avg. Travel Time= 2.8 min

Peak Storage= 12,092 cf @ 12.19 hrs  
 Average Depth at Peak Storage= 4.52'  
 Bank-Full Depth= 11.73' Flow Area= 310.4 sf, Capacity= 2,157.50 cfs

3.00' x 11.73' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 49.92'  
 Length= 222.0' Slope= 0.0020 '/'  
 Inlet Invert= 53.89', Outlet Invert= 53.45'



**Reach 1CC: 1CC Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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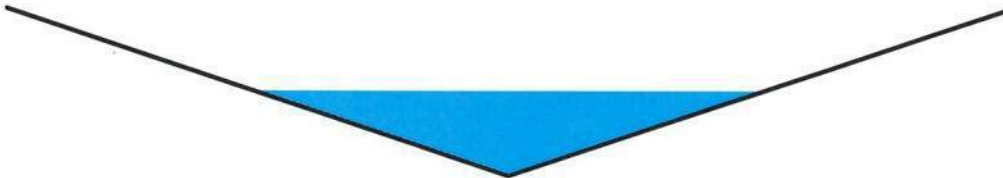
**Summary for Reach 2CC: 2CC Collector Channel**

Inflow Area = 1.480 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 9.20 cfs @ 12.14 hrs, Volume= 0.760 af  
 Outflow = 7.72 cfs @ 12.32 hrs, Volume= 0.760 af, Atten= 16%, Lag= 11.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.58 fps, Min. Travel Time= 6.8 min  
 Avg. Velocity = 0.52 fps, Avg. Travel Time= 20.9 min

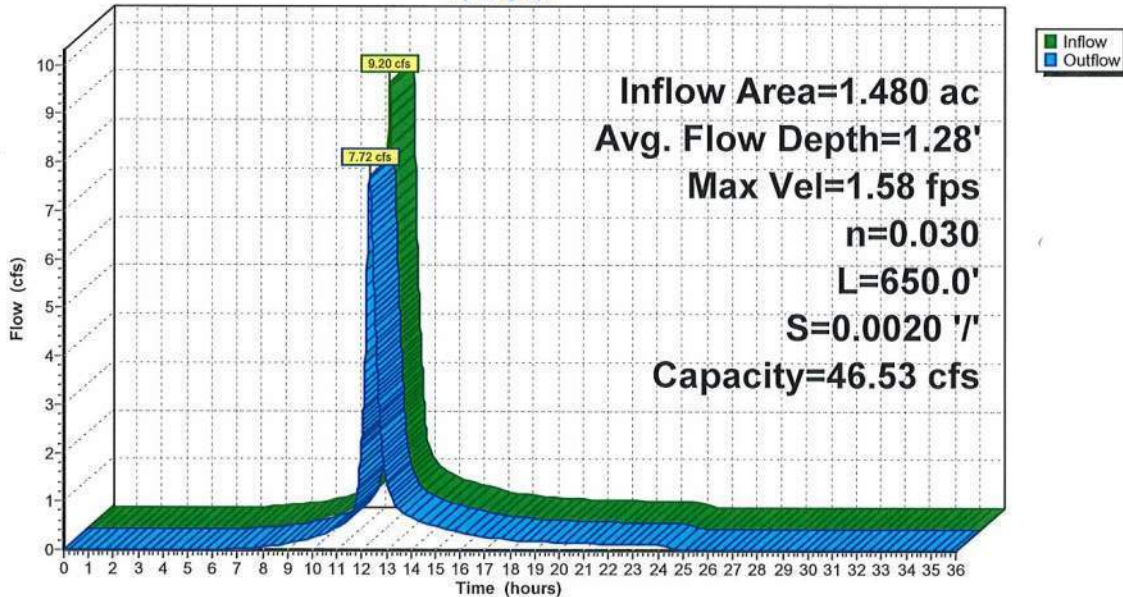
Peak Storage= 3,170 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 1.28'  
 Bank-Full Depth= 2.50' Flow Area= 18.8 sf, Capacity= 46.53 cfs

0.00' x 2.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 3.0 '/' Top Width= 15.00'  
 Length= 650.0' Slope= 0.0020 '/'  
 Inlet Invert= 54.50', Outlet Invert= 53.20'



**Reach 2CC: 2CC Collector Channel**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach 5CC: A2 Collector Channel**

Inflow Area = 1.000 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af  
 Outflow = 5.17 cfs @ 12.33 hrs, Volume= 0.514 af, Atten= 17%, Lag= 11.5 min

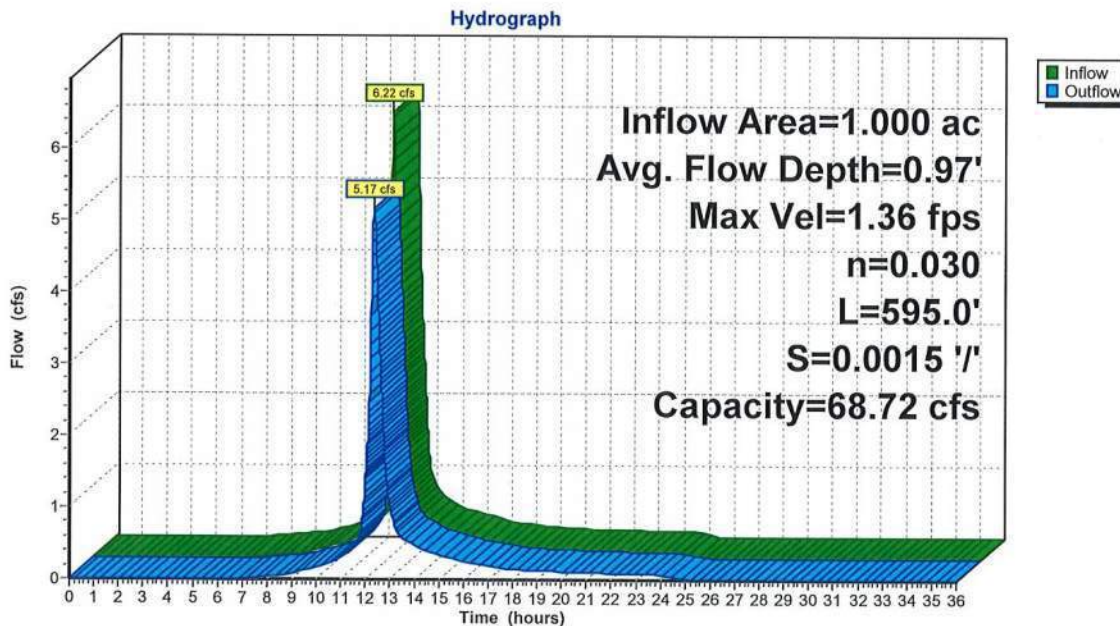
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.36 fps, Min. Travel Time= 7.3 min  
 Avg. Velocity = 0.42 fps, Avg. Travel Time= 23.7 min

Peak Storage= 2,258 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 0.97'  
 Bank-Full Depth= 3.14' Flow Area= 26.0 sf, Capacity= 68.72 cfs

2.00' x 3.14' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 14.56'  
 Length= 595.0' Slope= 0.0015 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.61'



**Reach 5CC: A2 Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach 6CC: A3 Collector Channel**

Inflow Area = 1.000 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 6.22 cfs @ 12.14 hrs, Volume= 0.514 af  
 Outflow = 5.34 cfs @ 12.30 hrs, Volume= 0.514 af, Atten= 14%, Lag= 10.0 min

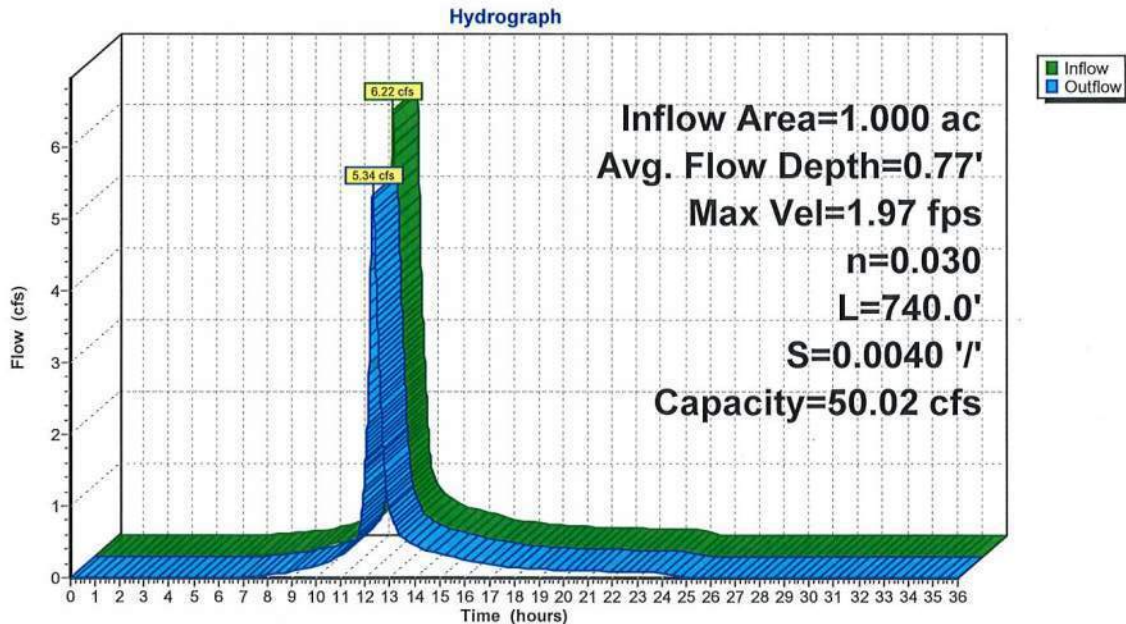
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.97 fps, Min. Travel Time= 6.3 min  
 Avg. Velocity= 0.58 fps, Avg. Travel Time= 21.1 min

Peak Storage= 2,006 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 0.77'  
 Bank-Full Depth= 2.21' Flow Area= 14.2 sf, Capacity= 50.02 cfs

2.00' x 2.21' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 10.84'  
 Length= 740.0' Slope= 0.0040 ' / '  
 Inlet Invert= 59.50', Outlet Invert= 56.54'



**Reach 6CC: A3 Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach A2-1: A2-1 Channel**

Inflow Area = 2.000 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 8.74 cfs @ 12.28 hrs, Volume= 1.027 af  
 Outflow = 8.70 cfs @ 12.35 hrs, Volume= 1.027 af, Atten= 0%, Lag= 3.9 min

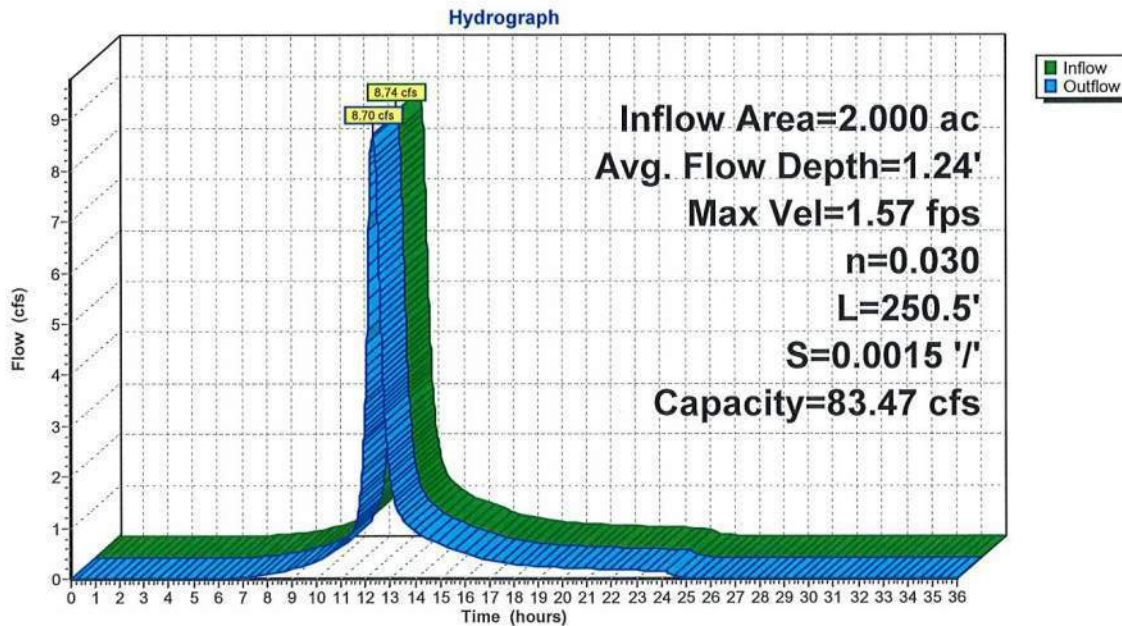
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.57 fps, Min. Travel Time= 2.7 min  
 Avg. Velocity= 0.51 fps, Avg. Travel Time= 8.2 min

Peak Storage= 1,387 cf @ 12.30 hrs  
 Average Depth at Peak Storage= 1.24'  
 Bank-Full Depth= 3.40' Flow Area= 29.9 sf, Capacity= 83.47 cfs

2.00' x 3.40' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 15.60'  
 Length= 250.5' Slope= 0.0015 '/'  
 Inlet Invert= 57.61', Outlet Invert= 57.23'



**Reach A2-1: A2-1 Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach A2-2: A2-2 Channel**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 114.51 cfs @ 12.15 hrs, Volume= 9.943 af  
 Outflow = 113.50 cfs @ 12.19 hrs, Volume= 9.943 af, Atten= 1%, Lag= 2.0 min

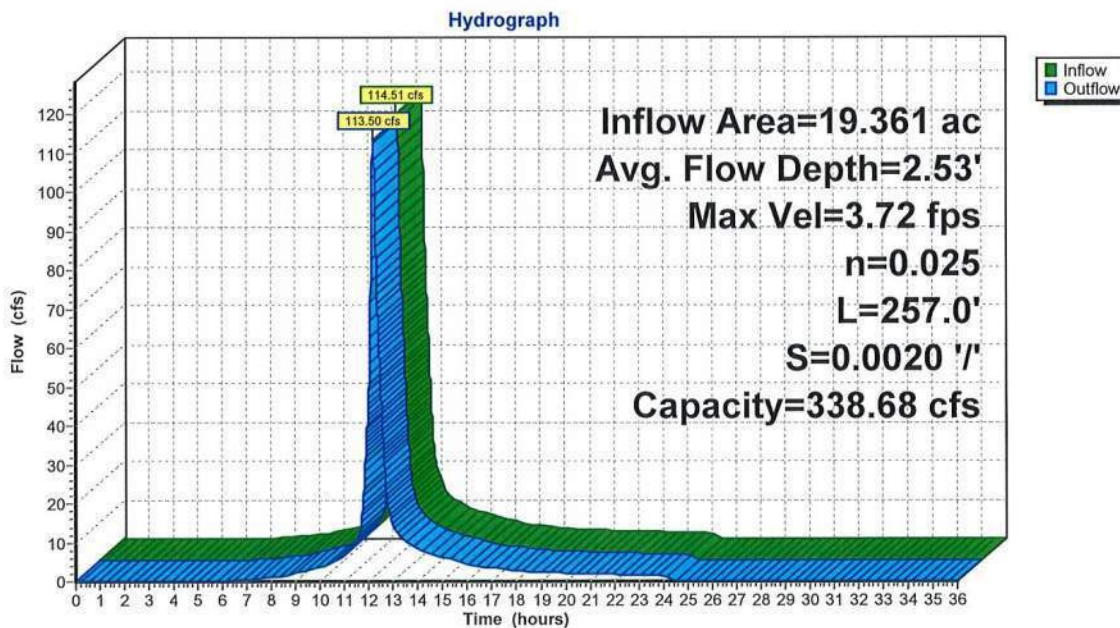
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.72 fps, Min. Travel Time= 1.2 min  
 Avg. Velocity = 1.00 fps, Avg. Travel Time= 4.3 min

Peak Storage= 7,841 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 2.53'  
 Bank-Full Depth= 4.34' Flow Area= 68.1 sf, Capacity= 338.68 cfs

7.00' x 4.34' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 2.0 ' / ' Top Width= 24.36'  
 Length= 257.0' Slope= 0.0020 ' / '  
 Inlet Invert= 55.84', Outlet Invert= 55.33'



**Reach A2-2: A2-2 Channel**





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach A2-3: A2-3 Channel**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 113.50 cfs @ 12.19 hrs, Volume= 9.943 af  
 Outflow = 108.05 cfs @ 12.27 hrs, Volume= 9.943 af, Atten= 5%, Lag= 5.2 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.19 fps, Min. Travel Time= 3.0 min  
 Avg. Velocity = 0.86 fps, Avg. Travel Time= 11.3 min

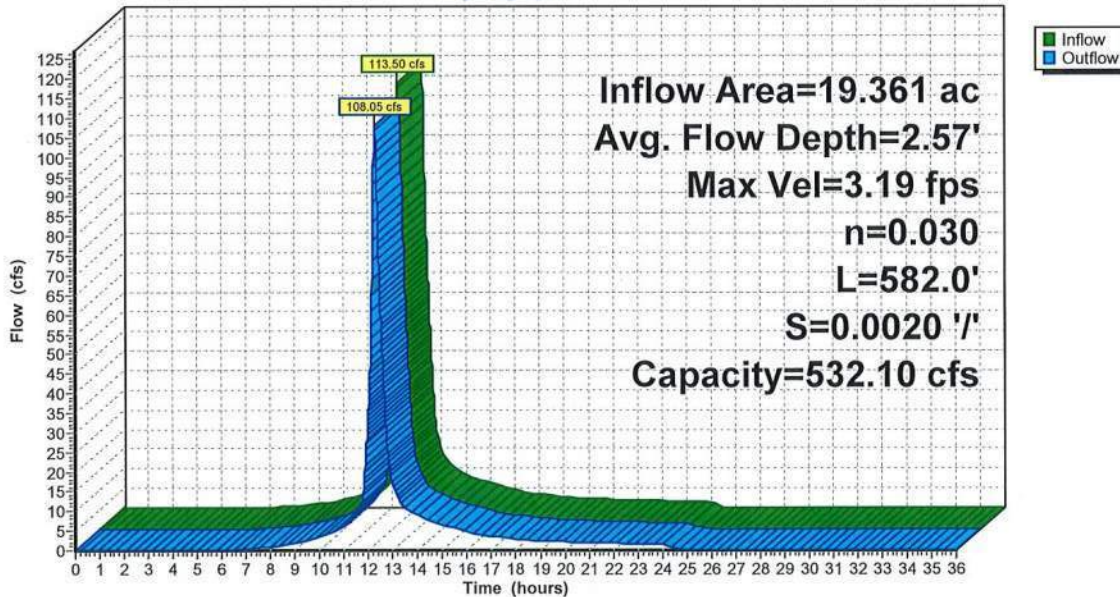
Peak Storage= 19,700 cf @ 12.22 hrs  
 Average Depth at Peak Storage= 2.57'  
 Bank-Full Depth= 5.65' Flow Area= 109.0 sf, Capacity= 532.10 cfs

8.00' x 5.65' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/ Top Width= 30.60'  
 Length= 582.0' Slope= 0.0020 '/  
 Inlet Invert= 55.33', Outlet Invert= 54.17'



**Reach A2-3: A2-3 Channel**

**Hydrograph**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach A2-4: Chute-Concrete Block Open Cell**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 108.05 cfs @ 12.27 hrs, Volume= 9.943 af  
 Outflow = 107.90 cfs @ 12.28 hrs, Volume= 9.943 af, Atten= 0%, Lag= 0.6 min

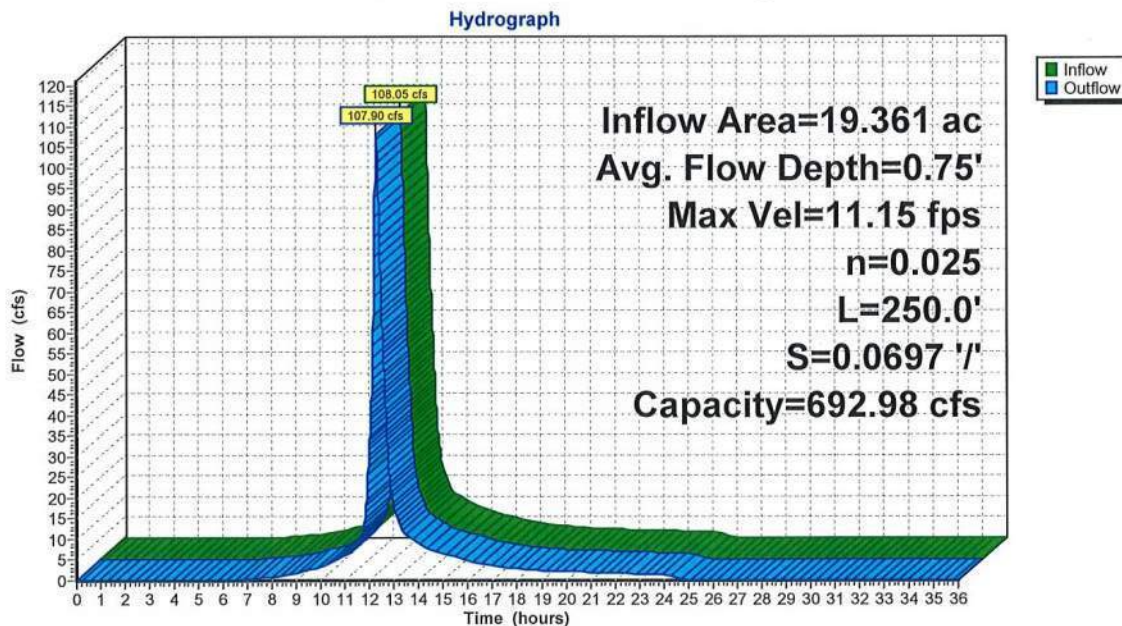
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 11.15 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 2.81 fps, Avg. Travel Time= 1.5 min

Peak Storage= 2,420 cf @ 12.28 hrs  
 Average Depth at Peak Storage= 0.75'  
 Bank-Full Depth= 2.00' Flow Area= 36.0 sf, Capacity= 692.98 cfs

10.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 26.00'  
 Length= 250.0' Slope= 0.0697 '/'  
 Inlet Invert= 54.17', Outlet Invert= 36.75'



**Reach A2-4: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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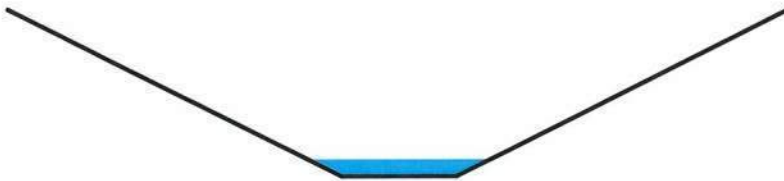
**Summary for Reach A2-5: Concrete Block-Channel Transition**

Inflow Area = 2.000 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 8.70 cfs @ 12.35 hrs, Volume= 1.027 af  
 Outflow = 8.70 cfs @ 12.35 hrs, Volume= 1.027 af, Atten= 0%, Lag= 0.0 min

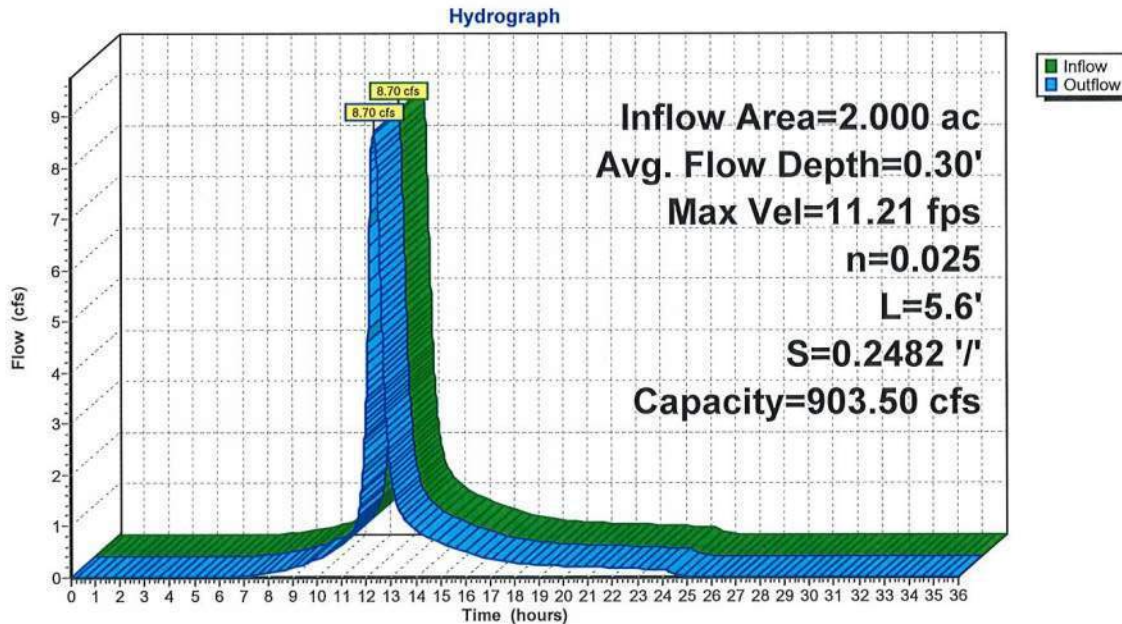
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 11.21 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity= 3.73 fps, Avg. Travel Time= 0.0 min

Peak Storage= 4 cf @ 12.35 hrs  
 Average Depth at Peak Storage= 0.30'  
 Bank-Full Depth= 2.93' Flow Area= 23.0 sf, Capacity= 903.50 cfs

2.00' x 2.93' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 2.0 '/ Top Width= 13.72'  
 Length= 5.6' Slope= 0.2482 '/  
 Inlet Invert= 57.23', Outlet Invert= 55.84'



**Reach A2-5: Concrete Block-Channel Transition**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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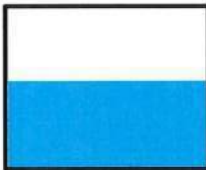
**Summary for Reach B1: 5' x 4' Box Culvert**

Inflow Area = 19.249 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 103.76 cfs @ 12.17 hrs, Volume= 9.886 af  
 Outflow = 103.38 cfs @ 12.20 hrs, Volume= 9.886 af, Atten= 0%, Lag= 1.5 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 9.54 fps, Min. Travel Time= 0.8 min  
 Avg. Velocity = 2.65 fps, Avg. Travel Time= 2.9 min

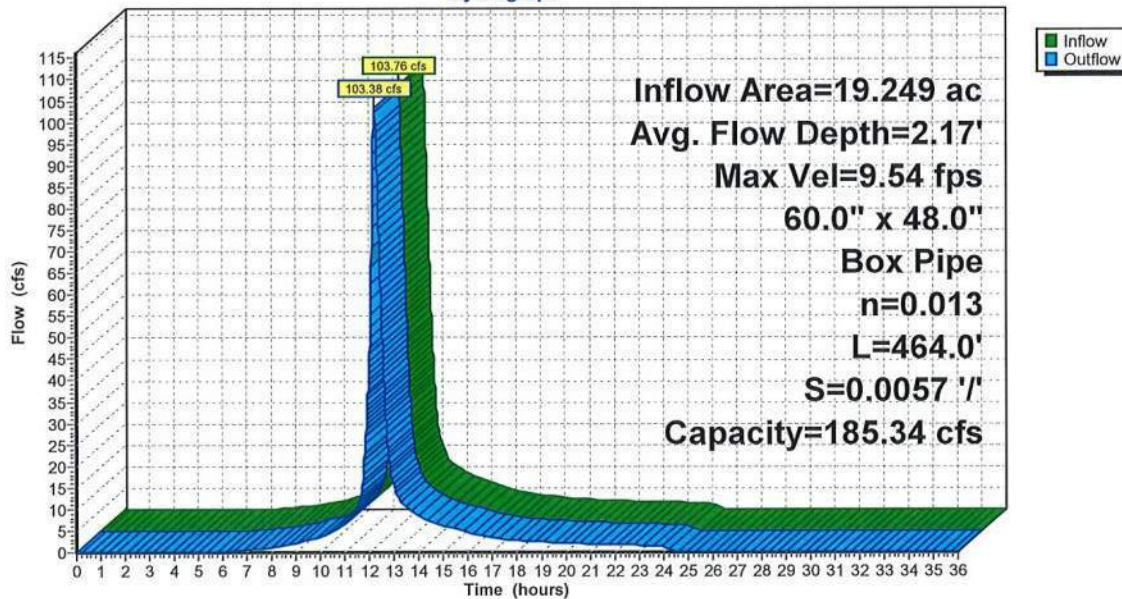
Peak Storage= 5,030 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 2.17'  
 Bank-Full Depth= 4.00' Flow Area= 20.0 sf, Capacity= 185.34 cfs

60.0" W x 48.0" H Box Pipe  
 n= 0.013 Concrete pipe, bends & connections  
 Length= 464.0' Slope= 0.0057 '/'  
 Inlet Invert= 56.54', Outlet Invert= 53.89'



**Reach B1: 5' x 4' Box Culvert**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach B2: 5' x 4' Box Culvert**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 211.91 cfs @ 12.20 hrs, Volume= 19.540 af  
 Outflow = 211.71 cfs @ 12.21 hrs, Volume= 19.540 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 17.67 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 4.94 fps, Avg. Travel Time= 0.7 min

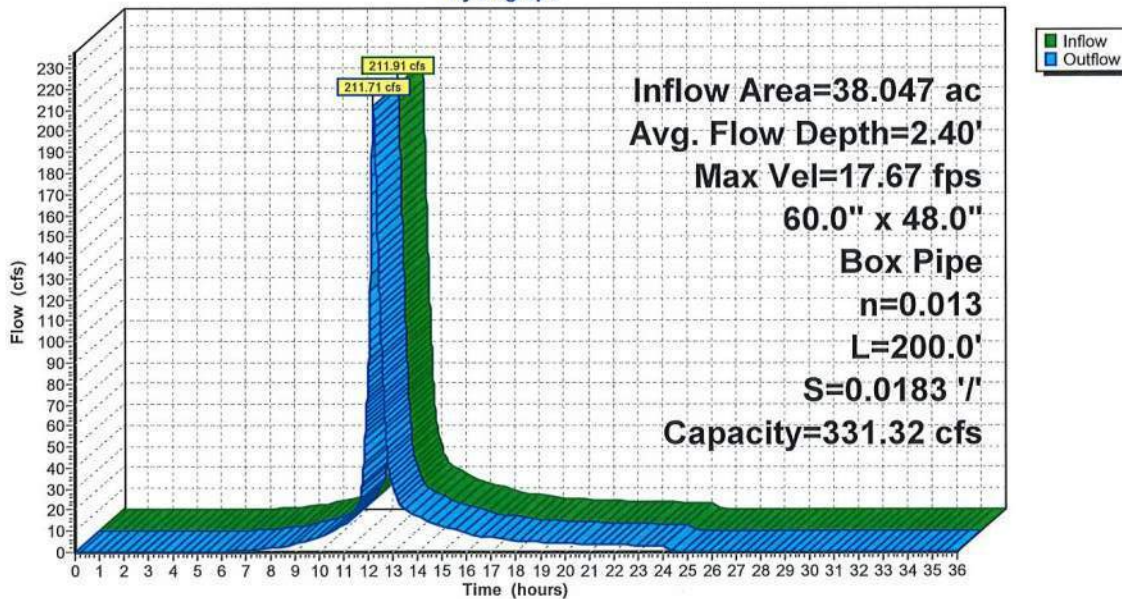
Peak Storage= 2,398 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 2.40'  
 Bank-Full Depth= 4.00' Flow Area= 20.0 sf, Capacity= 331.32 cfs

60.0" W x 48.0" H Box Pipe  
 n= 0.013 Concrete pipe, bends & connections  
 Length= 200.0' Slope= 0.0183 '/'  
 Inlet Invert= 53.45', Outlet Invert= 49.80'



**Reach B2: 5' x 4' Box Culvert**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C1-4: Chute-Concrete Block Open Cell**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 211.71 cfs @ 12.21 hrs, Volume= 19.540 af  
 Outflow = 211.66 cfs @ 12.21 hrs, Volume= 19.540 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 23.03 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 6.80 fps, Avg. Travel Time= 0.2 min

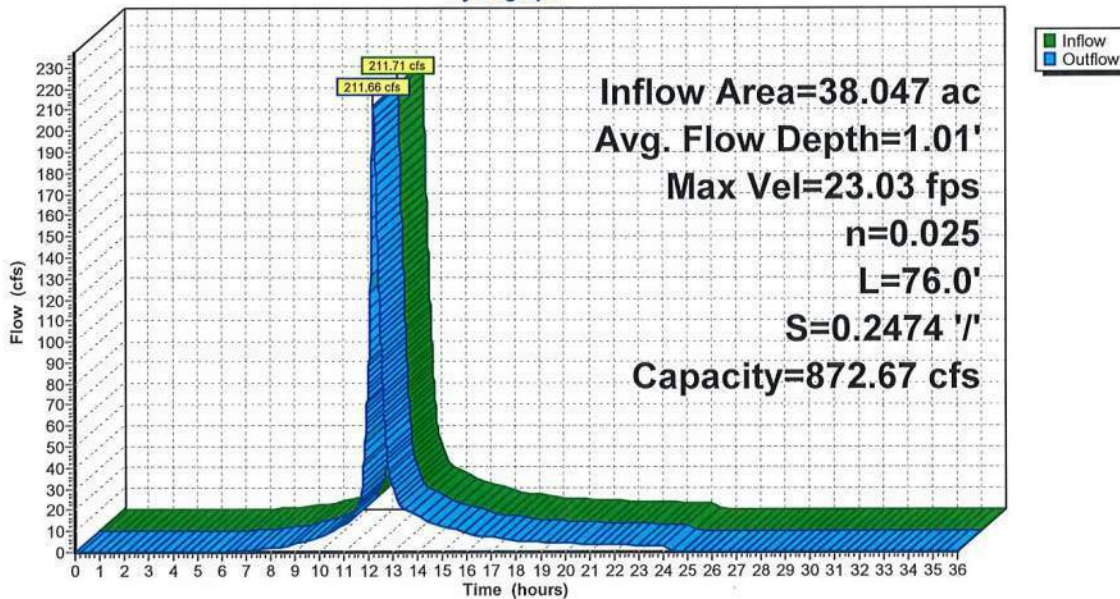
Peak Storage= 699 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 1.01'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 872.67 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 76.0' Slope= 0.2474 '/'  
 Inlet Invert= 49.80', Outlet Invert= 31.00'



**Reach C1-4: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C1SCCN1: C1SCCN1 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af  
 Outflow = 1.44 cfs @ 12.25 hrs, Volume= 0.128 af, Atten= 7%, Lag= 6.5 min

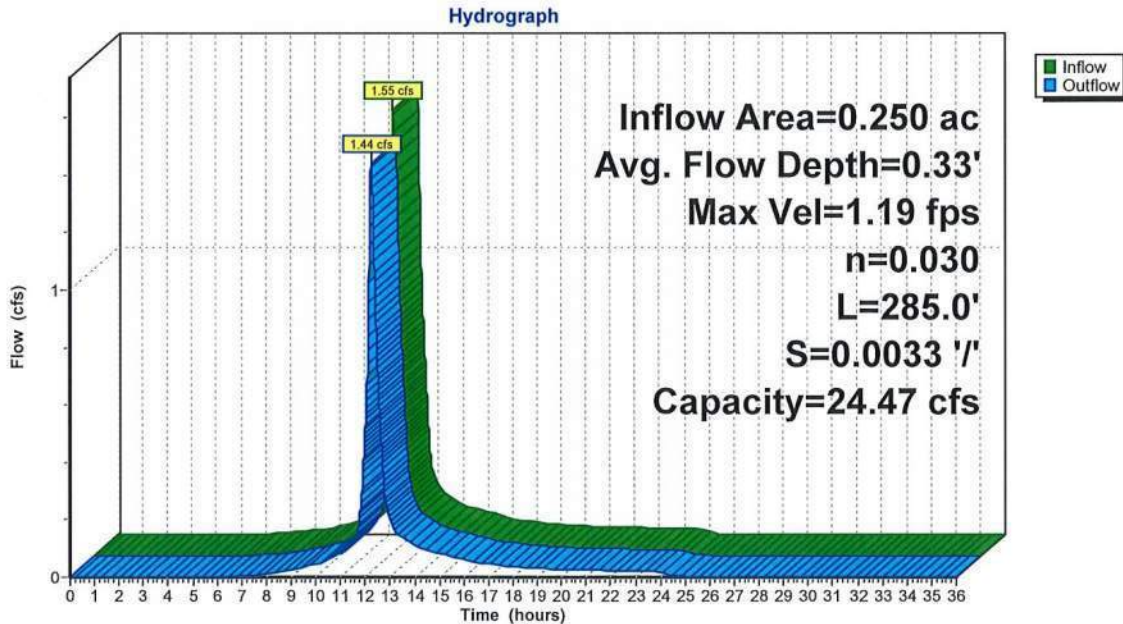
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.19 fps, Min. Travel Time= 4.0 min  
 Avg. Velocity = 0.33 fps, Avg. Travel Time= 14.4 min

Peak Storage= 344 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 0.33'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.47 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 9.00'  
 Length= 285.0' Slope= 0.0033 '/'  
 Inlet Invert= 58.50', Outlet Invert= 57.55'



**Reach C1SCCN1: C1SCCN1 Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C1SCCN2: C1SCCN2 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af  
 Outflow = 1.44 cfs @ 12.25 hrs, Volume= 0.128 af, Atten= 7%, Lag= 6.6 min

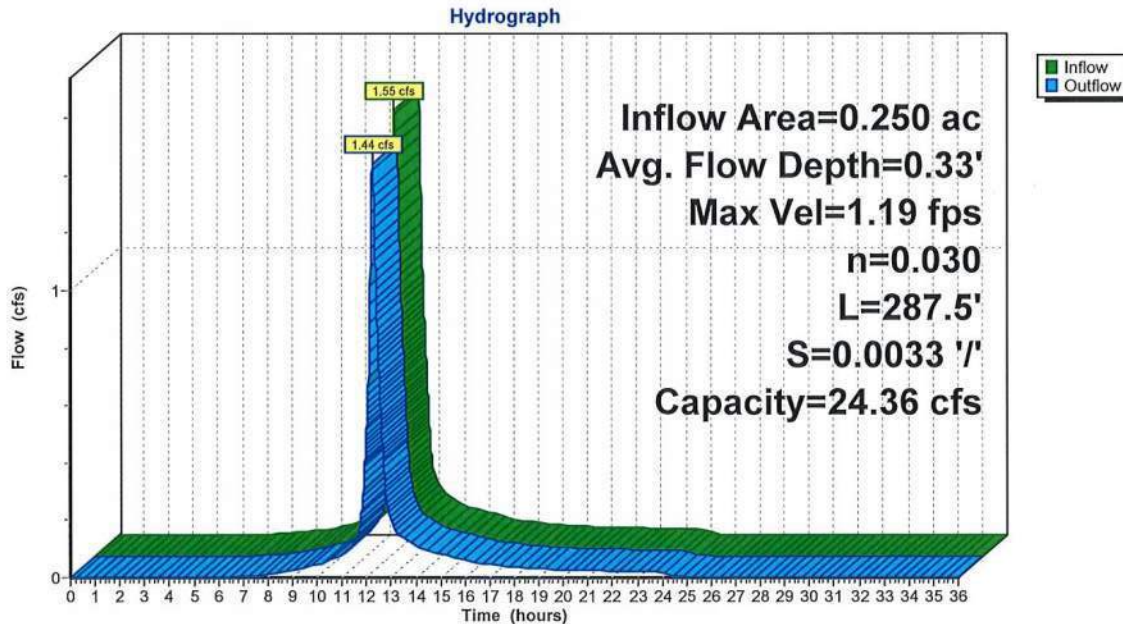
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.19 fps, Min. Travel Time= 4.0 min  
 Avg. Velocity = 0.33 fps, Avg. Travel Time= 14.6 min

Peak Storage= 348 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 0.33'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.36 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 9.00'  
 Length= 287.5' Slope= 0.0033 '/'  
 Inlet Invert= 58.50', Outlet Invert= 57.55'



**Reach C1SCCN2: C1SCCN2 Collector Channel**





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C1SCCS1: C1SCCS1 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af  
 Outflow = 1.44 cfs @ 12.24 hrs, Volume= 0.128 af, Atten= 7%, Lag= 6.4 min

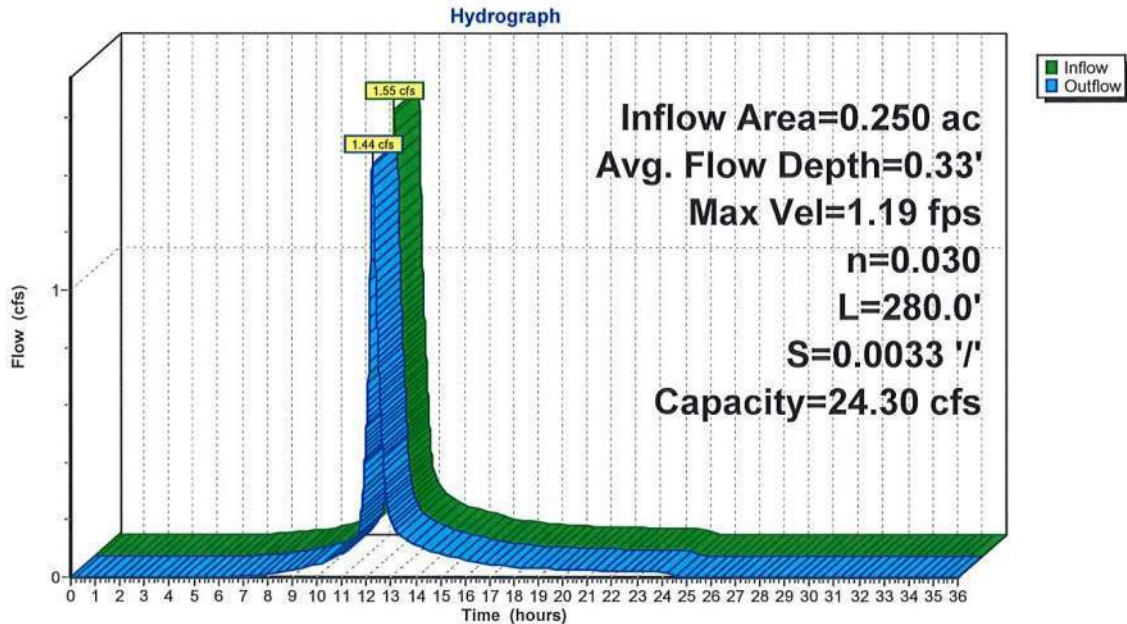
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.19 fps, Min. Travel Time= 3.9 min  
 Avg. Velocity = 0.33 fps, Avg. Travel Time= 14.2 min

Peak Storage= 340 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 0.33'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.30 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 9.00'  
 Length= 280.0' Slope= 0.0033 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.58'



**Reach C1SCCS1: C1SCCS1 Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C1SCCS2: C1SCCS2 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 1.55 cfs @ 12.14 hrs, Volume= 0.128 af  
 Outflow = 1.44 cfs @ 12.24 hrs, Volume= 0.128 af, Atten= 7%, Lag= 6.4 min

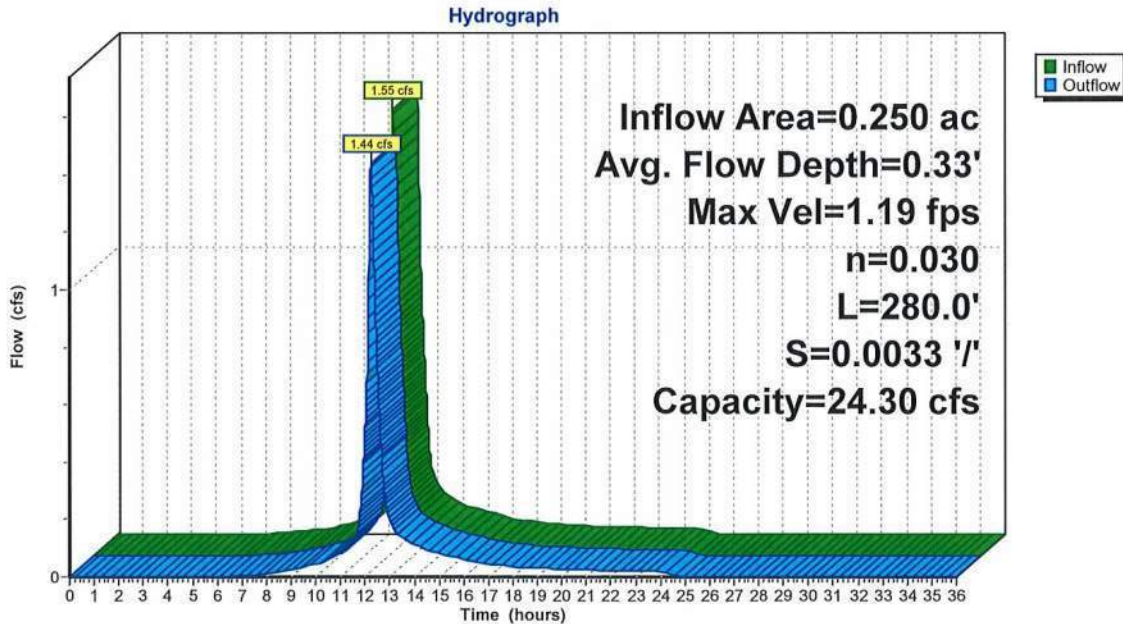
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.19 fps, Min. Travel Time= 3.9 min  
 Avg. Velocity= 0.33 fps, Avg. Travel Time= 14.2 min

Peak Storage= 340 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 0.33'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.30 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 9.00'  
 Length= 280.0' Slope= 0.0033 '/'  
 Inlet Invert= 58.50', Outlet Invert= 57.58'



**Reach C1SCCS2: C1SCCS2 Collector Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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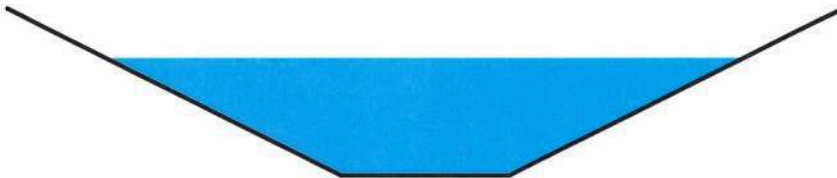
**Summary for Reach C2-3: C2-3 Channel**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 91.74 cfs @ 12.16 hrs, Volume= 7.851 af  
 Outflow = 82.99 cfs @ 12.29 hrs, Volume= 7.851 af, Atten= 10%, Lag= 8.1 min

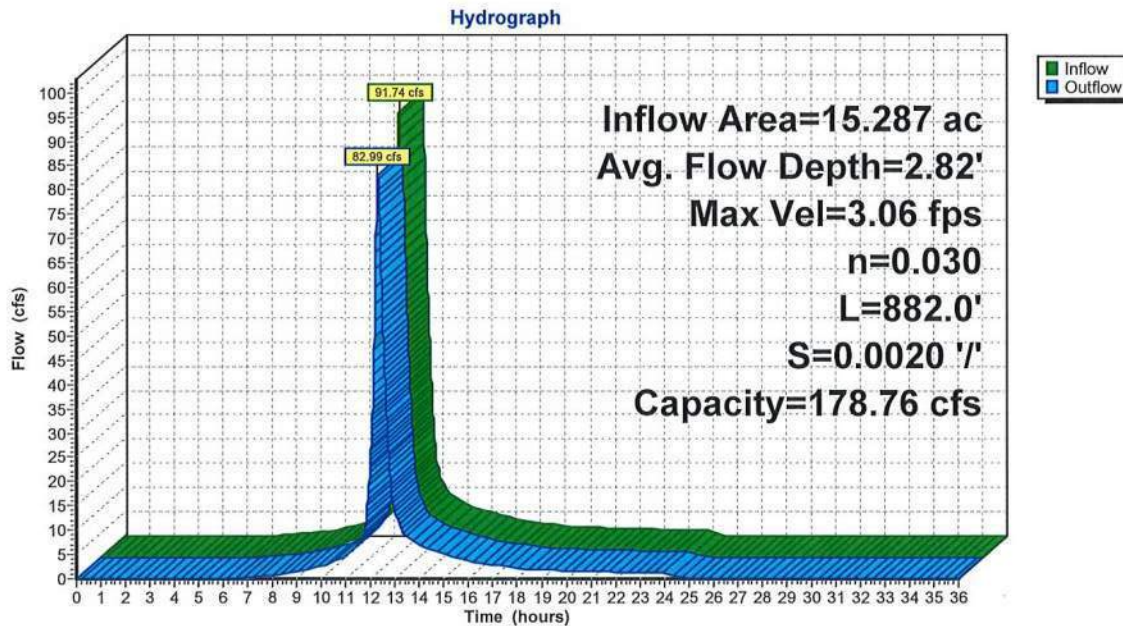
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.06 fps, Min. Travel Time= 4.8 min  
 Avg. Velocity = 0.88 fps, Avg. Travel Time= 16.8 min

Peak Storage= 23,911 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 2.82'  
 Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 178.76 cfs

4.00' x 4.00' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 20.00'  
 Length= 882.0' Slope= 0.0020 '/'  
 Inlet Invert= 53.50', Outlet Invert= 51.75'



**Reach C2-3: C2-3 Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C2-4: Chute-Concrete Block Open Cell**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 82.89 cfs @ 12.30 hrs, Volume= 7.851 af  
 Outflow = 82.88 cfs @ 12.30 hrs, Volume= 7.851 af, Atten= 0%, Lag= 0.1 min

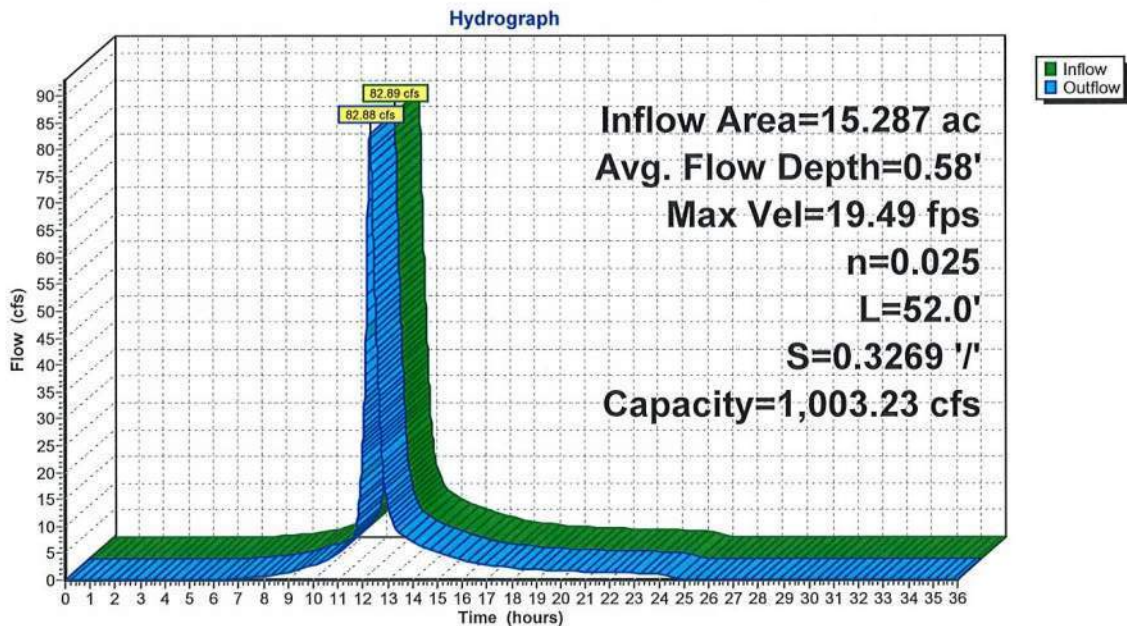
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.49 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 5.37 fps, Avg. Travel Time= 0.2 min

Peak Storage= 221 cf @ 12.30 hrs  
 Average Depth at Peak Storage= 0.58'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 1,003.23 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 52.0' Slope= 0.3269 '/'  
 Inlet Invert= 48.00', Outlet Invert= 31.00'



**Reach C2-4: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach C2-5: C2-5 Channel**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 82.96 cfs @ 12.29 hrs, Volume= 7.851 af  
 Outflow = 82.89 cfs @ 12.30 hrs, Volume= 7.851 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 8.22 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity= 2.31 fps, Avg. Travel Time= 0.8 min

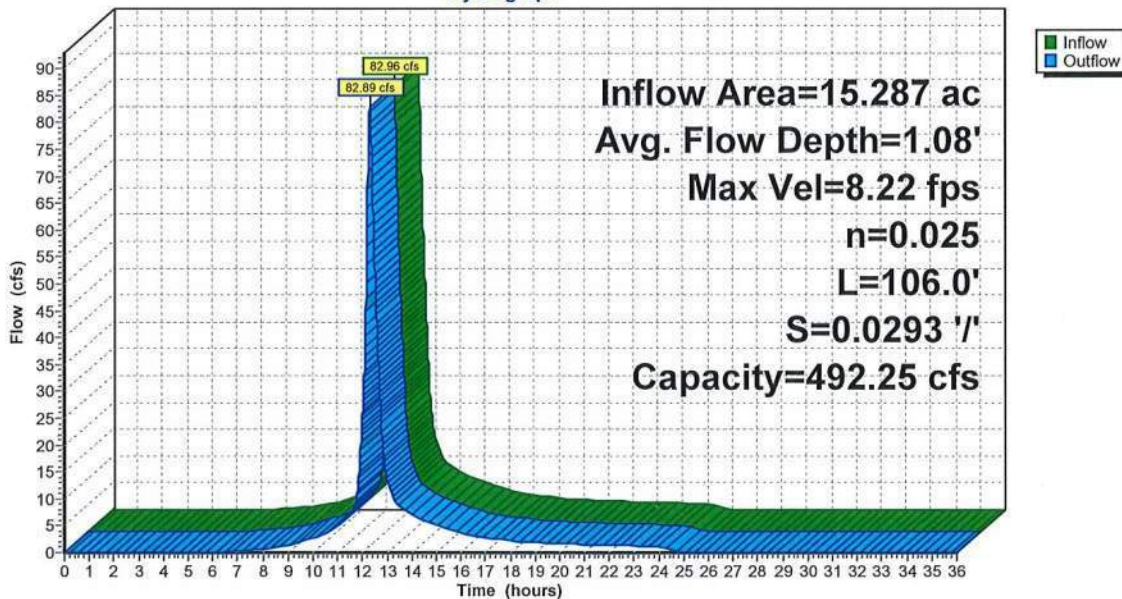
Peak Storage= 1,070 cf @ 12.30 hrs  
 Average Depth at Peak Storage= 1.08'  
 Bank-Full Depth= 2.50' Flow Area= 37.5 sf, Capacity= 492.25 cfs

5.00' x 2.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 25.00'  
 Length= 106.0' Slope= 0.0293 '/'  
 Inlet Invert= 51.11', Outlet Invert= 48.00'



**Reach C2-5: C2-5 Channel**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach CC: Chute-Concrete Block Open Cell**

Inflow Area = 1.480 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 7.72 cfs @ 12.32 hrs, Volume= 0.760 af  
 Outflow = 7.71 cfs @ 12.33 hrs, Volume= 0.760 af, Atten= 0%, Lag= 0.7 min

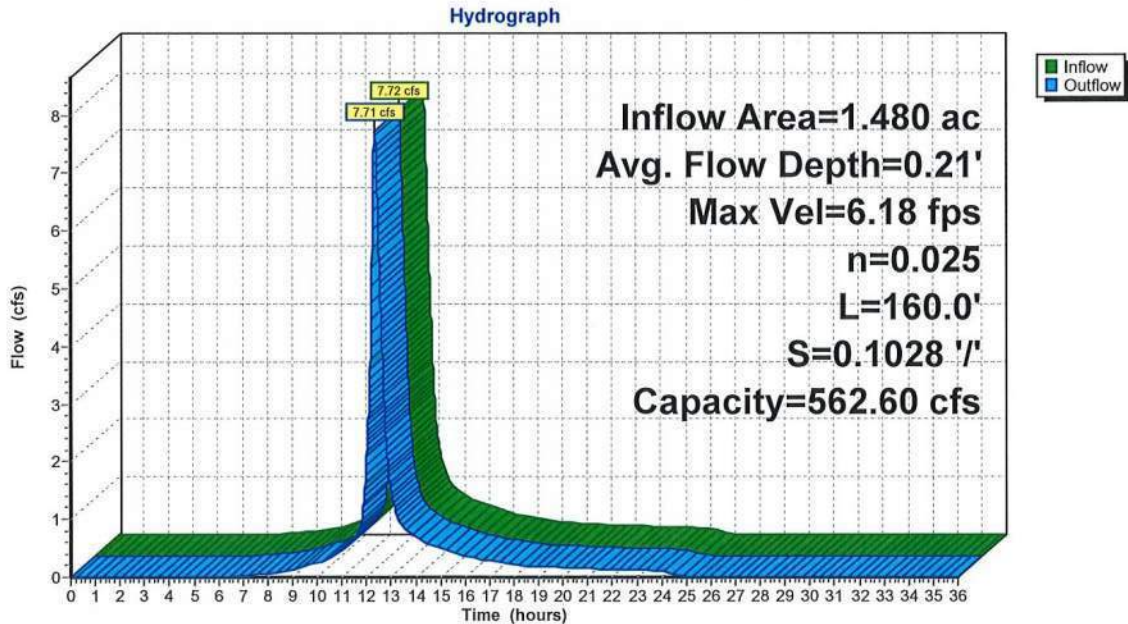
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.18 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 1.85 fps, Avg. Travel Time= 1.4 min

Peak Storage= 200 cf @ 12.32 hrs  
 Average Depth at Peak Storage= 0.21'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 562.60 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/ Top Width= 21.00'  
 Length= 160.0' Slope= 0.1028 '/  
 Inlet Invert= 53.20', Outlet Invert= 36.75'



**Reach CC: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach E: Chute-Concrete Block Open Cell**

Inflow Area = 17.798 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 106.93 cfs @ 12.15 hrs, Volume= 9.140 af  
 Outflow = 106.72 cfs @ 12.16 hrs, Volume= 9.140 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.11 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.96 fps, Avg. Travel Time= 1.3 min

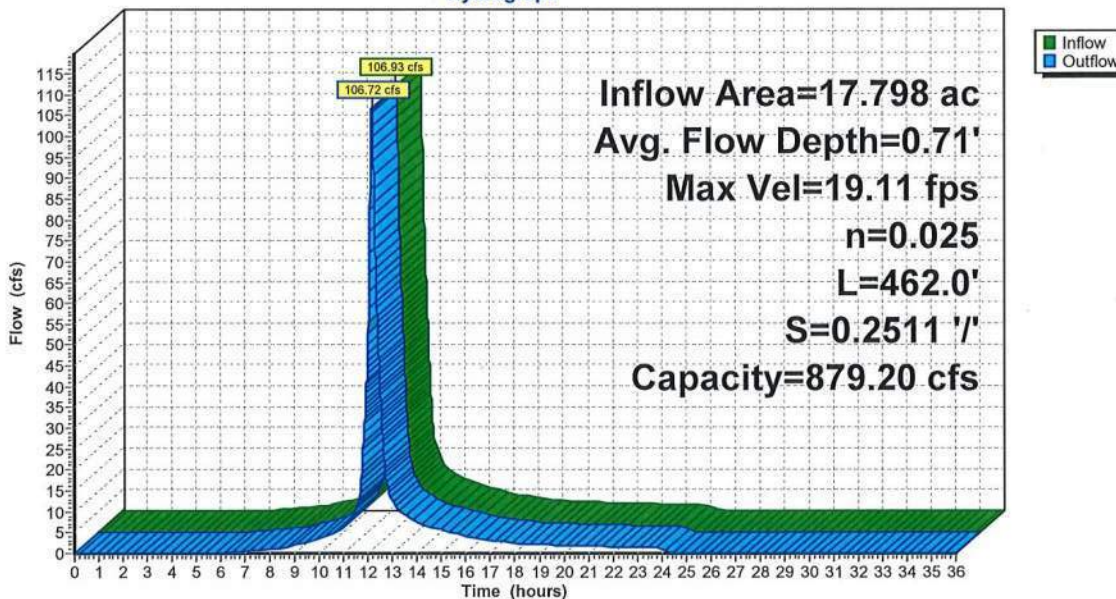
Peak Storage= 2,582 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.71'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 879.20 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 462.0' Slope= 0.2511 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach E: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach NE: Chute-Concrete Block Open Cell**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 91.93 cfs @ 12.15 hrs, Volume= 7.851 af  
 Outflow = 91.74 cfs @ 12.16 hrs, Volume= 7.851 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.27 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.65 fps, Avg. Travel Time= 1.4 min

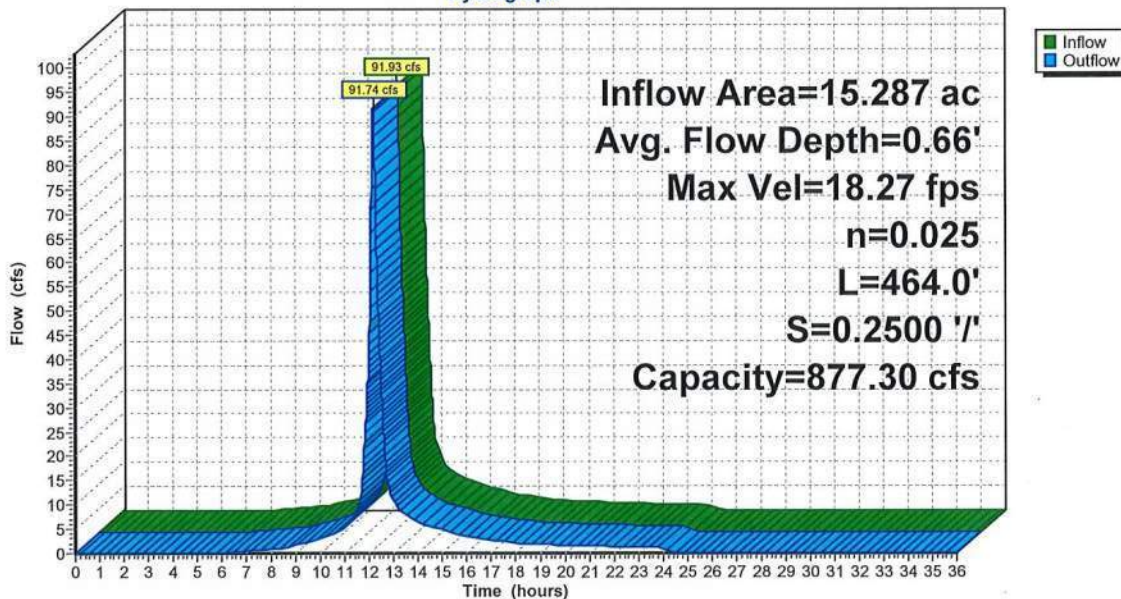
Peak Storage= 2,332 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.66'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/ Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach NE: Chute-Concrete Block Open Cell**

Hydrograph





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach NW: Chute-Concrete Block Open Cell**

Inflow Area = 13.115 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 77.52 cfs @ 12.15 hrs, Volume= 6.735 af  
 Outflow = 77.39 cfs @ 12.16 hrs, Volume= 6.735 af, Atten= 0%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 17.38 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.36 fps, Avg. Travel Time= 1.4 min

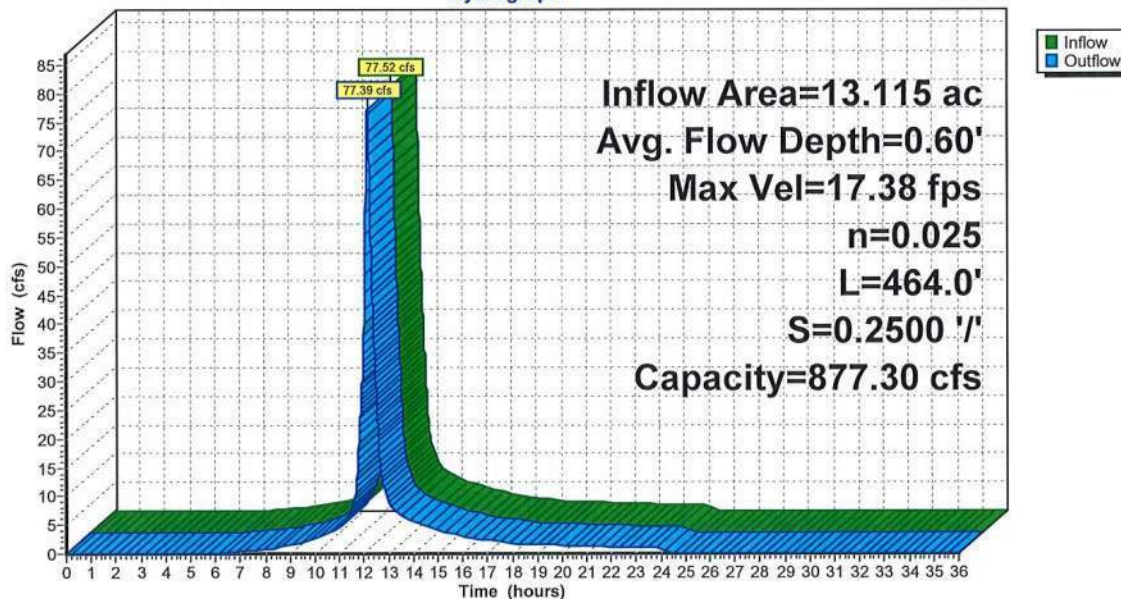
Peak Storage= 2,067 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.60'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach NW: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach OC: Existing Offsite Channel**

Inflow Area = 42.338 ac, 0.00% Impervious, Inflow Depth > 6.18" for 25-Year event  
 Inflow = 33.70 cfs @ 12.91 hrs, Volume= 21.821 af  
 Outflow = 32.78 cfs @ 14.06 hrs, Volume= 21.722 af, Atten= 3%, Lag= 68.9 min

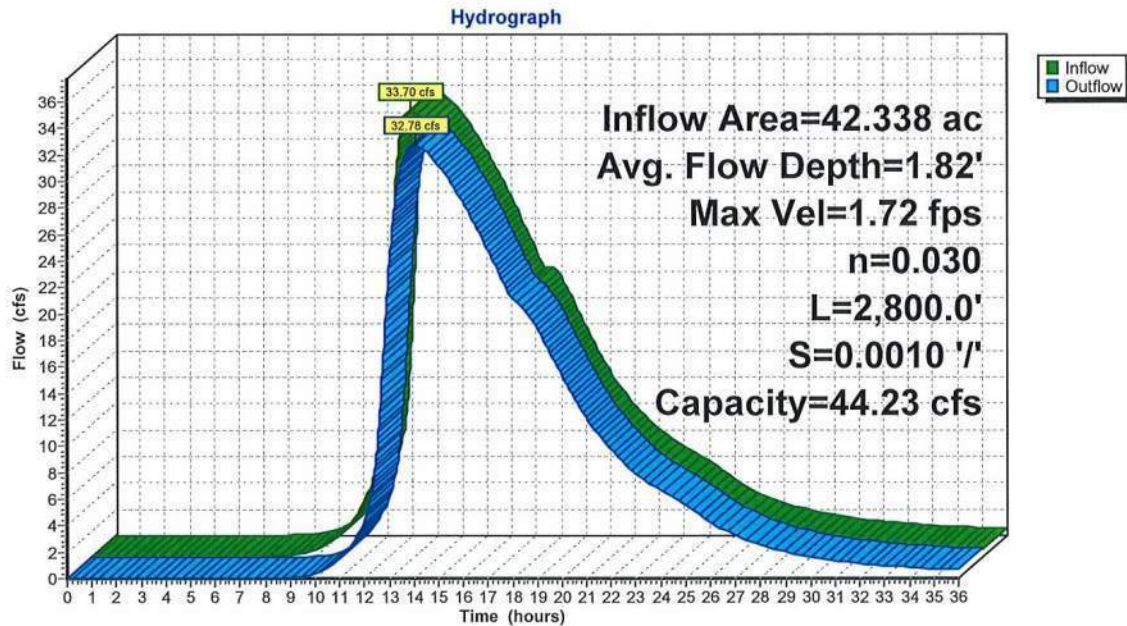
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.72 fps, Min. Travel Time= 27.1 min  
 Avg. Velocity = 0.84 fps, Avg. Travel Time= 55.4 min

Peak Storage= 53,292 cf @ 13.60 hrs  
 Average Depth at Peak Storage= 1.82'  
 Bank-Full Depth= 2.10' Flow Area= 23.7 sf, Capacity= 44.23 cfs

5.00' x 2.10' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 3.0 '/' Top Width= 17.60'  
 Length= 2,800.0' Slope= 0.0010 '/'  
 Inlet Invert= 46.66', Outlet Invert= 43.86'



**Reach OC: Existing Offsite Channel**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach P1: Culvert**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 82.99 cfs @ 12.29 hrs, Volume= 7.851 af  
 Outflow = 82.96 cfs @ 12.29 hrs, Volume= 7.851 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 13.43 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 4.02 fps, Avg. Travel Time= 0.3 min

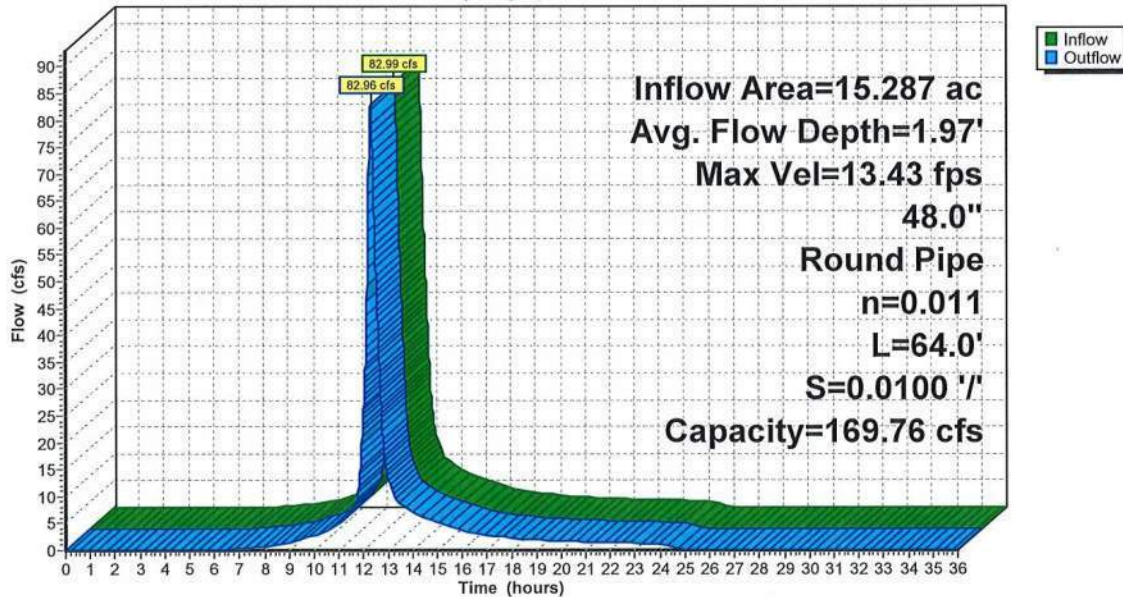
Peak Storage= 395 cf @ 12.29 hrs  
 Average Depth at Peak Storage= 1.97'  
 Bank-Full Depth= 4.00' Flow Area= 12.6 sf, Capacity= 169.76 cfs

48.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 64.0' Slope= 0.0100 '/'  
 Inlet Invert= 51.75', Outlet Invert= 51.11'



**Reach P1: Culvert**

**Hydrograph**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach P2: Culvert**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 2.88 cfs @ 12.25 hrs, Volume= 0.257 af  
 Outflow = 2.88 cfs @ 12.25 hrs, Volume= 0.257 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.62 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 2.18 fps, Avg. Travel Time= 0.6 min

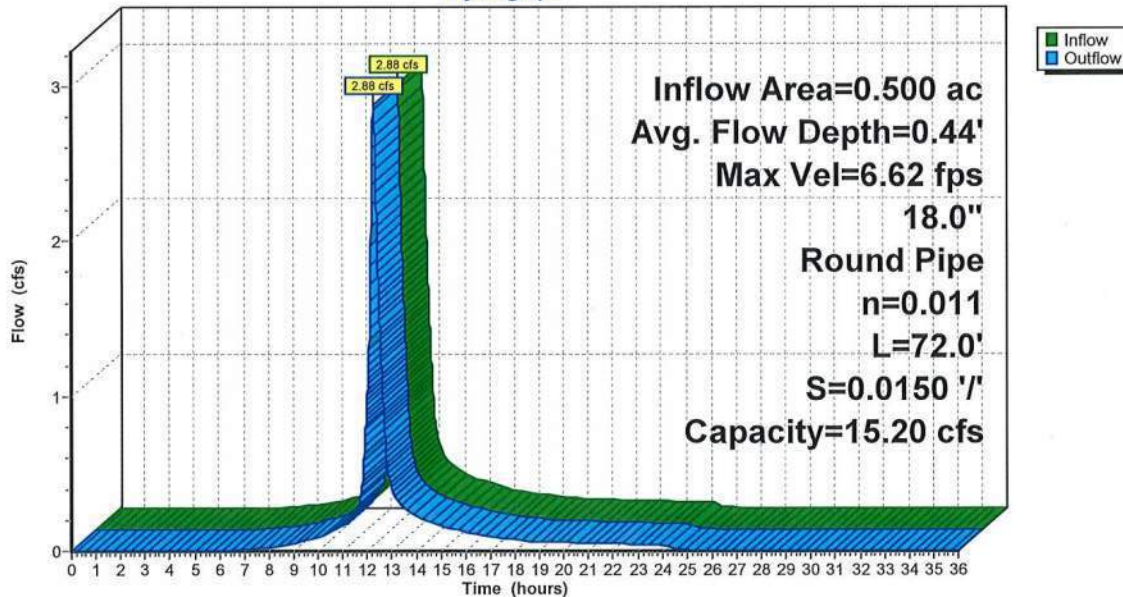
Peak Storage= 31 cf @ 12.25 hrs  
 Average Depth at Peak Storage= 0.44'  
 Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.20 cfs

18.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 72.0' Slope= 0.0150 '/'  
 Inlet Invert= 54.39', Outlet Invert= 53.31'



**Reach P2: Culvert**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach P2-1: Chute-Concrete Block Open Cell**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 2.88 cfs @ 12.25 hrs, Volume= 0.257 af  
 Outflow = 2.88 cfs @ 12.25 hrs, Volume= 0.257 af, Atten= 0%, Lag= 0.2 min

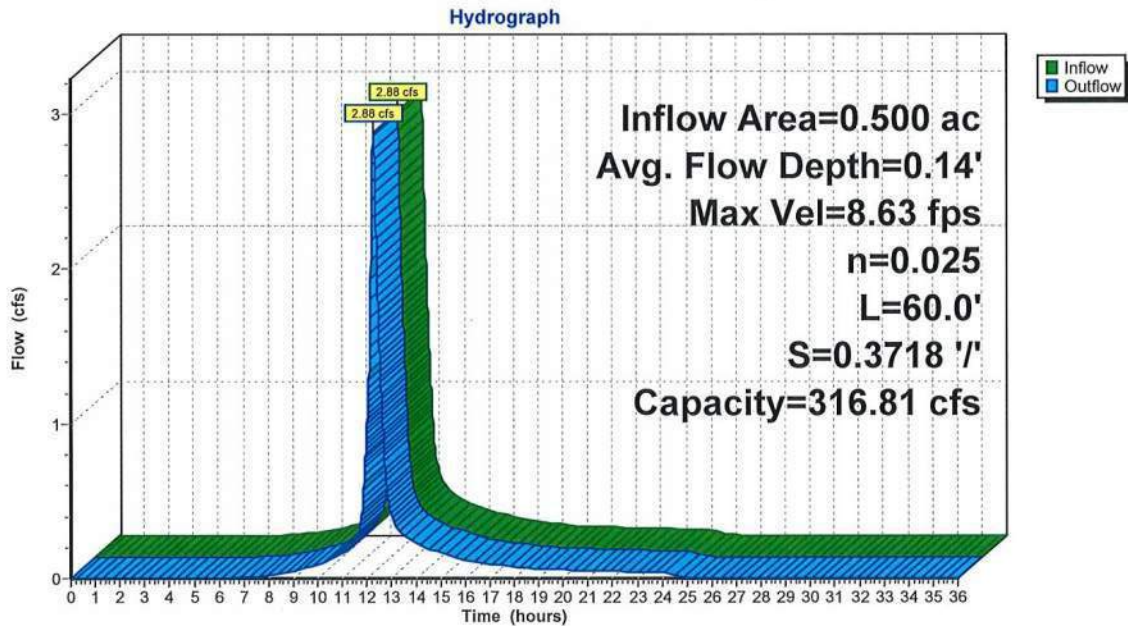
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 8.63 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.71 fps, Avg. Travel Time= 0.4 min

Peak Storage= 20 cf @ 12.25 hrs  
 Average Depth at Peak Storage= 0.14'  
 Bank-Full Depth= 1.50' Flow Area= 9.8 sf, Capacity= 316.81 cfs

2.00' x 1.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 3.0 '/' Top Width= 11.00'  
 Length= 60.0' Slope= 0.3718 '/'  
 Inlet Invert= 53.31', Outlet Invert= 31.00'



**Reach P2-1: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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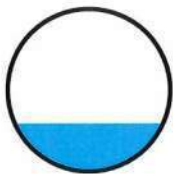
**Summary for Reach P3: Culvert**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 2.89 cfs @ 12.24 hrs, Volume= 0.257 af  
 Outflow = 2.89 cfs @ 12.25 hrs, Volume= 0.257 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.62 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity= 2.18 fps, Avg. Travel Time= 0.6 min

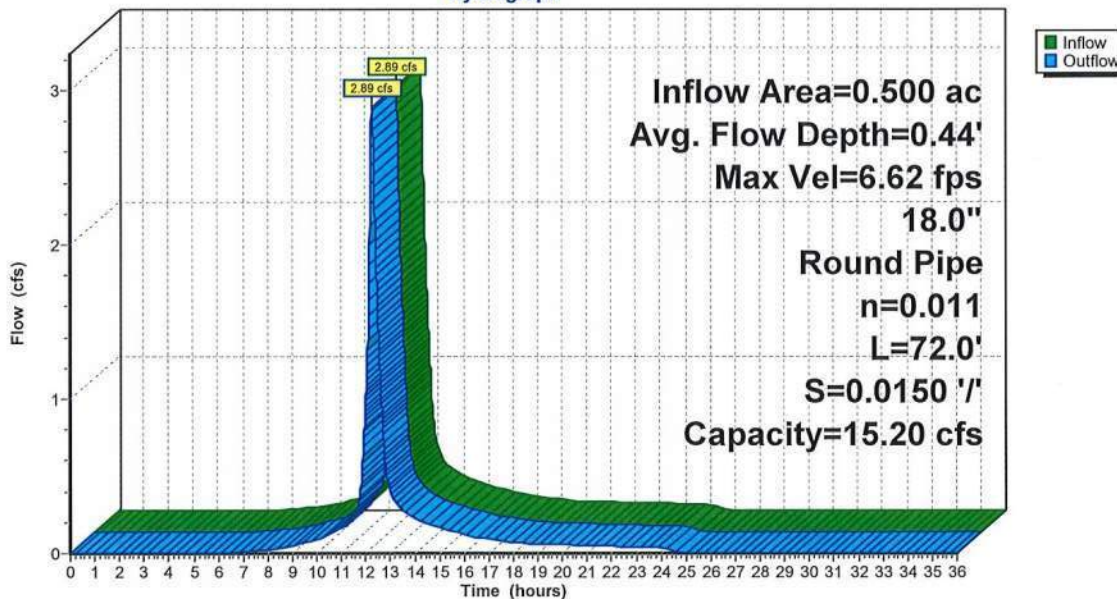
Peak Storage= 31 cf @ 12.25 hrs  
 Average Depth at Peak Storage= 0.44'  
 Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.20 cfs

18.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 72.0' Slope= 0.0150 '/'  
 Inlet Invert= 55.41', Outlet Invert= 54.33'



**Reach P3: Culvert**

**Hydrograph**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach P3-1: Chute-Concrete Block Open Cell**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 2.89 cfs @ 12.25 hrs, Volume= 0.257 af  
 Outflow = 2.89 cfs @ 12.25 hrs, Volume= 0.257 af, Atten= 0%, Lag= 0.2 min

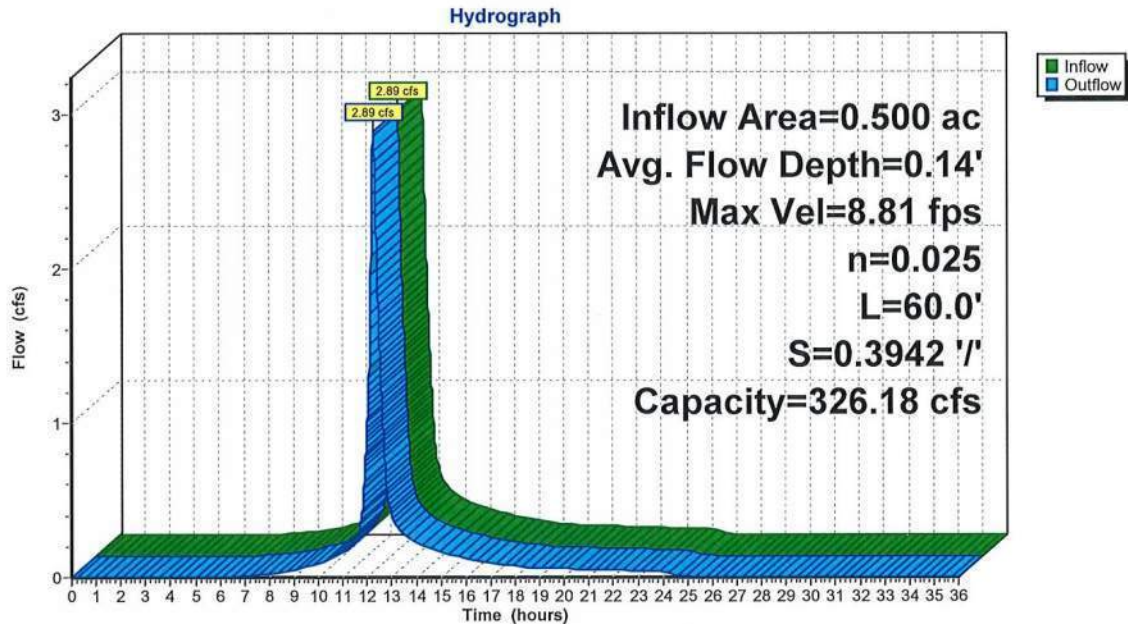
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 8.81 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.78 fps, Avg. Travel Time= 0.4 min

Peak Storage= 20 cf @ 12.25 hrs  
 Average Depth at Peak Storage= 0.14'  
 Bank-Full Depth= 1.50' Flow Area= 9.8 sf, Capacity= 326.18 cfs

2.00' x 1.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 3.0 '/' Top Width= 11.00'  
 Length= 60.0' Slope= 0.3942 '/'  
 Inlet Invert= 54.65', Outlet Invert= 31.00'



**Reach P3-1: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach S: Chute-Concrete Block Open Cell**

Inflow Area = 17.361 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 107.94 cfs @ 12.14 hrs, Volume= 8.916 af  
 Outflow = 107.70 cfs @ 12.15 hrs, Volume= 8.916 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.13 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.91 fps, Avg. Travel Time= 1.3 min

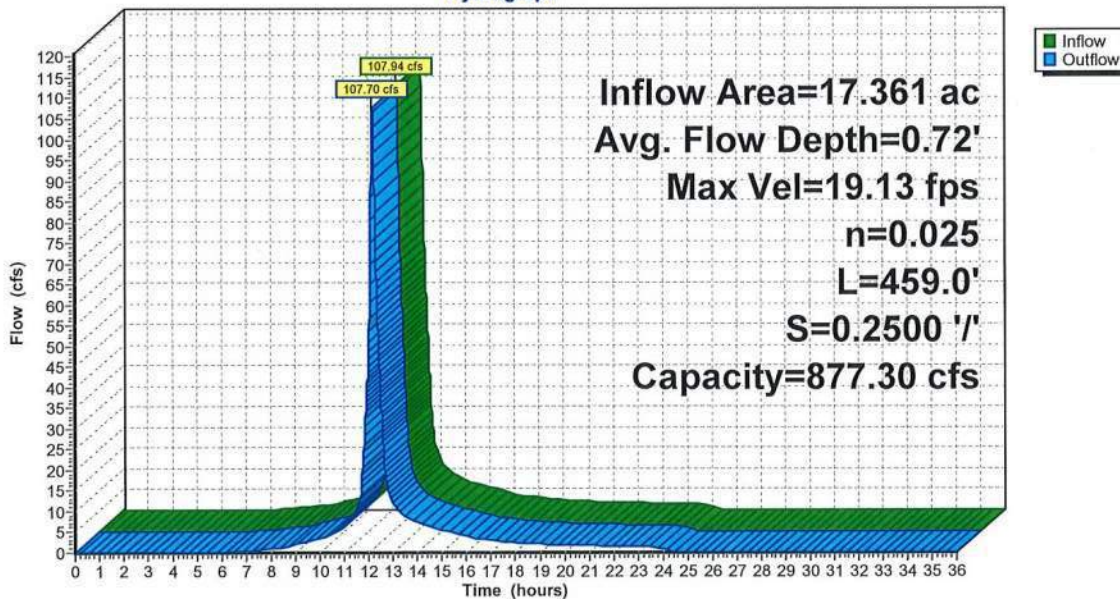
Peak Storage= 2,586 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.72'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 459.0' Slope= 0.2500 ' / '  
 Inlet Invert= 174.00', Outlet Invert= 59.25'



**Reach S: Chute-Concrete Block Open Cell**

Hydrograph





**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SE: Chute-Concrete Block Open Cell**

Inflow Area = 18.249 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 100.71 cfs @ 12.16 hrs, Volume= 9.372 af  
 Outflow = 100.58 cfs @ 12.17 hrs, Volume= 9.372 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.76 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.97 fps, Avg. Travel Time= 1.3 min

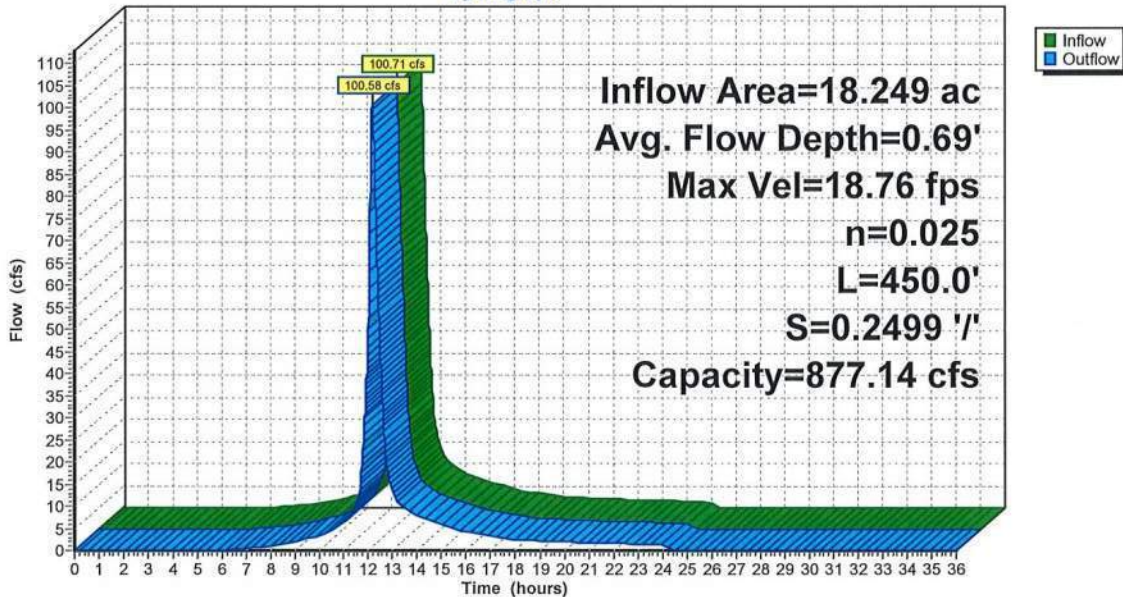
Peak Storage= 2,415 cf @ 12.16 hrs  
 Average Depth at Peak Storage= 0.69'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.14 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/ Top Width= 21.00'  
 Length= 450.0' Slope= 0.2499 '/  
 Inlet Invert= 174.00', Outlet Invert= 61.54'



**Reach SE: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SE1: Chute-Concrete Block Open Cell**

Inflow Area = 18.249 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 100.58 cfs @ 12.17 hrs, Volume= 9.372 af  
 Outflow = 100.54 cfs @ 12.17 hrs, Volume= 9.372 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 12.50 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity= 4.11 fps, Avg. Travel Time= 0.3 min

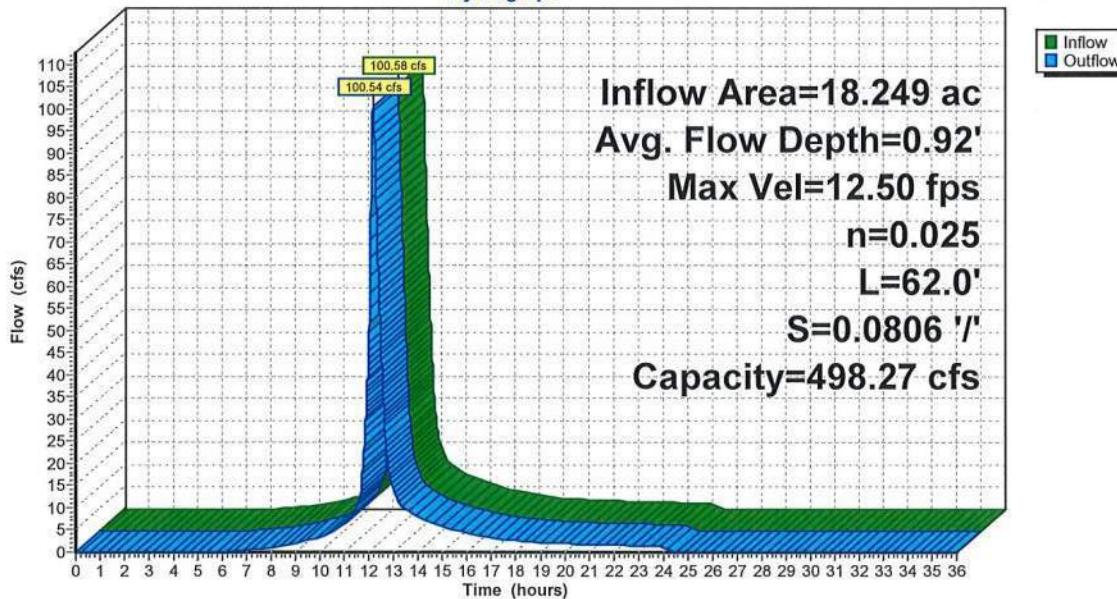
Peak Storage= 499 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 0.92'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 498.27 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 62.0' Slope= 0.0806 ' / '  
 Inlet Invert= 61.54', Outlet Invert= 56.54'



**Reach SE1: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SW: Chute-Concrete Block Open Cell**

Inflow Area = 15.434 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 95.96 cfs @ 12.14 hrs, Volume= 7.926 af  
 Outflow = 95.76 cfs @ 12.15 hrs, Volume= 7.926 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.50 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.68 fps, Avg. Travel Time= 1.2 min

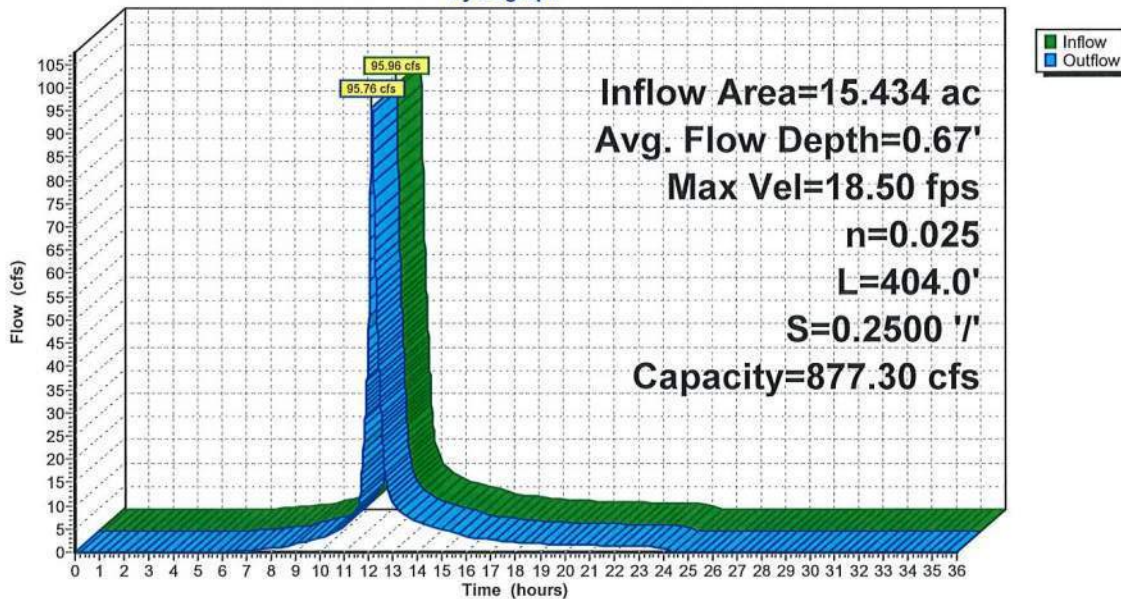
Peak Storage= 2,094 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.67'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 404.0' Slope= 0.2500 ' / '  
 Inlet Invert= 174.00', Outlet Invert= 73.00'



**Reach SW: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SW-1: Chute-Concrete Block Open Cell**

Inflow Area = 15.434 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 95.76 cfs @ 12.15 hrs, Volume= 7.926 af  
 Outflow = 95.59 cfs @ 12.16 hrs, Volume= 7.926 af, Atten= 0%, Lag= 0.5 min

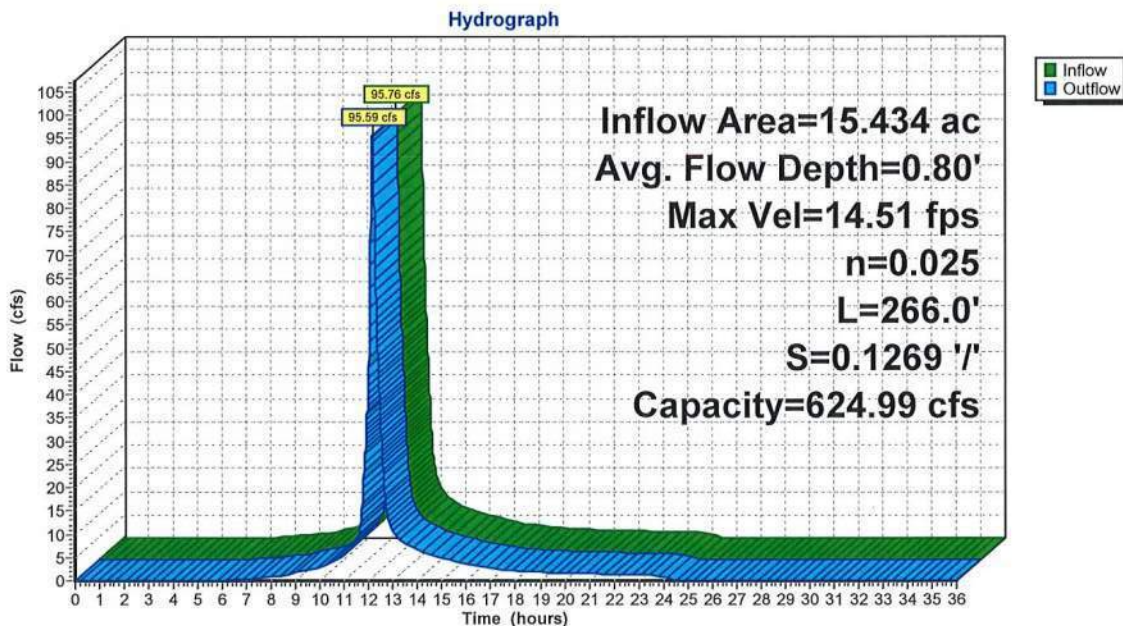
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 14.51 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity = 4.54 fps, Avg. Travel Time= 1.0 min

Peak Storage= 1,754 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.80'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 624.99 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 266.0' Slope= 0.1269 '/'  
 Inlet Invert= 70.50', Outlet Invert= 36.75'



**Reach SW-1: Chute-Concrete Block Open Cell**



**Post Development 25 Yr Drainage**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach W: Chute-Concrete Block Open Cell**

Inflow Area = 22.383 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 127.46 cfs @ 12.15 hrs, Volume= 11.495 af  
 Outflow = 127.27 cfs @ 12.16 hrs, Volume= 11.495 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 20.06 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 6.41 fps, Avg. Travel Time= 1.2 min

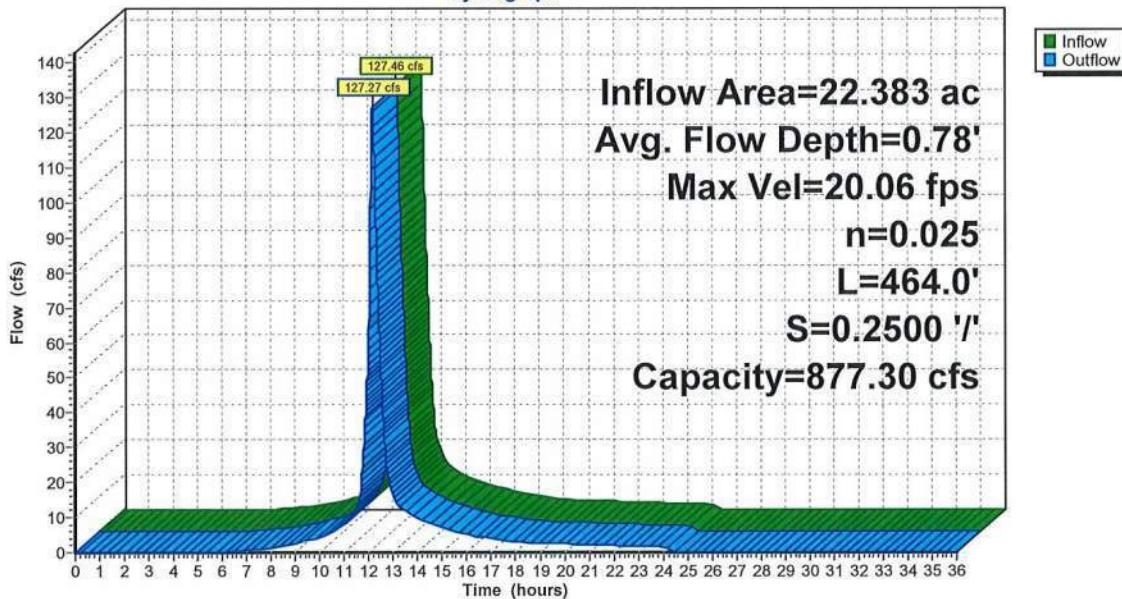
Peak Storage= 2,946 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.78'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach W: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 25 Yr Drainage**

*Type III 24-hr 25-Year Rainfall=8.70"*

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**Summary for Pond PA: Retention Pond A**

No Discharge. Reshaping of Existing Pond A Bottom Required.

Inflow Area = 47.697 ac, 0.00% Impervious, Inflow Depth = 6.59" for 25-Year event  
 Inflow = 225.75 cfs @ 12.22 hrs, Volume= 26.201 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 47.33' @ 36.00 hrs Surf.Area= 4.028 ac Storage= 26.200 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert	Avail.Storage	Storage Description		
	36.75'	82.379 af	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (acres)	Perim. (feet)	Inc.Store (acre-feet)	Cum.Store (acre-feet)	Wet.Area (acres)
36.75	1.340	1,049.8	0.000	0.000	1.340
37.00	1.380	1,064.9	0.340	0.340	1.399
38.00	1.540	1,125.4	1.459	1.799	1.642
39.00	1.720	1,171.5	1.629	3.428	1.837
40.00	1.890	1,216.8	1.804	5.233	2.037
41.00	2.120	1,292.5	2.004	7.237	2.385
42.00	2.360	1,370.6	2.239	9.476	2.766
43.00	2.620	1,447.9	2.489	11.964	3.166
44.00	2.900	1,537.3	2.759	14.723	3.654
45.00	3.210	1,623.3	3.054	17.777	4.152
46.00	3.550	1,699.4	3.379	21.156	4.616
47.00	3.910	1,769.6	3.729	24.884	5.062
48.00	4.270	1,832.8	4.089	28.973	5.480
49.00	4.640	1,894.6	4.454	33.426	5.903
50.00	5.020	1,956.1	4.829	38.255	6.338
51.00	5.450	2,024.3	5.234	43.489	6.836
52.00	5.860	2,075.6	5.654	49.143	7.223
53.00	6.180	2,125.3	6.019	55.162	7.608
54.00	6.490	2,167.2	6.334	61.496	7.940
55.00	6.800	2,209.1	6.644	68.141	8.279
56.00	7.120	2,250.9	6.959	75.100	8.623
57.00	7.440	2,292.6	7.279	82.379	8.973

**Post Development 25 Yr Drainage**

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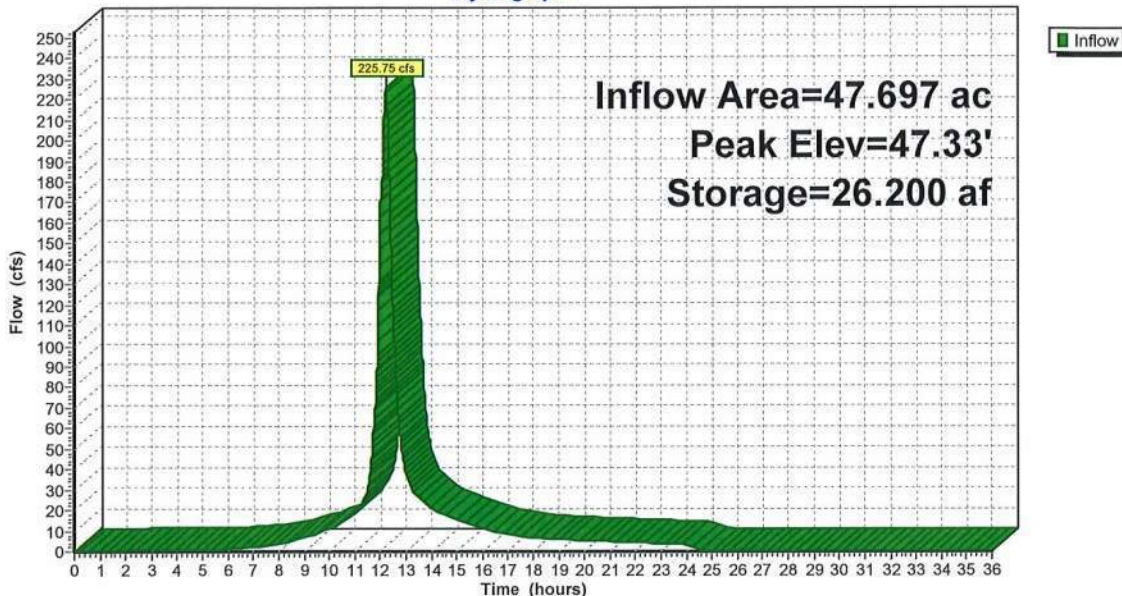
Type III 24-hr 25-Year Rainfall=8.70"

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**Pond PA: Retention Pond A**

Hydrograph



**Post Development 25 Yr Drainage**

*Type III 24-hr 25-Year Rainfall=8.70"*

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**Summary for Pond PB: Detention Pond B**

Inflow Area = 42.338 ac, 0.00% Impervious, Inflow Depth = 6.40" for 25-Year event  
 Inflow = 235.89 cfs @ 12.16 hrs, Volume= 22.565 af  
 Outflow = 33.70 cfs @ 12.91 hrs, Volume= 21.821 af, Atten= 86%, Lag= 45.0 min  
 Primary = 33.70 cfs @ 12.91 hrs, Volume= 21.821 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 50.87' @ 12.91 hrs Surf.Area= 3.532 ac Storage= 11.562 af

Plug-Flow detention time= 244.2 min calculated for 21.821 af (97% of inflow)  
 Center-of-Mass det. time= 224.8 min ( 1,023.3 - 798.5 )

Volume	Invert	Avail. Storage	Storage Description		
#1	47.00'	19.739 af	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf. Area (acres)	Perim. (feet)	Inc. Store (acre-feet)	Cum. Store (acre-feet)	Wet. Area (acres)
47.00	2.450	3,998.7	0.000	0.000	2.450
48.00	2.730	4,022.7	2.589	2.589	2.814
49.00	3.010	4,046.7	2.869	5.458	3.179
50.00	3.290	4,070.7	3.149	8.607	3.547
51.00	3.570	4,094.6	3.429	12.036	3.916
52.00	3.850	4,118.8	3.709	15.745	4.291
53.00	4.140	4,158.1	3.994	19.739	4.893

Device	Routing	Invert	Outlet Devices
#1	Primary	47.00'	<b>21.0" Round RCP_Round 21"</b> L= 128.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 47.00' / 46.75' S= 0.0020 1/ S= 0.0020 1/ Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 2.41 sf
#2	Primary	47.00'	<b>21.0" Round RCP_Round 21"</b> L= 128.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 47.00' / 46.75' S= 0.0020 1/ Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 2.41 sf

**Primary OutFlow** Max=33.70 cfs @ 12.91 hrs HW=50.87' (Free Discharge)

- 1=RCP\_Round 21" (Barrel Controls 16.85 cfs @ 7.00 fps)
- 2=RCP\_Round 21" (Barrel Controls 16.85 cfs @ 7.00 fps)



**Post Development 25 Yr Drainage**

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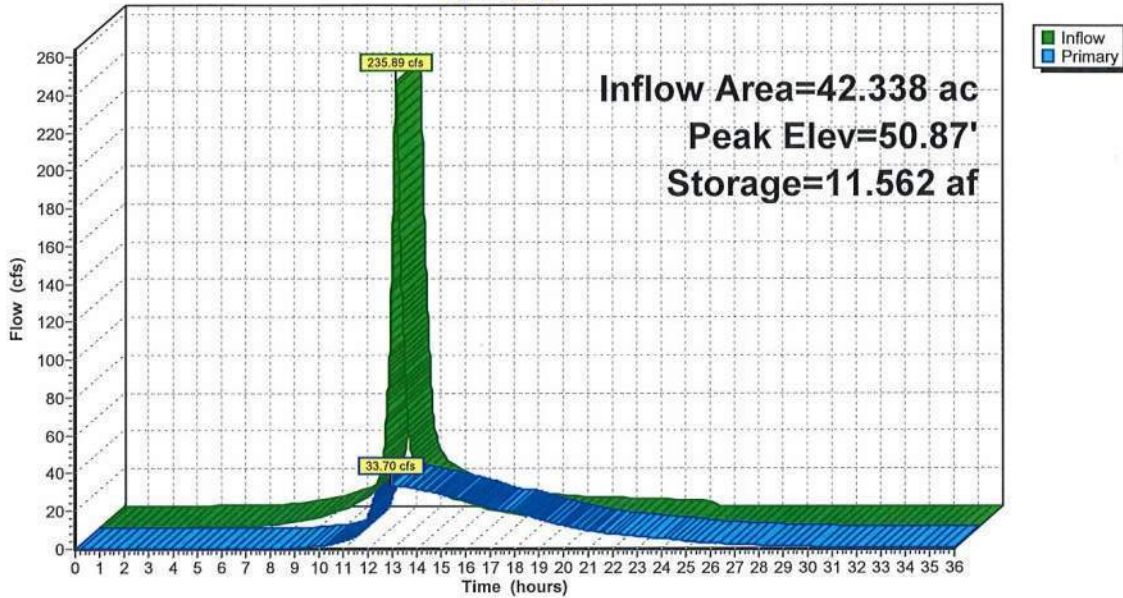
Type III 24-hr 25-Year Rainfall=8.70"

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**Pond PB: Detention Pond B**

Hydrograph



**Post Development 25 Yr Drainage**

*Type III 24-hr 25-Year Rainfall=8.70"*

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**Summary for Pond PC: Retention Pond C**

No Discharge. Constrction of Perimeter Berm to Elevation 48 ft. Required.

Inflow Area = 61.584 ac, 0.00% Impervious, Inflow Depth = 6.37" for 25-Year event  
 Inflow = 313.19 cfs @ 12.23 hrs, Volume= 32.676 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 42.36' @ 36.00 hrs Surf.Area= 3.718 ac Storage= 32.676 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume #1	Invert	Avail.Storage	Storage Description		
	31.00'	56.115 af	<b>Custom Stage Data (Irregular) Listed below (Recalc)</b>		
Elevation (feet)	Surf.Area (acres)	Perim. (feet)	Inc.Store (acre-feet)	Cum.Store (acre-feet)	Wet.Area (acres)
31.00	2.060	2,014.1	0.000	0.000	2.060
32.00	2.200	2,032.9	2.130	2.130	2.207
33.00	2.340	2,051.7	2.270	4.399	2.354
34.00	2.480	2,070.5	2.410	6.809	2.504
35.00	2.630	2,089.2	2.555	9.364	2.654
36.00	2.770	2,108.0	2.700	12.063	2.806
37.00	2.920	2,126.8	2.845	14.908	2.959
38.00	3.060	2,145.6	2.990	17.898	3.114
39.00	3.210	2,164.4	3.135	21.032	3.270
40.00	3.360	2,183.2	3.285	24.317	3.427
41.00	3.510	2,201.9	3.435	27.752	3.585
42.00	3.660	2,220.7	3.585	31.337	3.745
43.00	3.820	2,239.5	3.740	35.076	3.907
44.00	3.970	2,258.3	3.895	38.971	4.070
45.00	4.130	2,277.1	4.050	43.021	4.234
46.00	4.290	2,295.9	4.210	47.230	4.400
47.00	4.440	2,314.6	4.365	51.595	4.566
48.00	4.600	2,333.4	4.520	56.115	4.734

**Post Development 25 Yr Drainage**

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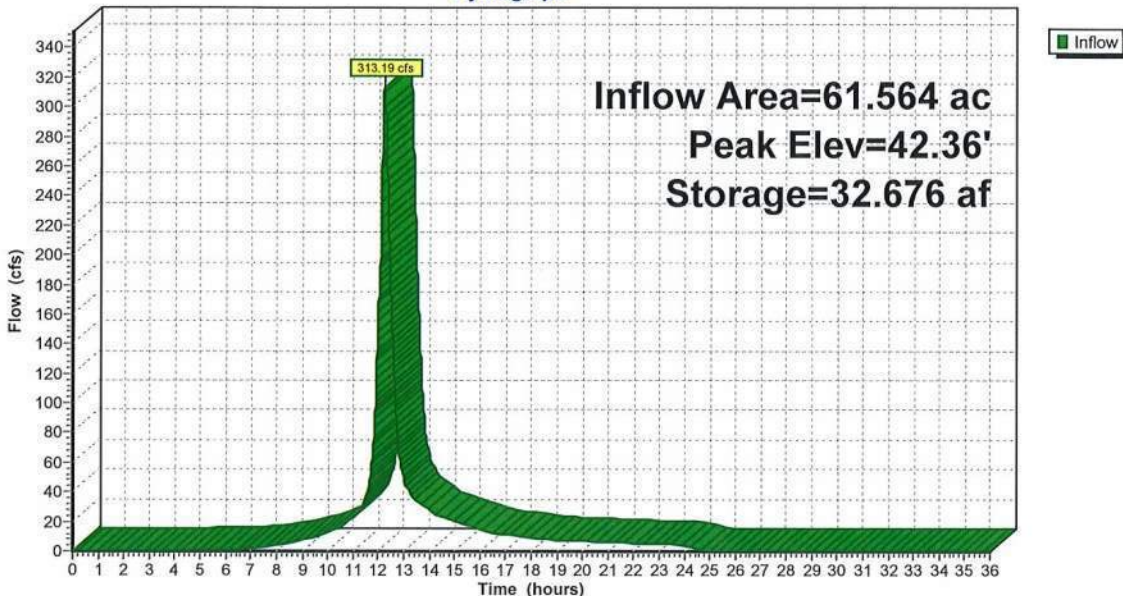
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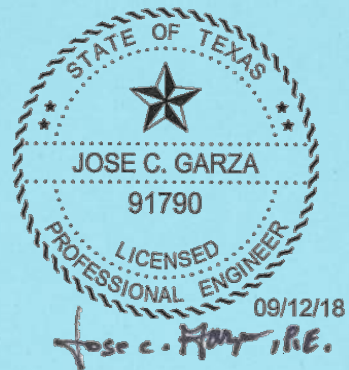
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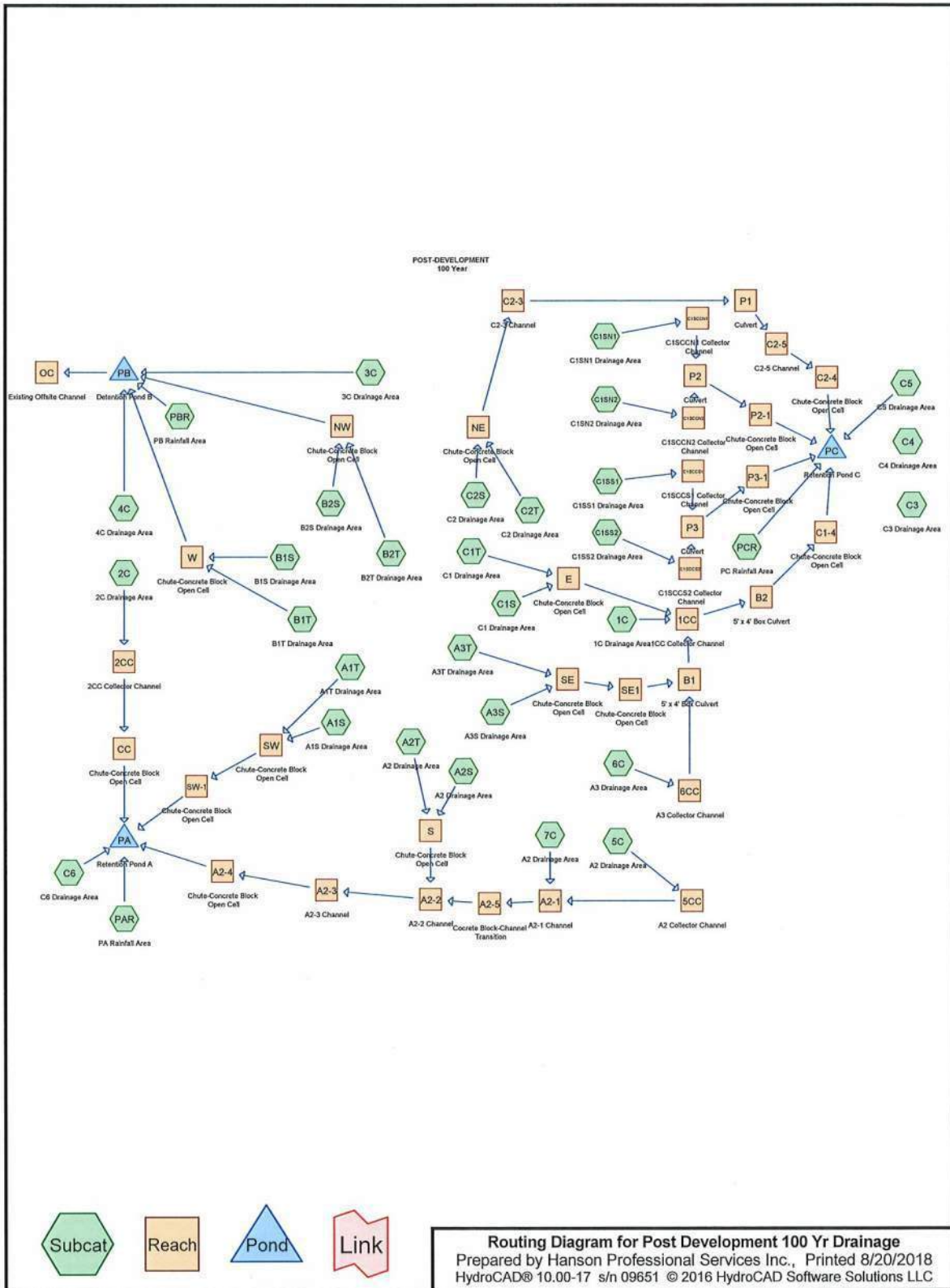
**Pond PC: Retention Pond C**

Hydrograph



APPENDIX 6B.5  
HYDROCAD MODEL POST DEVELOPMENT-100 YEAR





**Post Development 100 Yr Drainage**

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
128.657	79	50-75% Grass cover, Fair, HSG C (1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T)
19.672	66	<50% Grass cover, Poor, HSG C (C3, C4, C5, C6)
16.270	98	Water Surface, 0% imp, HSG C (PAR, PBR, PCR)
<b>164.599</b>	<b>82</b>	<b>TOTAL AREA</b>

**Post Development 100 Yr Drainage**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
164.599	HSG C	1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T, C3, C4, C5, C6, PAR, PBR, PCR
0.000	HSG D	
0.000	Other	
<b>164.599</b>		<b>TOTAL AREA</b>

**Post Development 100 Yr Drainage**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	128.657	0.000	0.000	128.657	50-75% Grass cover, Fair	1C, 2C, 3C, 4C, 5C, 6C, 7C, A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1SN1, C1SN2, C1SS1, C1SS2, C1T, C2S, C2T
0.000	0.000	19.672	0.000	0.000	19.672	<50% Grass cover, Poor	C3, C4, C5, C6
0.000	0.000	16.270	0.000	0.000	16.270	Water Surface, 0% imp	PAR, PBR, PCR
<b>0.000</b>	<b>0.000</b>	<b>164.599</b>	<b>0.000</b>	<b>0.000</b>	<b>164.599</b>	<b>TOTAL AREA</b>	



**Post Development 100 Yr Drainage**

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**Pipe Listing (all nodes)**

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	B1	56.54	53.89	464.0	0.0057	0.013	60.0	48.0	0.0
2	B2	53.45	49.80	200.0	0.0182	0.013	60.0	48.0	0.0
3	P1	51.75	51.11	64.0	0.0100	0.011	48.0	0.0	0.0
4	P2	54.39	53.31	72.0	0.0150	0.011	18.0	0.0	0.0
5	P3	55.41	54.33	72.0	0.0150	0.011	18.0	0.0	0.0
6	PB	47.00	46.75	128.0	0.0020	0.013	21.0	0.0	0.0
7	PB	47.00	46.75	128.0	0.0020	0.013	21.0	0.0	0.0

**Post Development 100 Yr Drainage**

*Type III 24-hr 100-Year Rainfall=11.50"*

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Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment 1C: 1C Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=8.77 cfs 0.736 af
<b>Subcatchment 2C: 2C Drainage Area</b>	Runoff Area=1.480 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=12.98 cfs 1.089 af
<b>Subcatchment 3C: 3C Drainage Area</b>	Runoff Area=1.640 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=14.38 cfs 1.207 af
<b>Subcatchment 4C: 4C Drainage Area</b>	Runoff Area=0.910 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=7.98 cfs 0.670 af
<b>Subcatchment 5C: A2 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=8.77 cfs 0.736 af
<b>Subcatchment 6C: A3 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=8.77 cfs 0.736 af
<b>Subcatchment 7C: A2 Drainage Area</b>	Runoff Area=1.000 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=8.77 cfs 0.736 af
<b>Subcatchment A1S: A1S Drainage Area</b>	Runoff Area=8.009 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=70.23 cfs 5.892 af
<b>Subcatchment A1T: A1T Drainage Area</b>	Runoff Area=7.425 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=65.11 cfs 5.463 af
<b>Subcatchment A2S: A2 Drainage Area</b>	Runoff Area=12.241 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=107.35 cfs 9.006 af
<b>Subcatchment A2T: A2 Drainage Area</b>	Runoff Area=5.120 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=44.90 cfs 3.767 af
<b>Subcatchment A3S: A3S Drainage Area</b>	Runoff Area=10.760 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=94.36 cfs 7.916 af
<b>Subcatchment A3T: A3T Drainage Area</b>	Runoff Area=7.489 ac 0.00% Impervious Runoff Depth=8.83" Flow Length=1,050' Tc=16.7 min CN=79 Runoff=54.75 cfs 5.510 af
<b>Subcatchment B1S: B1S Drainage Area</b>	Runoff Area=14.884 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=130.52 cfs 10.951 af
<b>Subcatchment B1T: B1T Drainage Area</b>	Runoff Area=7.499 ac 0.00% Impervious Runoff Depth=8.83" Flow Length=950' Tc=16.0 min CN=79 Runoff=55.80 cfs 5.517 af
<b>Subcatchment B2S: B2S Drainage Area</b>	Runoff Area=8.806 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=77.22 cfs 6.479 af

**Post Development 100 Yr Drainage**

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<b>Subcatchment B2T: B2T Drainage Area</b>	Runoff Area=4.309 ac 0.00% Impervious Runoff Depth=8.83" Flow Length=850' Tc=13.7 min CN=79 Runoff=33.95 cfs 3.170 af
<b>Subcatchment C1S: C1 Drainage Area</b>	Runoff Area=11.506 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=100.90 cfs 8.465 af
<b>Subcatchment C1SN1: C1SN1 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=2.19 cfs 0.184 af
<b>Subcatchment C1SN2: C1SN2 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=2.19 cfs 0.184 af
<b>Subcatchment C1SS1: C1SS1 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=2.19 cfs 0.184 af
<b>Subcatchment C1SS2: C1SS2 Drainage Area</b>	Runoff Area=0.250 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=2.19 cfs 0.184 af
<b>Subcatchment C1T: C1 Drainage Area</b>	Runoff Area=6.292 ac 0.00% Impervious Runoff Depth=8.83" Flow Length=800' Tc=12.5 min CN=79 Runoff=51.20 cfs 4.629 af
<b>Subcatchment C2S: C2 Drainage Area</b>	Runoff Area=10.038 ac 0.00% Impervious Runoff Depth=8.83" Tc=10.0 min CN=79 Runoff=88.03 cfs 7.385 af
<b>Subcatchment C2T: C2 Drainage Area</b>	Runoff Area=5.249 ac 0.00% Impervious Runoff Depth=8.83" Flow Length=800' Tc=12.5 min CN=79 Runoff=42.72 cfs 3.862 af
<b>Subcatchment C3: C3 Drainage Area</b>	Runoff Area=3.500 ac 0.00% Impervious Runoff Depth=9.75" Tc=10.0 min CN=86 Runoff=32.84 cfs 2.845 af
<b>Subcatchment C4: C4 Drainage Area</b>	Runoff Area=9.500 ac 0.00% Impervious Runoff Depth=9.75" Tc=10.0 min CN=86 Runoff=89.15 cfs 7.722 af
<b>Subcatchment C5: C5 Drainage Area</b>	Runoff Area=2.690 ac 0.00% Impervious Runoff Depth=9.75" Tc=10.0 min CN=86 Runoff=25.24 cfs 2.186 af
<b>Subcatchment C6: C6 Drainage Area</b>	Runoff Area=3.982 ac 0.00% Impervious Runoff Depth=9.75" Tc=10.0 min CN=86 Runoff=37.37 cfs 3.237 af
<b>Subcatchment PAR: PA Rainfall Area</b>	Runoff Area=7.440 ac 0.00% Impervious Runoff Depth=11.26" Tc=0.0 min CN=98 Runoff=102.59 cfs 6.980 af
<b>Subcatchment PBR: PB Rainfall Area</b>	Runoff Area=4.290 ac 0.00% Impervious Runoff Depth=11.26" Tc=0.0 min CN=98 Runoff=59.15 cfs 4.025 af
<b>Subcatchment PCR: PC Rainfall Area</b>	Runoff Area=4.540 ac 0.00% Impervious Runoff Depth=11.26" Tc=0.0 min CN=98 Runoff=62.60 cfs 4.260 af
<b>Reach 1CC: 1CC Collector Channel</b>	Avg. Flow Depth=5.24' Max Vel=4.25 fps Inflow=301.75 cfs 27.992 af n=0.030 L=222.0' S=0.0020 '/' Capacity=2,157.50 cfs Outflow=300.25 cfs 27.992 af

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<b>Reach 2CC: 2CC Collector Channel</b>	Avg. Flow Depth=1.46'	Max Vel=1.74 fps	Inflow=12.98 cfs	1.089 af
	n=0.030 L=650.0' S=0.0020 '/	Capacity=46.53 cfs	Outflow=11.11 cfs	1.089 af
<b>Reach 5CC: A2 Collector Channel</b>	Avg. Flow Depth=1.15'	Max Vel=1.50 fps	Inflow=8.77 cfs	0.736 af
	n=0.030 L=595.0' S=0.0015 '/	Capacity=68.72 cfs	Outflow=7.45 cfs	0.736 af
<b>Reach 6CC: A3 Collector Channel</b>	Avg. Flow Depth=0.92'	Max Vel=2.17 fps	Inflow=8.77 cfs	0.736 af
	n=0.030 L=740.0' S=0.0040 '/	Capacity=50.02 cfs	Outflow=7.67 cfs	0.736 af
<b>Reach A2-1: A2-1 Channel</b>	Avg. Flow Depth=1.48'	Max Vel=1.73 fps	Inflow=12.75 cfs	1.471 af
	n=0.030 L=250.5' S=0.0015 '/	Capacity=83.47 cfs	Outflow=12.71 cfs	1.471 af
<b>Reach A2-2: A2-2 Channel</b>	Avg. Flow Depth=3.02'	Max Vel=4.09 fps	Inflow=162.11 cfs	14.244 af
	n=0.025 L=257.0' S=0.0020 '/	Capacity=338.68 cfs	Outflow=160.83 cfs	14.244 af
<b>Reach A2-3: A2-3 Channel</b>	Avg. Flow Depth=3.09'	Max Vel=3.52 fps	Inflow=160.83 cfs	14.244 af
	n=0.030 L=582.0' S=0.0020 '/	Capacity=532.10 cfs	Outflow=154.07 cfs	14.244 af
<b>Reach A2-4: Chute-Concrete Block</b>	Avg. Flow Depth=0.91'	Max Vel=12.45 fps	Inflow=154.07 cfs	14.244 af
	n=0.025 L=250.0' S=0.0697 '/	Capacity=692.98 cfs	Outflow=153.86 cfs	14.244 af
<b>Reach A2-5: Concrete Block-Channel</b>	Avg. Flow Depth=0.37'	Max Vel=12.58 fps	Inflow=12.71 cfs	1.471 af
	n=0.025 L=5.6' S=0.2482 '/	Capacity=903.50 cfs	Outflow=12.71 cfs	1.471 af
<b>Reach B1: 5' x 4' Box Culvert</b>	Avg. Flow Depth=2.81'	Max Vel=10.42 fps	Inflow=146.99 cfs	14.162 af
	60.0" x 48.0" Box Pipe n=0.013 L=464.0' S=0.0057 '/	Capacity=185.34 cfs	Outflow=146.52 cfs	14.162 af
<b>Reach B2: 5' x 4' Box Culvert</b>	Avg. Flow Depth=3.12'	Max Vel=19.22 fps	Inflow=300.25 cfs	27.992 af
	60.0" x 48.0" Box Pipe n=0.013 L=200.0' S=0.0182 '/	Capacity=331.32 cfs	Outflow=300.01 cfs	27.992 af
<b>Reach C1-4: Chute-Concrete Block</b>	Avg. Flow Depth=1.21'	Max Vel=25.32 fps	Inflow=300.01 cfs	27.992 af
	n=0.025 L=76.0' S=0.2474 '/	Capacity=872.67 cfs	Outflow=299.94 cfs	27.992 af
<b>Reach C1SCCN1: C1SCCN1 Collector</b>	Avg. Flow Depth=0.40'	Max Vel=1.34 fps	Inflow=2.19 cfs	0.184 af
	n=0.030 L=285.0' S=0.0033 '/	Capacity=24.47 cfs	Outflow=2.06 cfs	0.184 af
<b>Reach C1SCCN2: C1SCCN2 Collector</b>	Avg. Flow Depth=0.40'	Max Vel=1.33 fps	Inflow=2.19 cfs	0.184 af
	n=0.030 L=287.5' S=0.0033 '/	Capacity=24.36 cfs	Outflow=2.06 cfs	0.184 af
<b>Reach C1SCCS1: C1SCCS1 Collector</b>	Avg. Flow Depth=0.41'	Max Vel=1.33 fps	Inflow=2.19 cfs	0.184 af
	n=0.030 L=280.0' S=0.0033 '/	Capacity=24.30 cfs	Outflow=2.06 cfs	0.184 af
<b>Reach C1SCCS2: C1SCCS2 Collector</b>	Avg. Flow Depth=0.41'	Max Vel=1.33 fps	Inflow=2.19 cfs	0.184 af
	n=0.030 L=280.0' S=0.0033 '/	Capacity=24.30 cfs	Outflow=2.06 cfs	0.184 af
<b>Reach C2-3: C2-3 Channel</b>	Avg. Flow Depth=3.32'	Max Vel=3.35 fps	Inflow=129.45 cfs	11.247 af
	n=0.030 L=882.0' S=0.0020 '/	Capacity=178.76 cfs	Outflow=118.51 cfs	11.247 af
<b>Reach C2-4: Chute-Concrete Block</b>	Avg. Flow Depth=0.70'	Max Vel=21.63 fps	Inflow=118.38 cfs	11.247 af
	n=0.025 L=52.0' S=0.3289 '/	Capacity=1,003.23 cfs	Outflow=118.36 cfs	11.247 af

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<b>Reach C2-5: C2-5 Channel</b>	Avg. Flow Depth=1.29'	Max Vel=9.05 fps	Inflow=118.48 cfs	11.247 af
n=0.025 L=106.0'	S=0.0293 '/	Capacity=492.25 cfs	Outflow=118.38 cfs	11.247 af
<b>Reach CC: Chute-Concrete Block</b>	Avg. Flow Depth=0.26'	Max Vel=6.99 fps	Inflow=11.11 cfs	1.089 af
n=0.025 L=160.0'	S=0.1028 '/	Capacity=562.60 cfs	Outflow=11.10 cfs	1.089 af
<b>Reach E: Chute-Concrete Block</b>	Avg. Flow Depth=0.85'	Max Vel=21.08 fps	Inflow=150.87 cfs	13.094 af
n=0.025 L=462.0'	S=0.2511 '/	Capacity=879.20 cfs	Outflow=150.58 cfs	13.094 af
<b>Reach NE: Chute-Concrete Block</b>	Avg. Flow Depth=0.79'	Max Vel=20.16 fps	Inflow=129.70 cfs	11.247 af
n=0.025 L=464.0'	S=0.2500 '/	Capacity=877.30 cfs	Outflow=129.45 cfs	11.247 af
<b>Reach NW: Chute-Concrete Block</b>	Avg. Flow Depth=0.72'	Max Vel=19.21 fps	Inflow=109.40 cfs	9.649 af
n=0.025 L=464.0'	S=0.2500 '/	Capacity=877.30 cfs	Outflow=109.21 cfs	9.649 af
<b>Reach OC: Existing Offsite Channel</b>	Avg. Flow Depth=2.04'	Max Vel=1.83 fps	Inflow=42.26 cfs	31.217 af
n=0.030 L=2,800.0'	S=0.0010 '/	Capacity=44.23 cfs	Outflow=41.59 cfs	31.108 af
<b>Reach P1: Culvert</b>	Avg. Flow Depth=2.46'	Max Vel=14.61 fps	Inflow=118.51 cfs	11.247 af
48.0" Round Pipe n=0.011 L=64.0'	S=0.0100 '/	Capacity=169.76 cfs	Outflow=118.48 cfs	11.247 af
<b>Reach P2: Culvert</b>	Avg. Flow Depth=0.53'	Max Vel=7.31 fps	Inflow=4.12 cfs	0.368 af
18.0" Round Pipe n=0.011 L=72.0'	S=0.0150 '/	Capacity=15.20 cfs	Outflow=4.11 cfs	0.368 af
<b>Reach P2-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.17'	Max Vel=9.69 fps	Inflow=4.11 cfs	0.368 af
n=0.025 L=60.0'	S=0.3718 '/	Capacity=316.81 cfs	Outflow=4.11 cfs	0.368 af
<b>Reach P3: Culvert</b>	Avg. Flow Depth=0.53'	Max Vel=7.31 fps	Inflow=4.12 cfs	0.368 af
18.0" Round Pipe n=0.011 L=72.0'	S=0.0150 '/	Capacity=15.20 cfs	Outflow=4.12 cfs	0.368 af
<b>Reach P3-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.17'	Max Vel=9.89 fps	Inflow=4.12 cfs	0.368 af
n=0.025 L=60.0'	S=0.3942 '/	Capacity=326.18 cfs	Outflow=4.12 cfs	0.368 af
<b>Reach S: Chute-Concrete Block</b>	Avg. Flow Depth=0.86'	Max Vel=21.09 fps	Inflow=152.24 cfs	12.773 af
n=0.025 L=459.0'	S=0.2500 '/	Capacity=877.30 cfs	Outflow=151.93 cfs	12.773 af
<b>Reach SE: Chute-Concrete Block</b>	Avg. Flow Depth=0.83'	Max Vel=20.70 fps	Inflow=142.28 cfs	13.426 af
n=0.025 L=450.0'	S=0.2499 '/	Capacity=877.14 cfs	Outflow=142.07 cfs	13.426 af
<b>Reach SE1: Chute-Concrete Block</b>	Avg. Flow Depth=1.10'	Max Vel=13.74 fps	Inflow=142.07 cfs	13.426 af
n=0.025 L=62.0'	S=0.0806 '/	Capacity=498.27 cfs	Outflow=142.01 cfs	13.426 af
<b>Reach SW: Chute-Concrete Block</b>	Avg. Flow Depth=0.81'	Max Vel=20.41 fps	Inflow=135.35 cfs	11.355 af
n=0.025 L=404.0'	S=0.2500 '/	Capacity=877.30 cfs	Outflow=135.10 cfs	11.355 af
<b>Reach SW-1: Chute-Concrete Block</b>	Avg. Flow Depth=0.96'	Max Vel=15.98 fps	Inflow=135.10 cfs	11.355 af
n=0.025 L=266.0'	S=0.1269 '/	Capacity=624.99 cfs	Outflow=134.87 cfs	11.355 af
<b>Reach W: Chute-Concrete Block</b>	Avg. Flow Depth=0.93'	Max Vel=22.10 fps	Inflow=179.96 cfs	16.468 af
n=0.025 L=464.0'	S=0.2500 '/	Capacity=877.30 cfs	Outflow=179.70 cfs	16.468 af

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<b>Pond PA: Retention Pond A</b>	Peak Elev=49.73'	Storage=36.905 af	Inflow=324.39 cfs	36.905 af	Outflow=0.00 cfs	0.000 af
<b>Pond PB: Detention Pond B</b>	Peak Elev=52.22'	Storage=16.607 af	Inflow=331.73 cfs	32.018 af	Outflow=42.26 cfs	31.217 af
<b>Pond PC: Retention Pond C</b>	Peak Elev=45.81'	Storage=46.421 af	Inflow=446.58 cfs	46.421 af	Outflow=0.00 cfs	0.000 af

**Total Runoff Area = 164.599 ac   Runoff Volume = 125.910 af   Average Runoff Depth = 9.18"**  
**100.00% Pervious = 164.599 ac   0.00% Impervious = 0.000 ac**

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**Summary for Subcatchment 1C: 1C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af, Depth= 8.83"

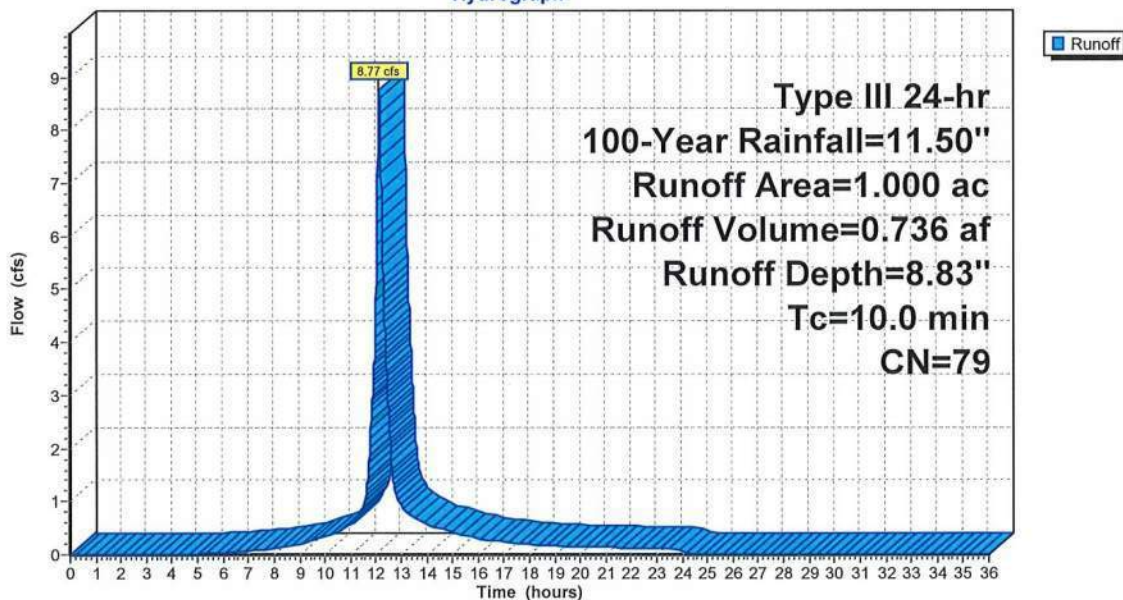
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 1C: 1C Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment 2C: 2C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 12.98 cfs @ 12.14 hrs, Volume= 1.089 af, Depth= 8.83"

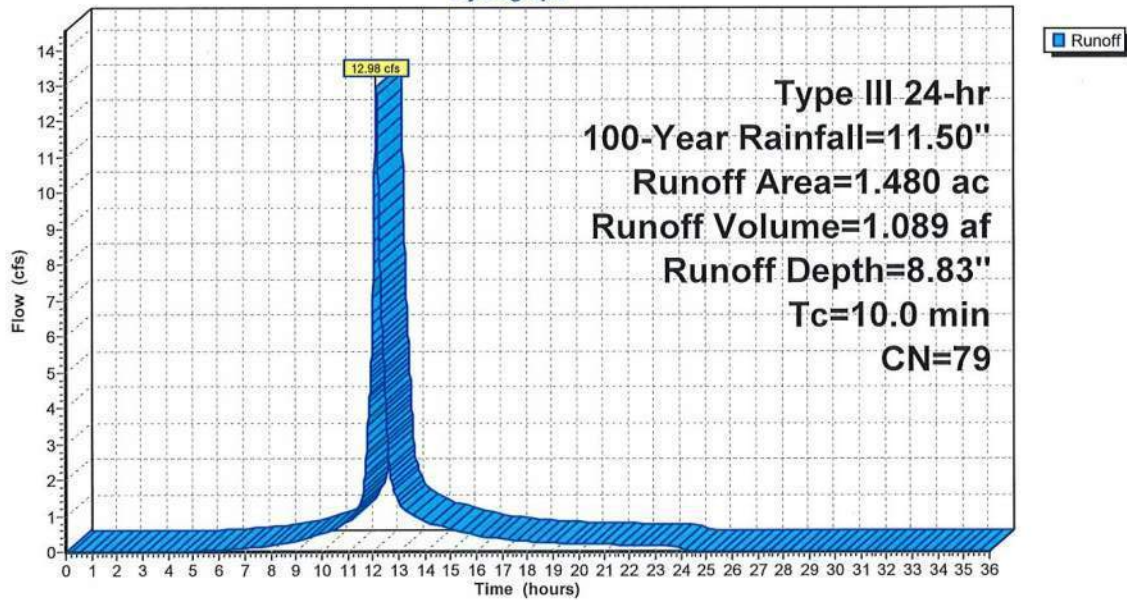
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.480	79	50-75% Grass cover, Fair, HSG C
1.480		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 2C: 2C Drainage Area**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment 3C: 3C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 14.38 cfs @ 12.14 hrs, Volume= 1.207 af, Depth= 8.83"

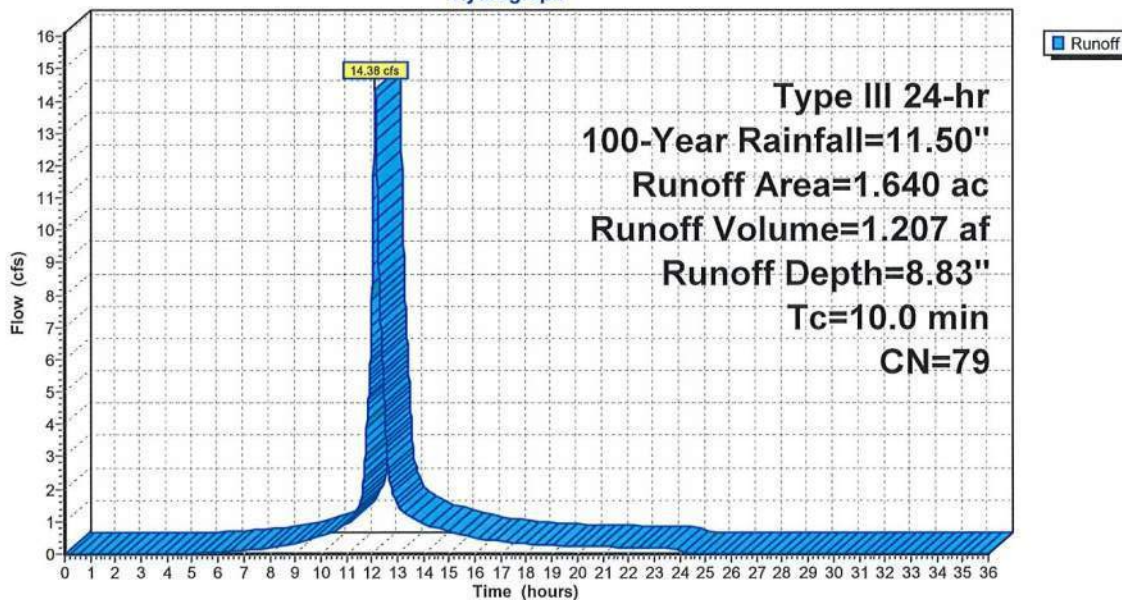
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.640	79	50-75% Grass cover, Fair, HSG C
1.640		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Surface Drainage to Pond B

**Subcatchment 3C: 3C Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment 4C: 4C Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 7.98 cfs @ 12.14 hrs, Volume= 0.670 af, Depth= 8.83"

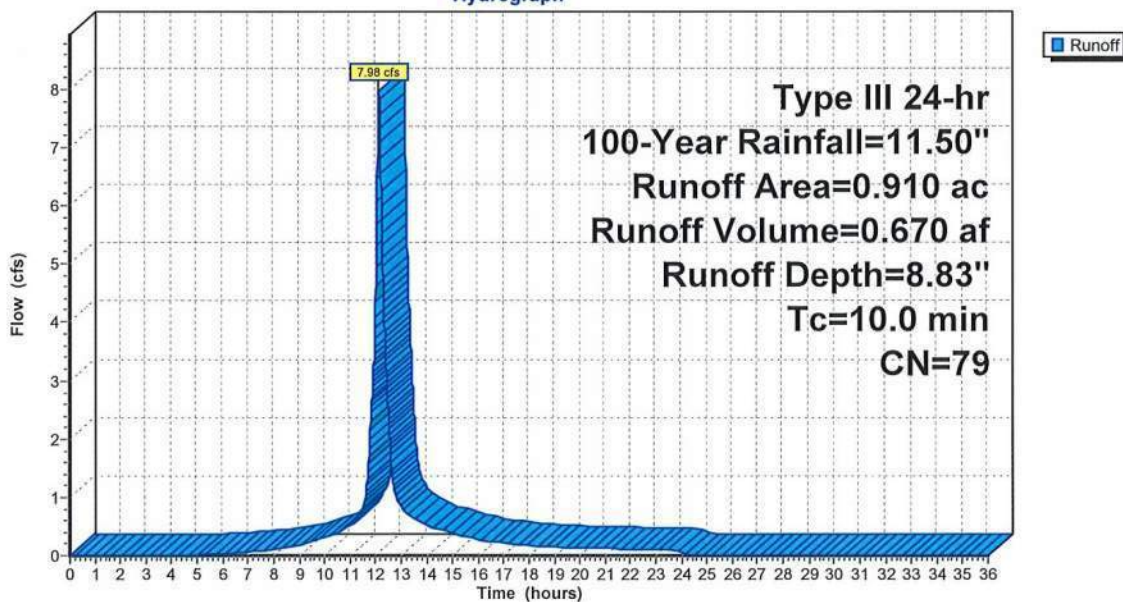
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
0.910	79	50-75% Grass cover, Fair, HSG C
0.910		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Surface Drainage to Pond B

**Subcatchment 4C: 4C Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

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**Summary for Subcatchment 5C: A2 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af, Depth= 8.83"

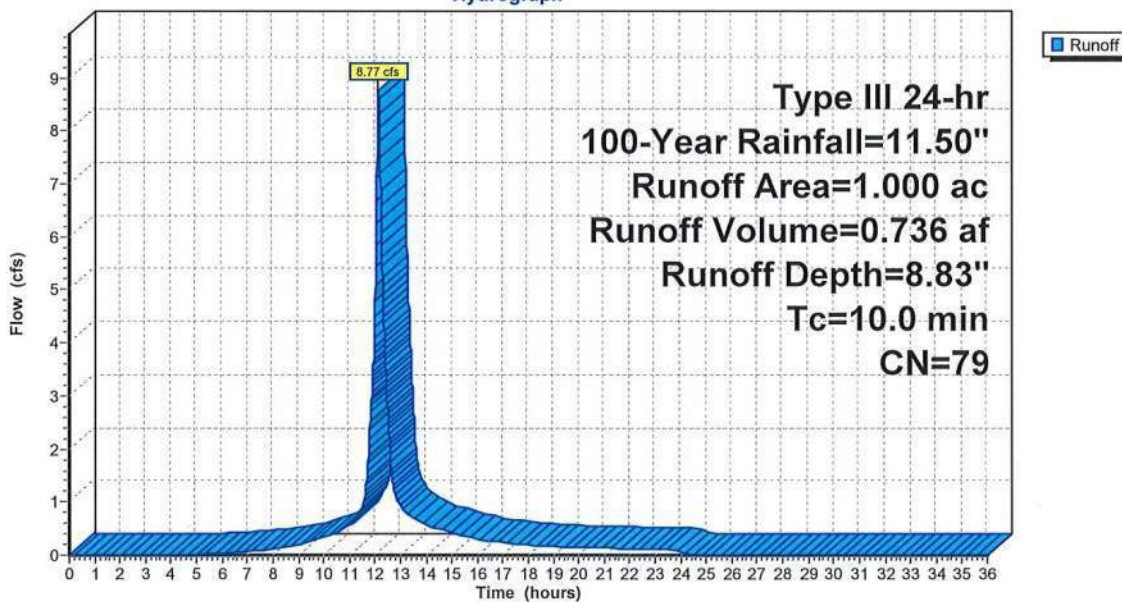
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 5C: A2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

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**Summary for Subcatchment 6C: A3 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af, Depth= 8.83"

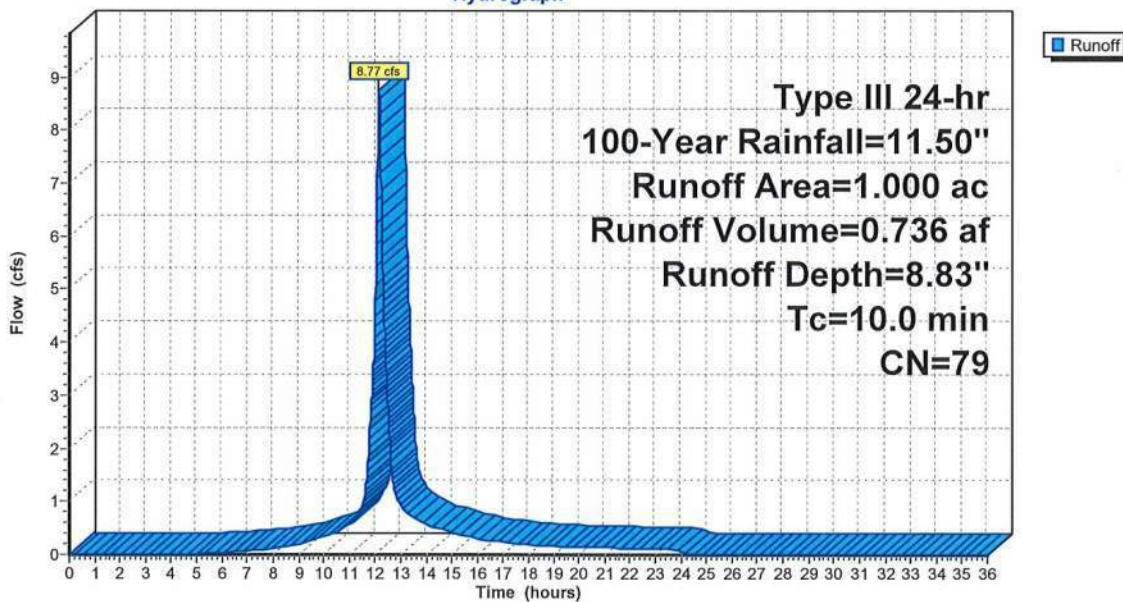
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 6C: A3 Drainage Area**

Hydrograph



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**Summary for Subcatchment 7C: A2 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af, Depth= 8.83"

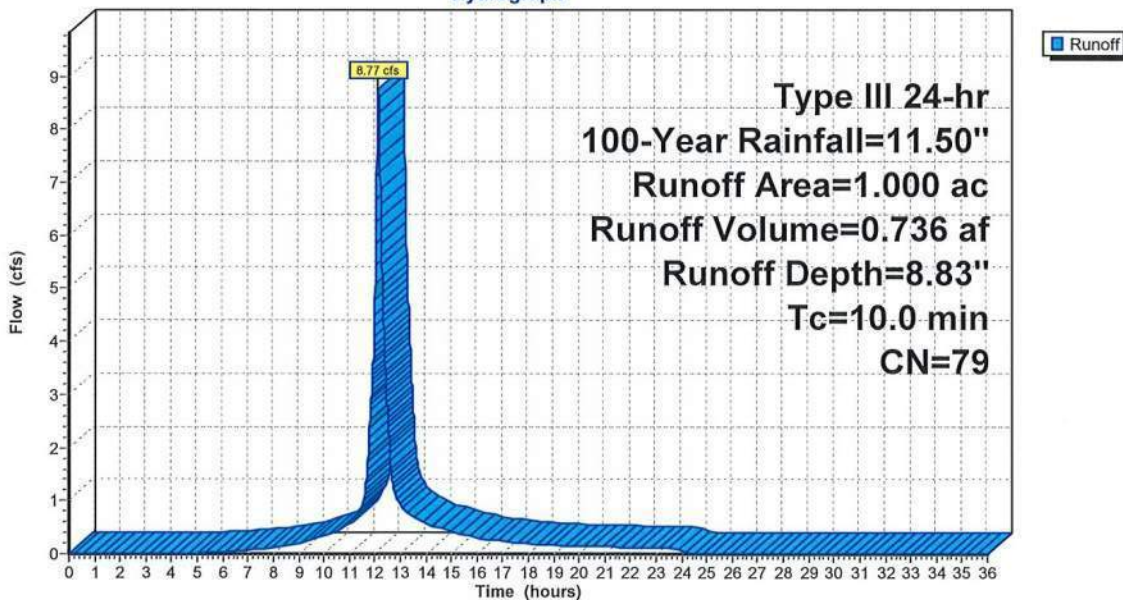
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
1.000	79	50-75% Grass cover, Fair, HSG C
1.000		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment 7C: A2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A1S: A1S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 70.23 cfs @ 12.14 hrs, Volume= 5.892 af, Depth= 8.83"

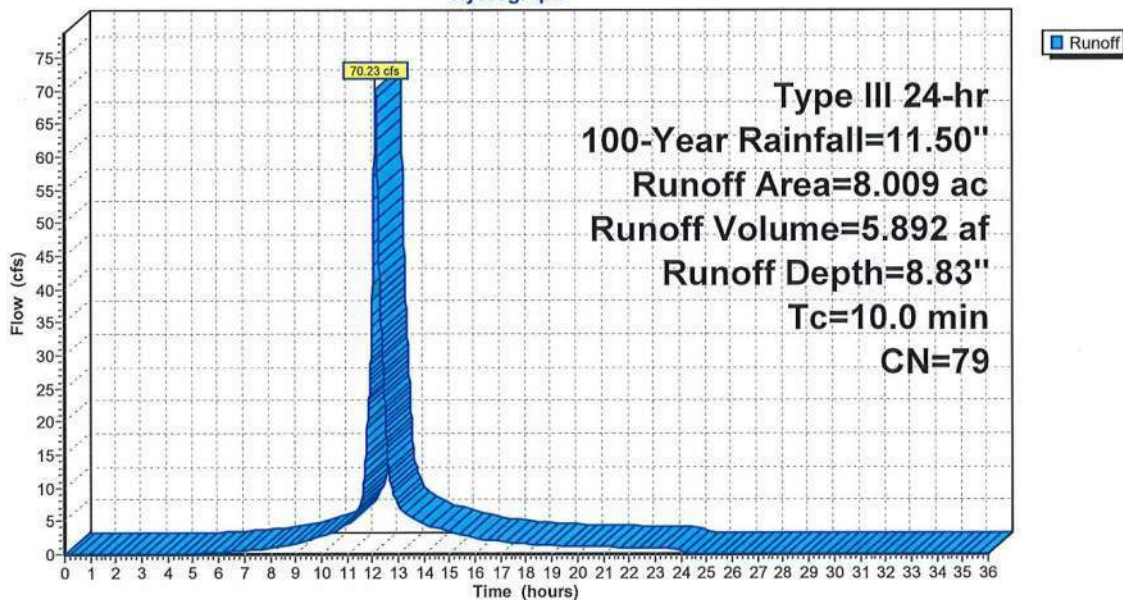
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
8.009	79	50-75% Grass cover, Fair, HSG C
8.009		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1S-Chute Flow Evaluation

**Subcatchment A1S: A1S Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A1T: A1T Drainage Area**

Runoff = 65.11 cfs @ 12.14 hrs, Volume= 5.463 af, Depth= 8.83"

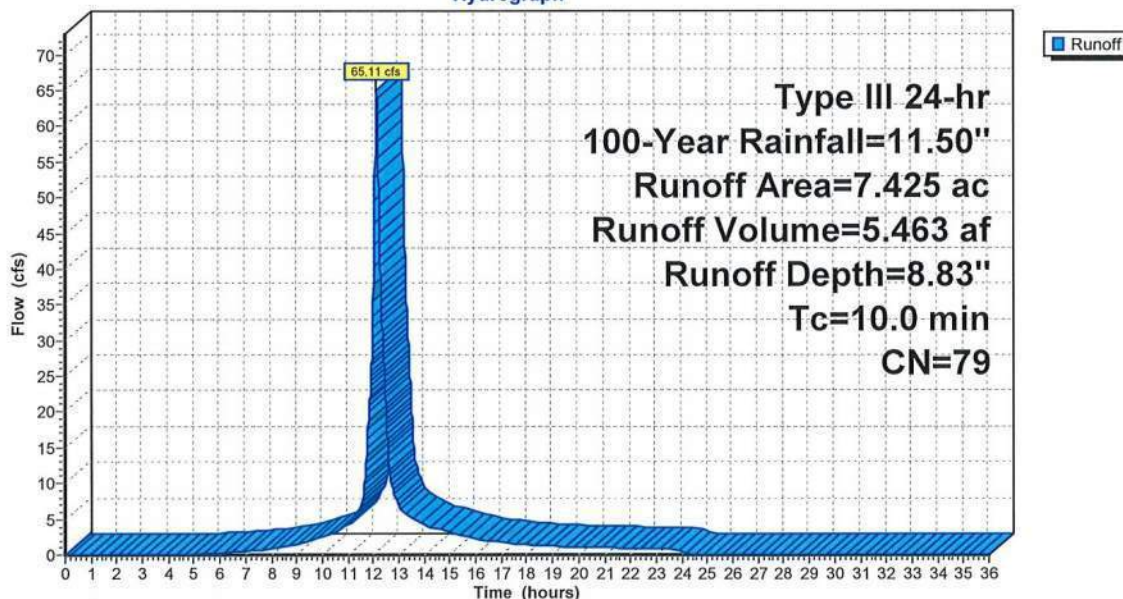
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
7.425	79	50-75% Grass cover, Fair, HSG C
7.425		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1T-Chute Flow Evaluation

**Subcatchment A1T: A1T Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A2S: A2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 107.35 cfs @ 12.14 hrs, Volume= 9.006 af, Depth= 8.83"

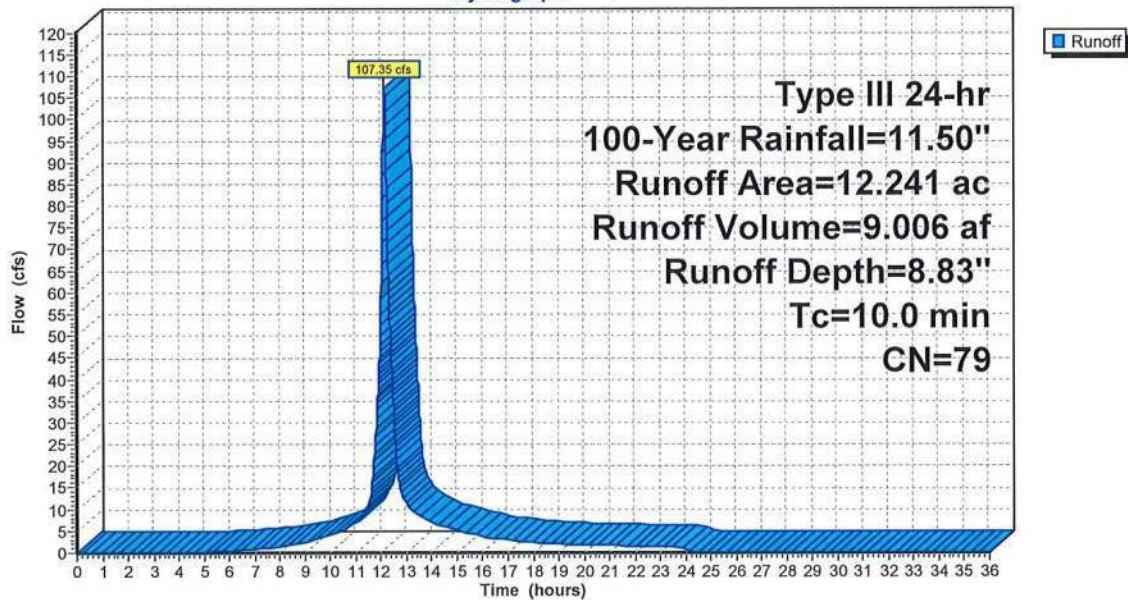
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
12.241	79	50-75% Grass cover, Fair, HSG C
12.241		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2S: A2 Drainage Area**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A2T: A2 Drainage Area**

Runoff = 44.90 cfs @ 12.14 hrs, Volume= 3.767 af, Depth= 8.83"

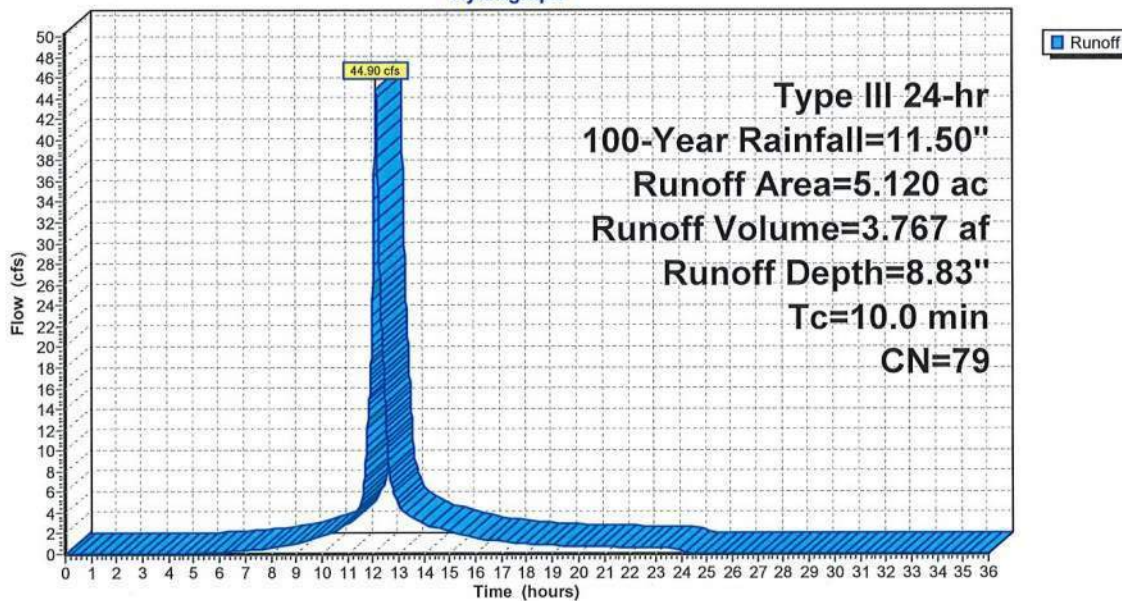
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
5.120	79	50-75% Grass cover, Fair, HSG C
5.120		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2T: A2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A3S: A3S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 94.36 cfs @ 12.14 hrs, Volume= 7.916 af, Depth= 8.83"

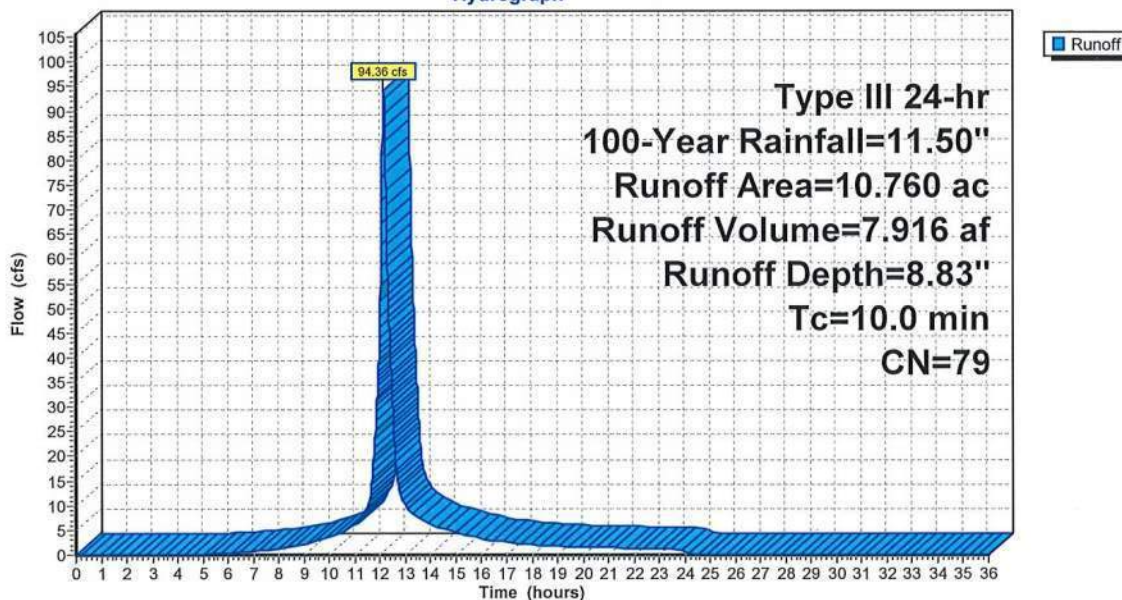
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
10.760	79	50-75% Grass cover, Fair, HSG C
10.760		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A3S-Chute Flow Evaluation

**Subcatchment A3S: A3S Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment A3T: A3T Drainage Area**

Runoff = 54.75 cfs @ 12.22 hrs, Volume= 5.510 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

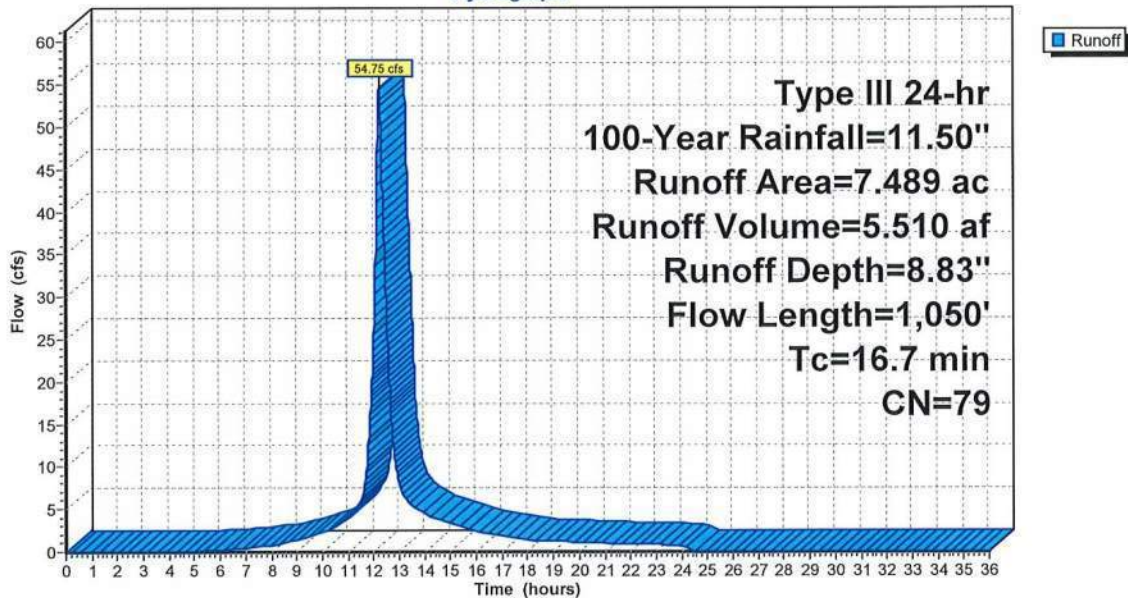
Area (ac)	CN	Description
7.489	79	50-75% Grass cover, Fair, HSG C
7.489		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.6	750		1.30		Direct Entry, A3T-Chute Flow Evaluation
7.1	300		0.70		Direct Entry,
16.7	1,050	Total			

**Subcatchment A3T: A3T Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment B1S: B1S Drainage Area**

Use Conservative Value of Tc= 10 min.

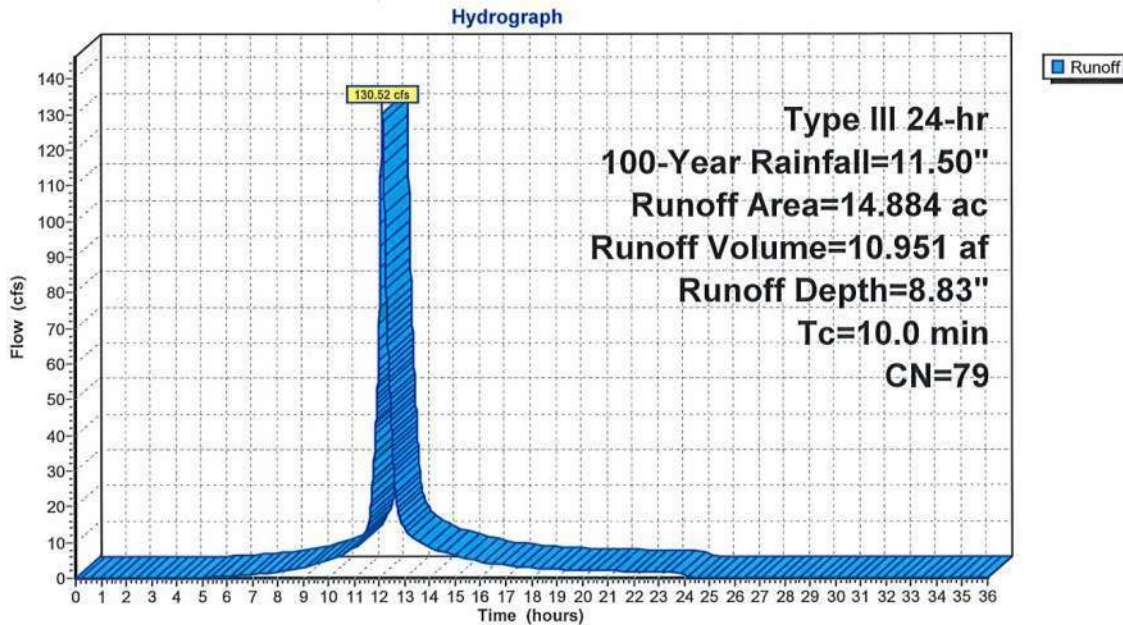
Runoff = 130.52 cfs @ 12.14 hrs, Volume= 10.951 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
14.884	79	50-75% Grass cover, Fair, HSG C
14.884		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B1S-Chute Flow Evaluation

**Subcatchment B1S: B1S Drainage Area**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment B1T: B1T Drainage Area**

Runoff = 55.80 cfs @ 12.21 hrs, Volume= 5.517 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

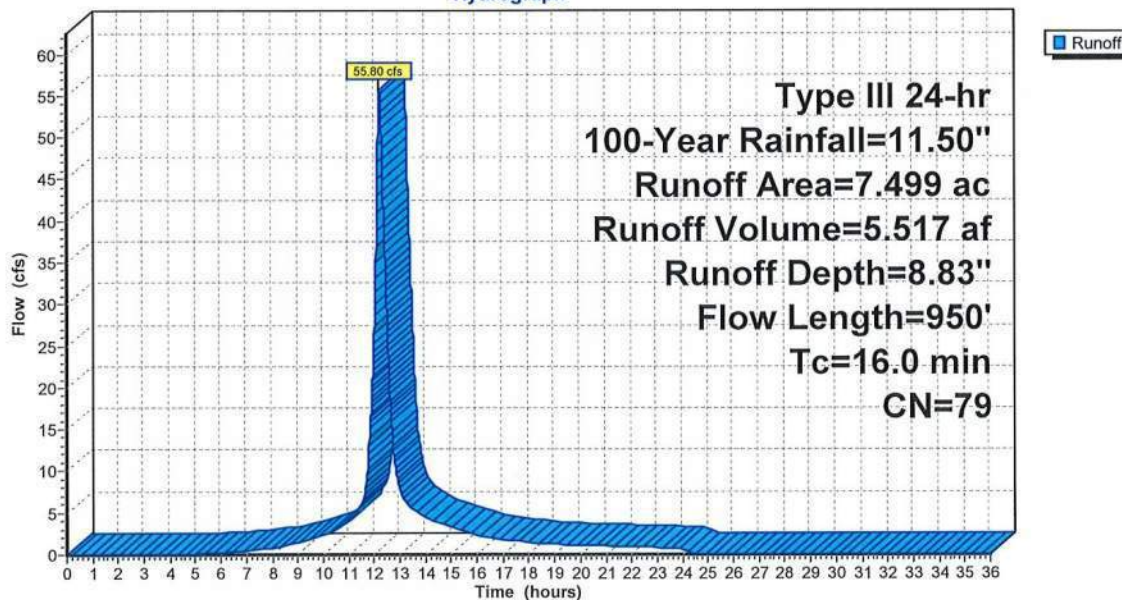
Area (ac)	CN	Description
7.499	79	50-75% Grass cover, Fair, HSG C
7.499		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B1T-Chute Flow Evaluation
8.3	350		0.70		Direct Entry,
16.0	950	Total			

**Subcatchment B1T: B1T Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment B2S: B2S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 77.22 cfs @ 12.14 hrs, Volume= 6.479 af, Depth= 8.83"

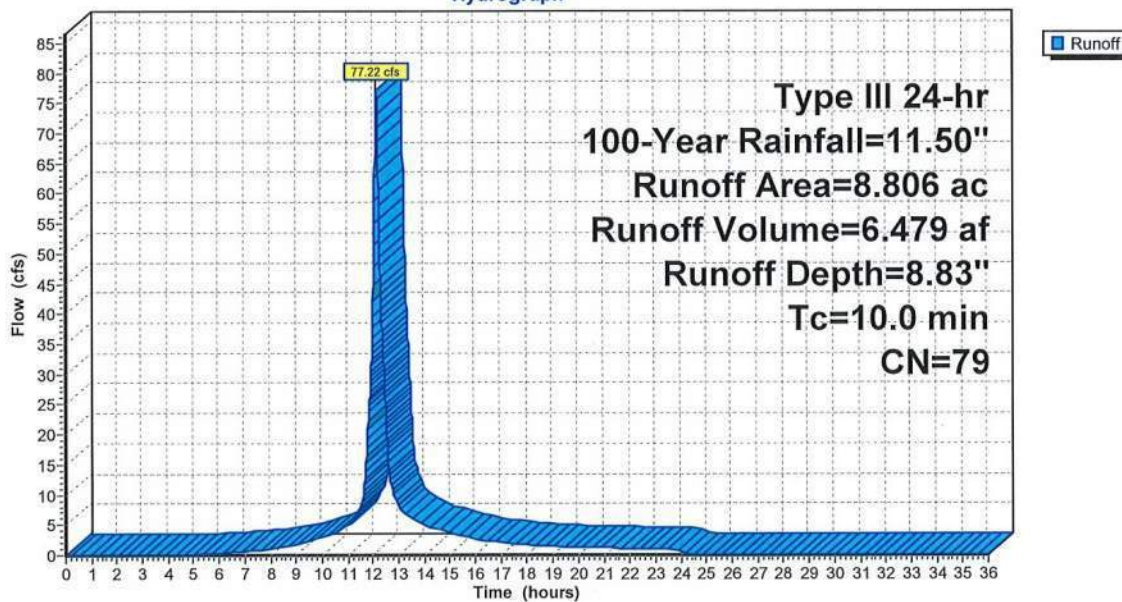
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
8.806	79	50-75% Grass cover, Fair, HSG C
8.806		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B2S-Chute Flow Evaluation

**Subcatchment B2S: B2S Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment B2T: B2T Drainage Area**

Runoff = 33.95 cfs @ 12.18 hrs, Volume= 3.170 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

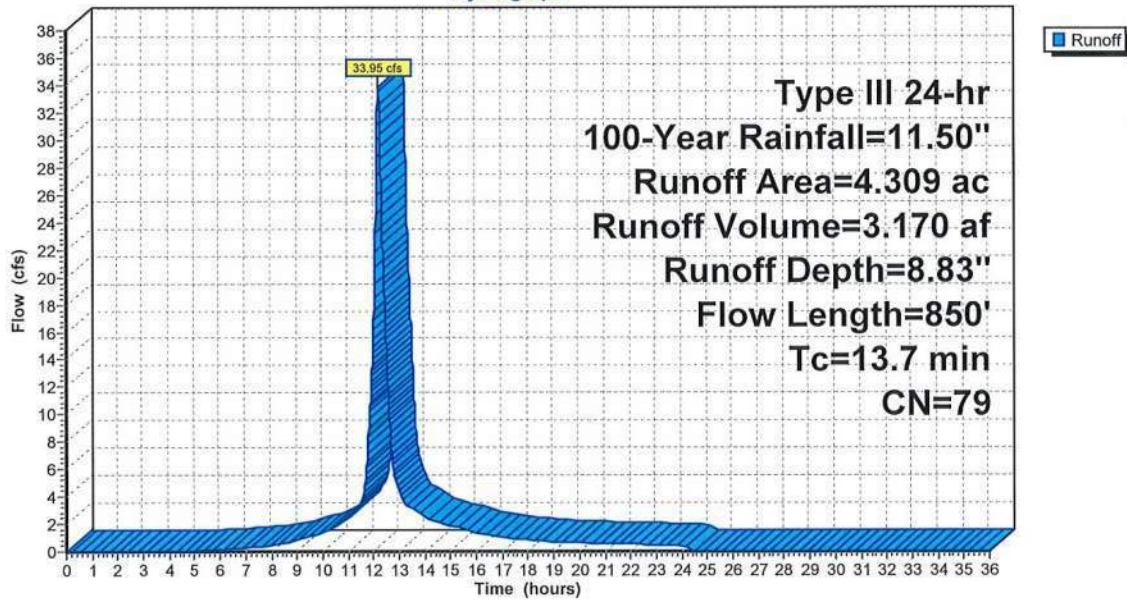
Area (ac)	CN	Description
4.309	79	50-75% Grass cover, Fair, HSG C
4.309		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B2T-Chute Flow Evaluation
6.0	250		0.70		Direct Entry,
13.7	850	Total			

**Subcatchment B2T: B2T Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1S: C1 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 100.90 cfs @ 12.14 hrs, Volume= 8.465 af, Depth= 8.83"

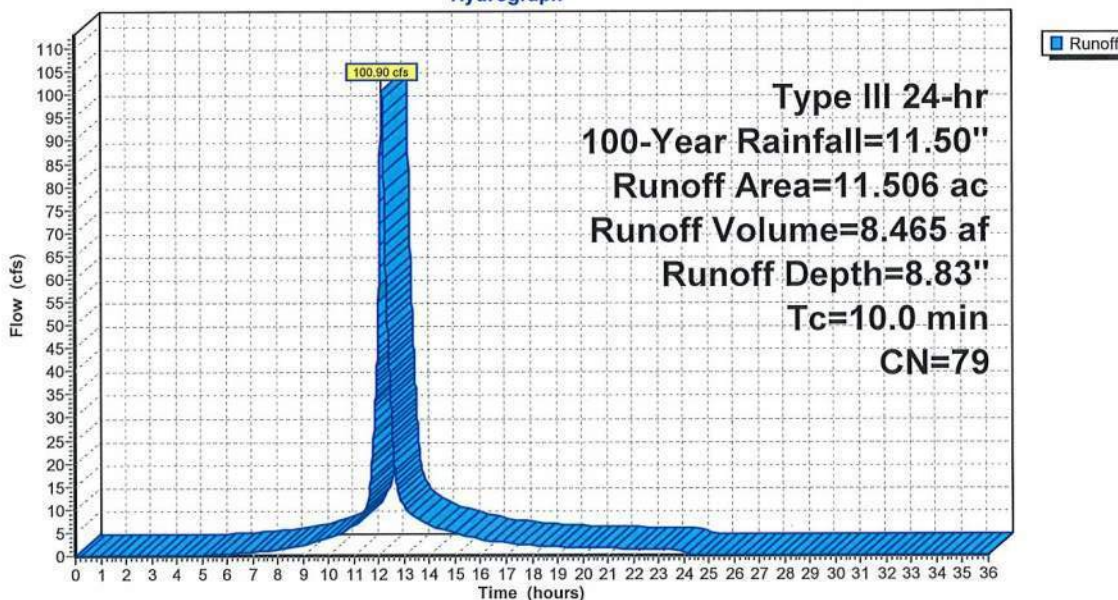
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
11.506	79	50-75% Grass cover, Fair, HSG C
11.506		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C1 Drainage Area

**Subcatchment C1S: C1 Drainage Area**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1SN1: C1SN1 Drainage Area**

Use Conservative Value of Tc=10 min

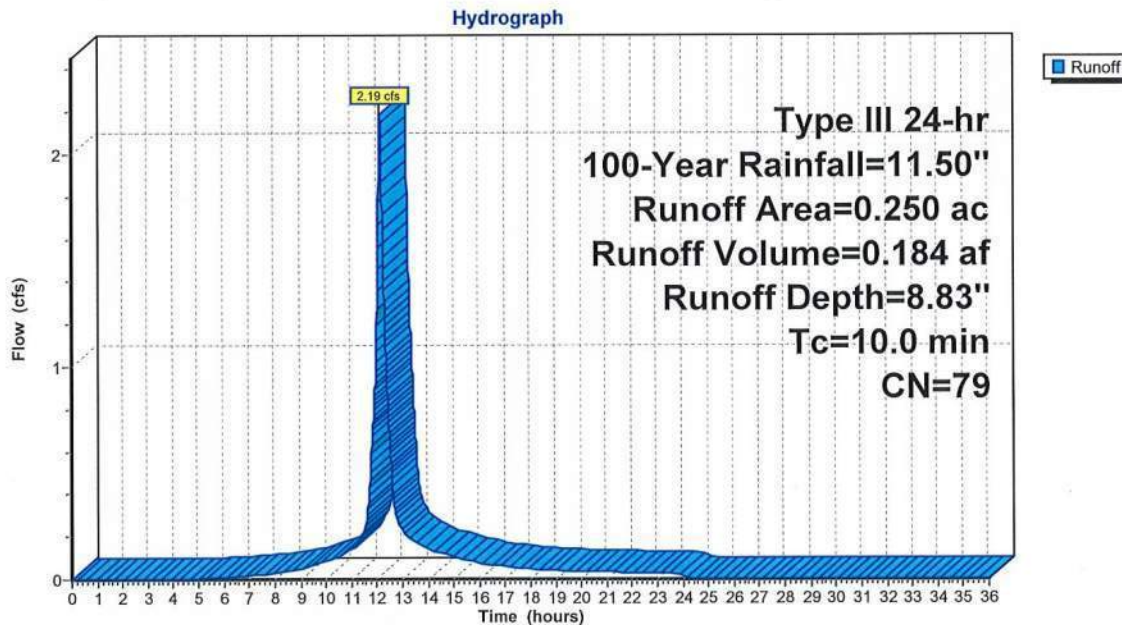
Runoff = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SN1: C1SN1 Drainage Area**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1SN2: C1SN2 Drainage Area**

Use Conservative Value of Tc=10 min

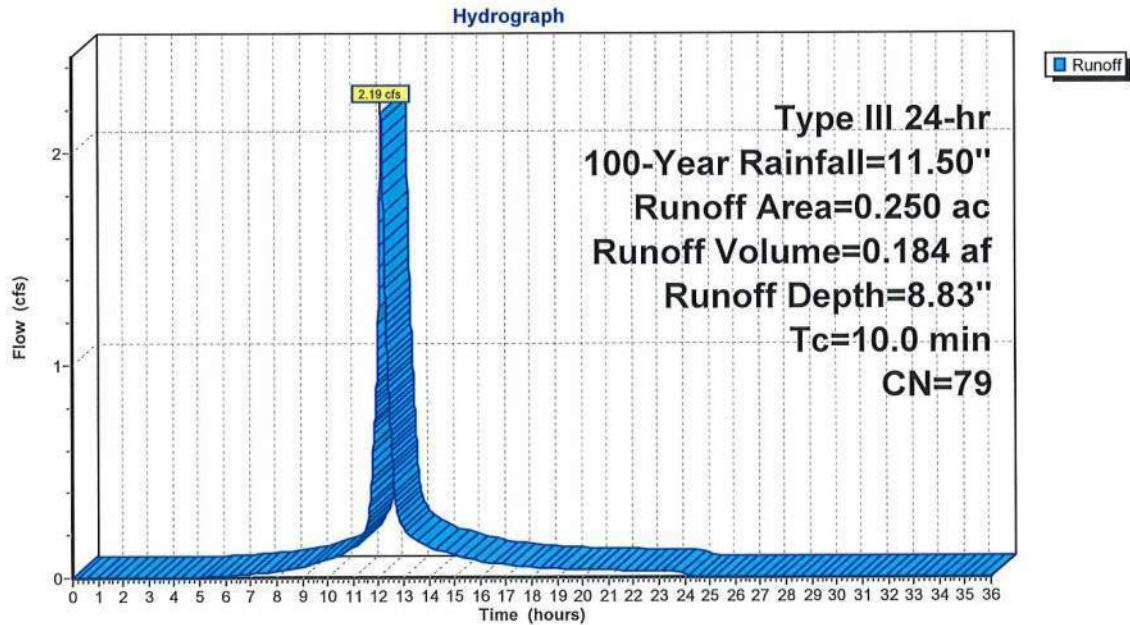
Runoff = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SN2: C1SN2 Drainage Area**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1SS1: C1SS1 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af, Depth= 8.83"

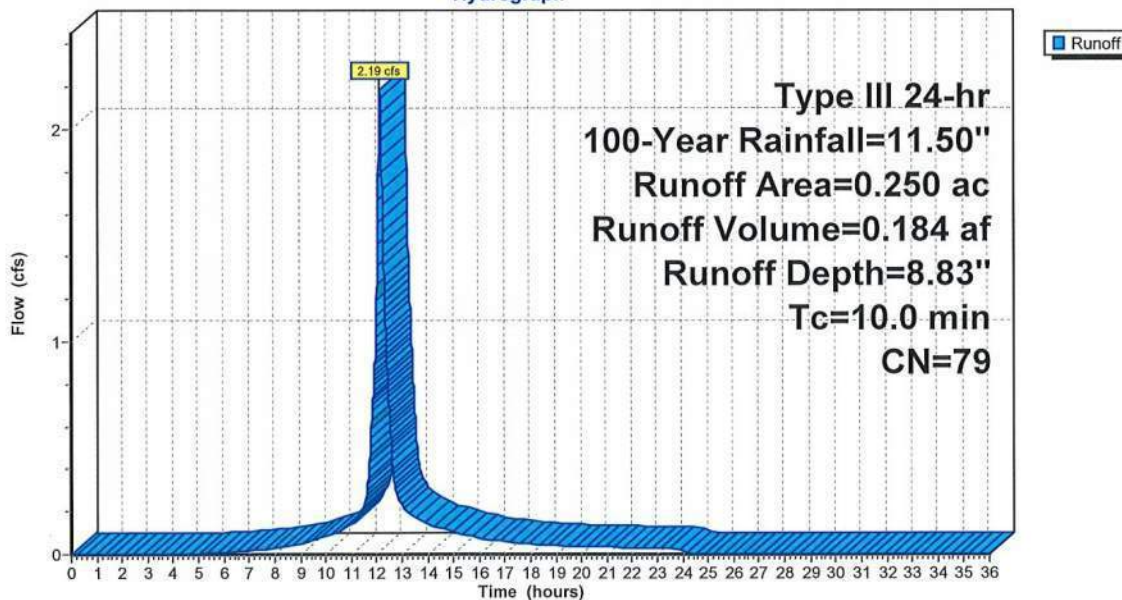
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SS1: C1SS1 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1SS2: C1SS2 Drainage Area**

Use Conservative Value of Tc=10 min

Runoff = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af, Depth= 8.83"

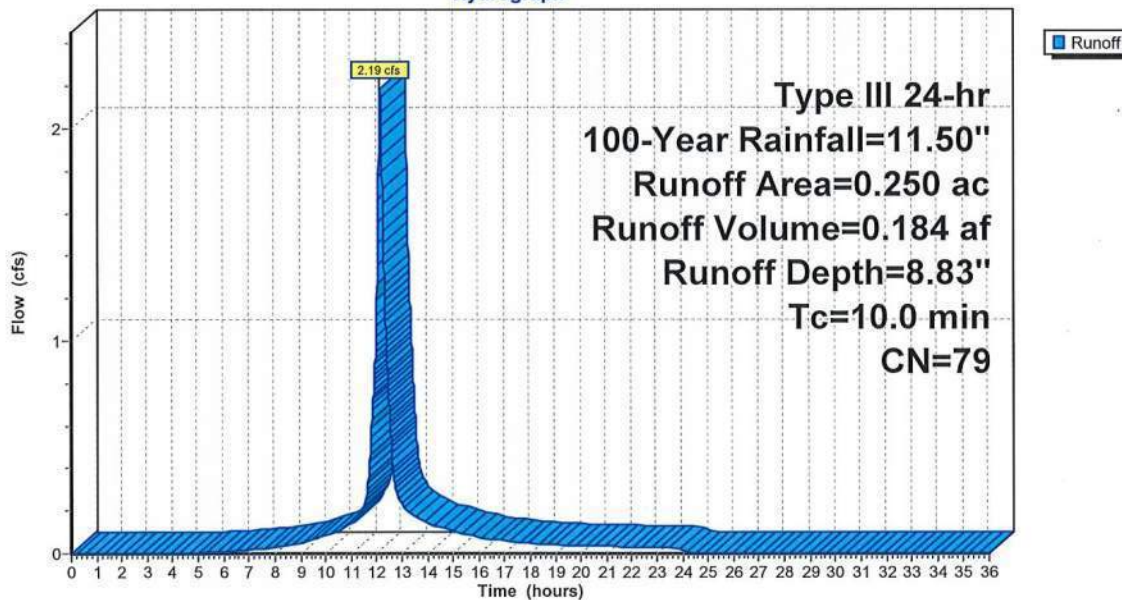
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
0.250	79	50-75% Grass cover, Fair, HSG C
0.250		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, Drainage Area at Bottom of Slope

**Subcatchment C1SS2: C1SS2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C1T: C1 Drainage Area**

Runoff = 51.20 cfs @ 12.17 hrs, Volume= 4.629 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

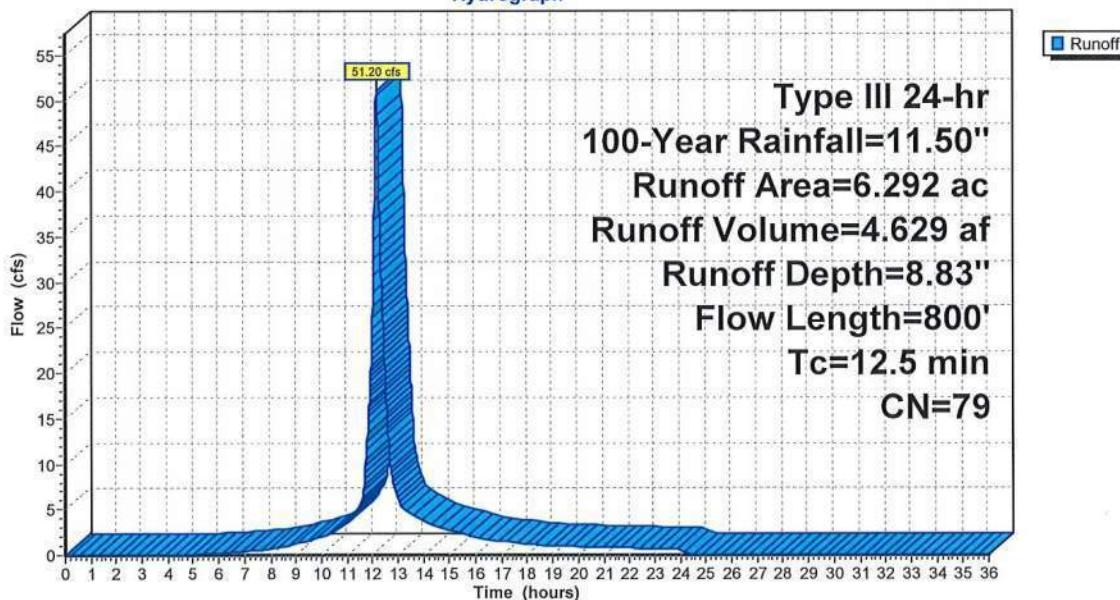
Area (ac)	CN	Description
6.292	79	50-75% Grass cover, Fair, HSG C
6.292		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C1 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800	Total			

**Subcatchment C1T: C1 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C2S: C2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 88.03 cfs @ 12.14 hrs, Volume= 7.385 af, Depth= 8.83"

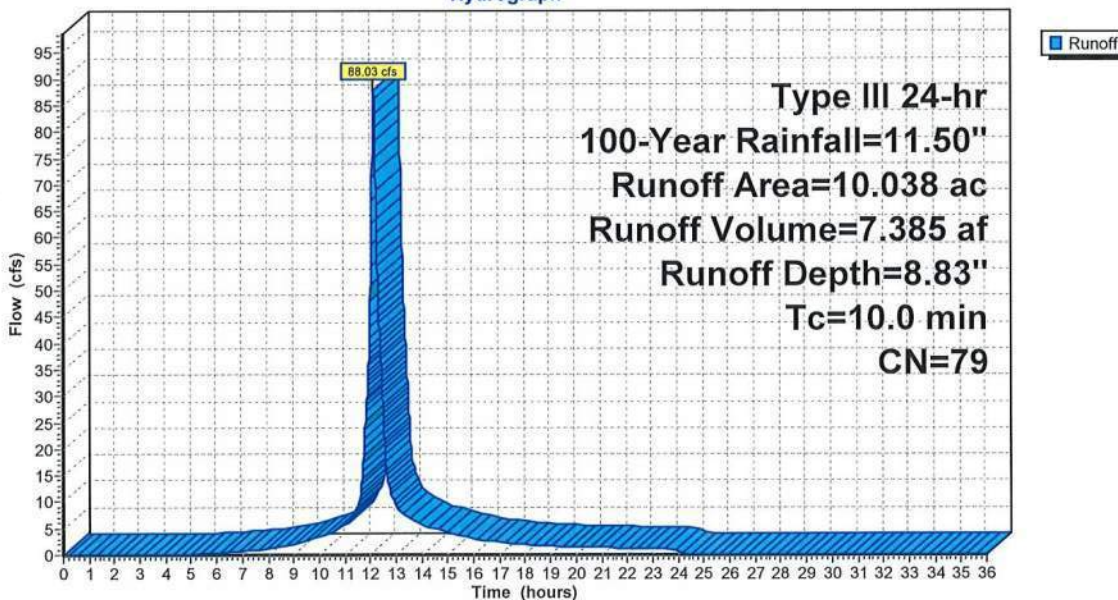
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
10.038	79	50-75% Grass cover, Fair, HSG C
10.038		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C2 Drainage Area

**Subcatchment C2S: C2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C2T: C2 Drainage Area**

Runoff = 42.72 cfs @ 12.17 hrs, Volume= 3.862 af, Depth= 8.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

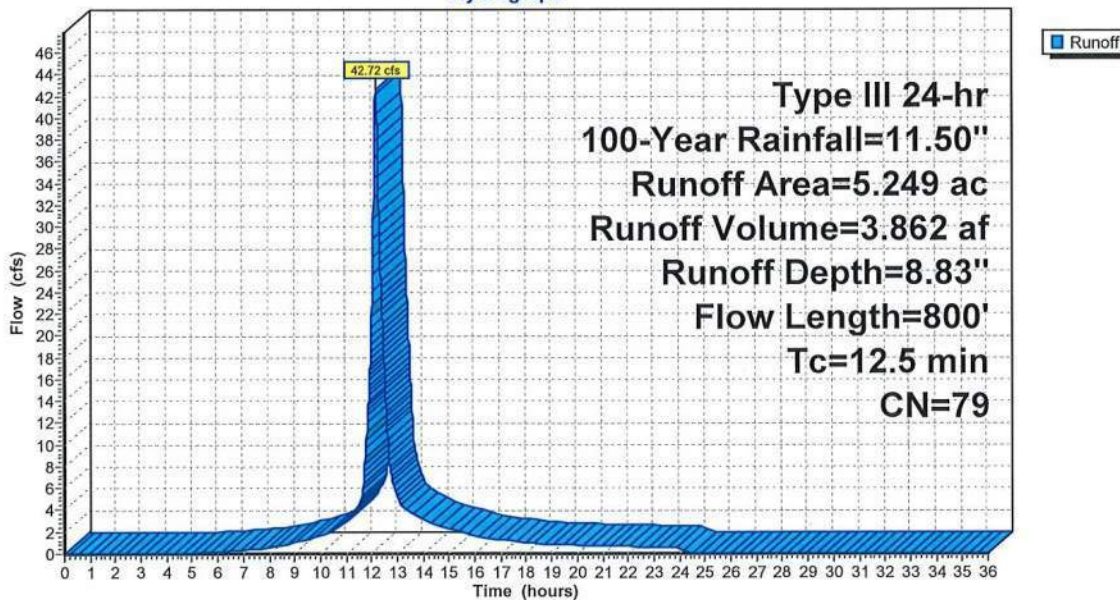
Area (ac)	CN	Description
5.249	79	50-75% Grass cover, Fair, HSG C
5.249		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C2 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800	Total			

**Subcatchment C2T: C2 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C3: C3 Drainage Area**

Existing Drainage Area Surface Drains to the North, Into Existing Low-Lying Excavated Pit C4 Drainage Area.

Runoff = 32.84 cfs @ 12.13 hrs, Volume= 2.845 af, Depth= 9.75"

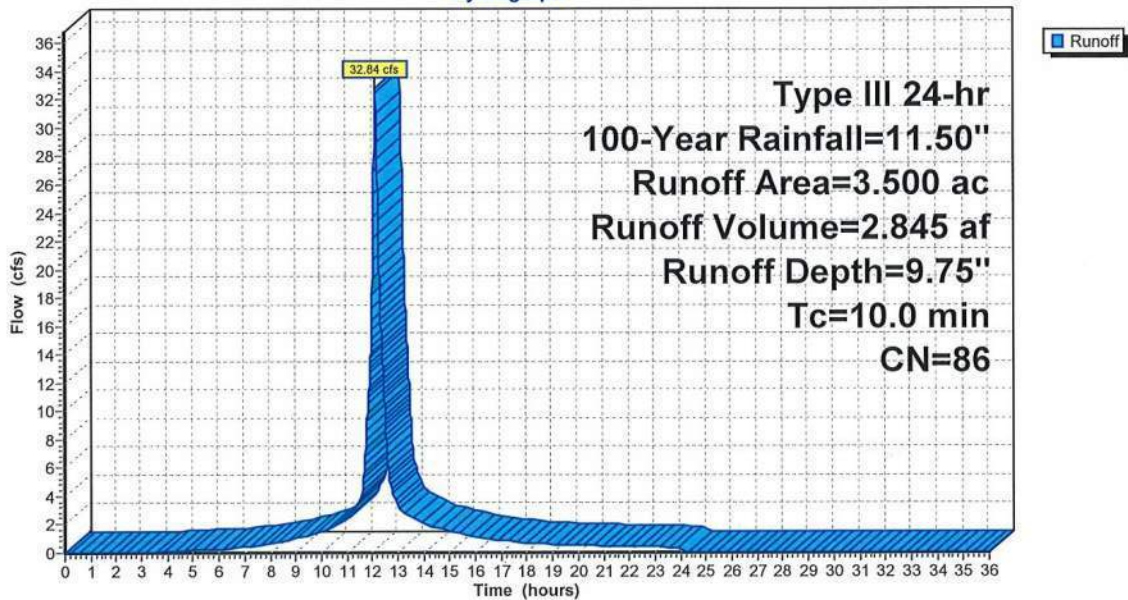
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
3.500	86	<50% Grass cover, Poor, HSG C
3.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C3 Drainage Area

**Subcatchment C3: C3 Drainage Area**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C4: C4 Drainage Area**

Existing Low-Lying Excavated Pit Area. Infiltration and Evaporation Occur Here.

Runoff = 89.15 cfs @ 12.13 hrs, Volume= 7.722 af, Depth= 9.75"

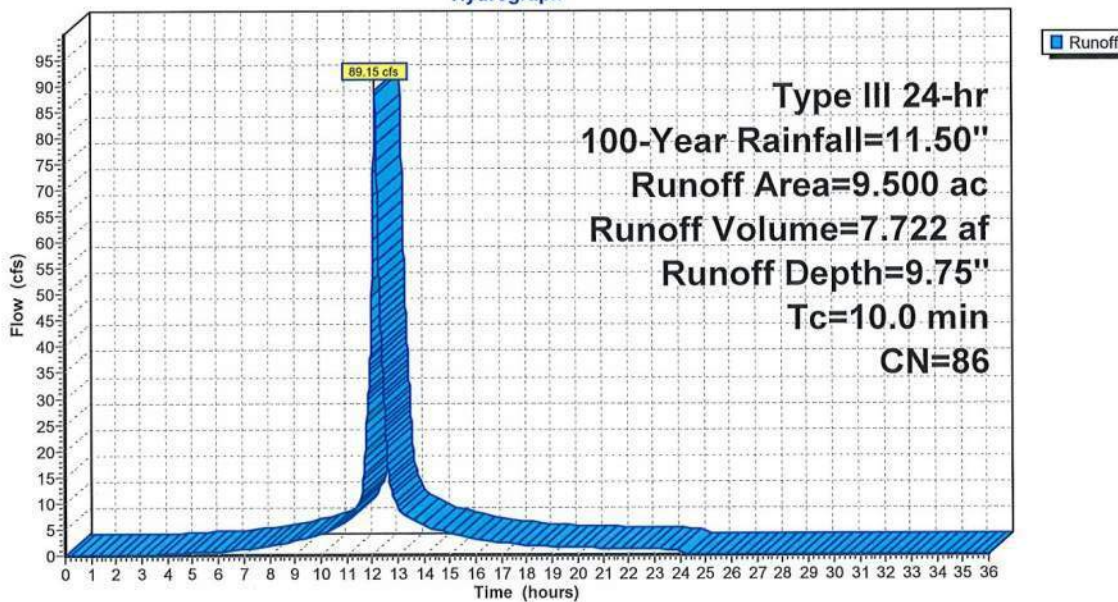
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
9.500	86	<50% Grass cover, Poor, HSG C
9.500		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C4 Drainage Area

**Subcatchment C4: C4 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C5: C5 Drainage Area**

Side Slope Drainage Area that Flows Into Pond C.

Runoff = 25.24 cfs @ 12.13 hrs, Volume= 2.186 af, Depth= 9.75"

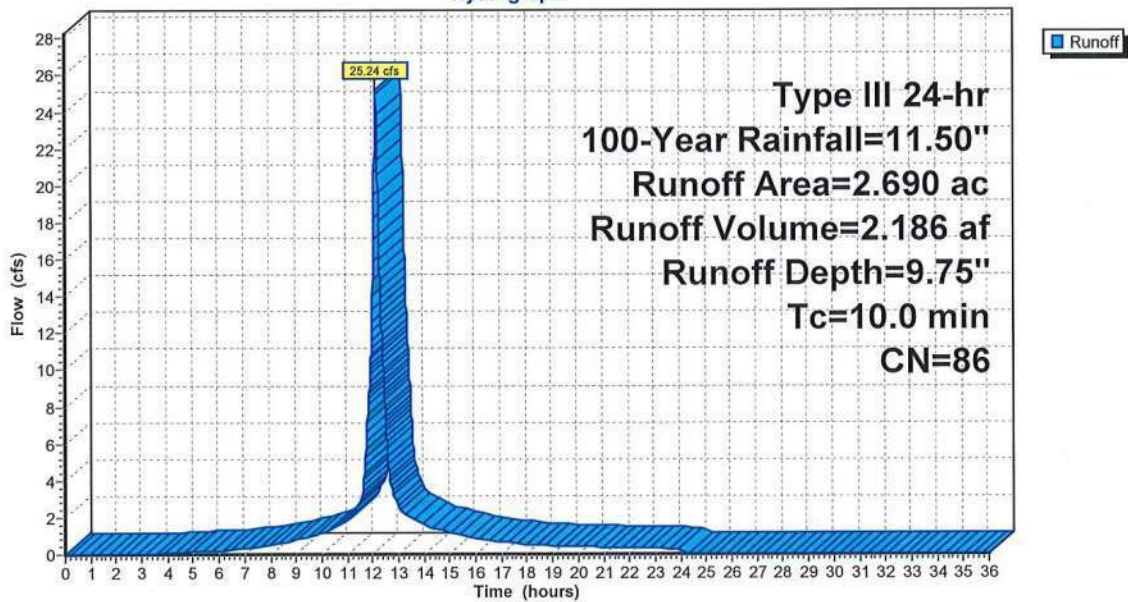
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
2.690	86	<50% Grass cover, Poor, HSG C
2.690		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C5 Drainage Area

**Subcatchment C5: C5 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment C6: C6 Drainage Area**

Surrounding Drainage Area that Flows Into Pond A.

Runoff = 37.37 cfs @ 12.13 hrs, Volume= 3.237 af, Depth= 9.75"

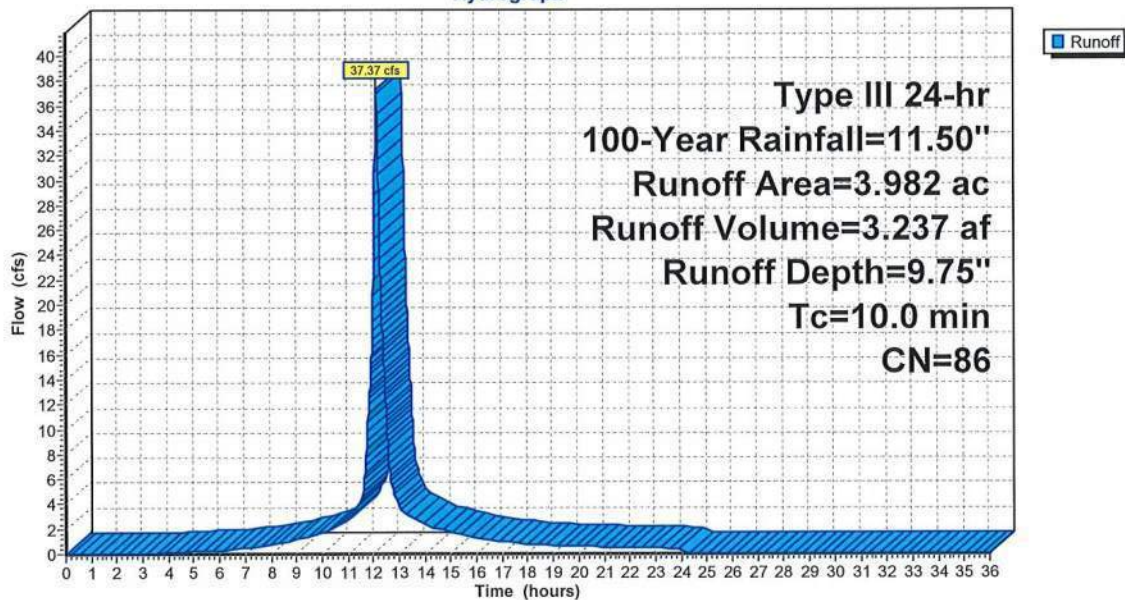
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
3.982	86	<50% Grass cover, Poor, HSG C
3.982		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C6 Drainage Area

**Subcatchment C6: C6 Drainage Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment PAR: PA Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 102.59 cfs @ 12.00 hrs, Volume= 6.980 af, Depth=11.26"

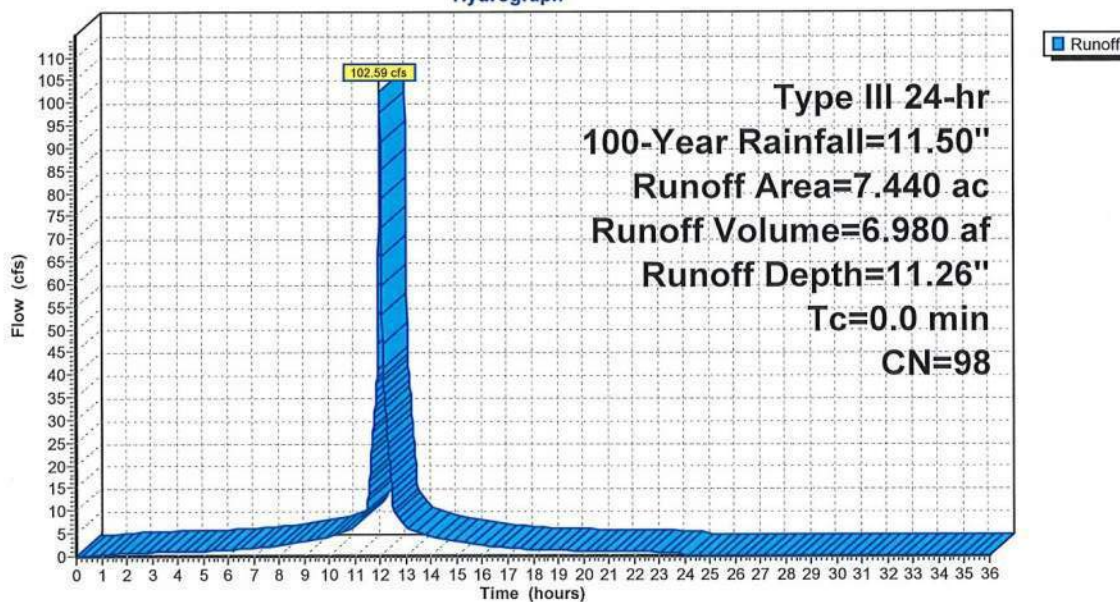
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
7.440	98	Water Surface, 0% imp, HSG C
7.440		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond A

**Subcatchment PAR: PA Rainfall Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment PBR: PB Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 59.15 cfs @ 12.00 hrs, Volume= 4.025 af, Depth=11.26"

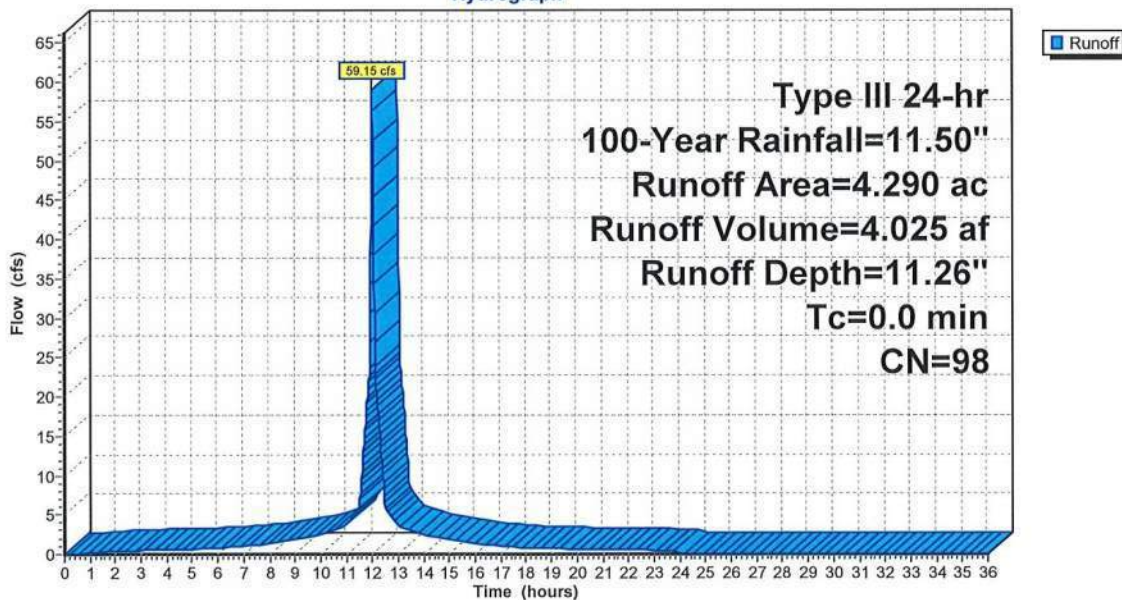
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
4.290	98	Water Surface, 0% imp, HSG C
4.290		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond B

**Subcatchment PBR: PB Rainfall Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Subcatchment PCR: PC Rainfall Area**

Use Conservative Value of Tc=10 min

Runoff = 62.60 cfs @ 12.00 hrs, Volume= 4.260 af, Depth=11.26"

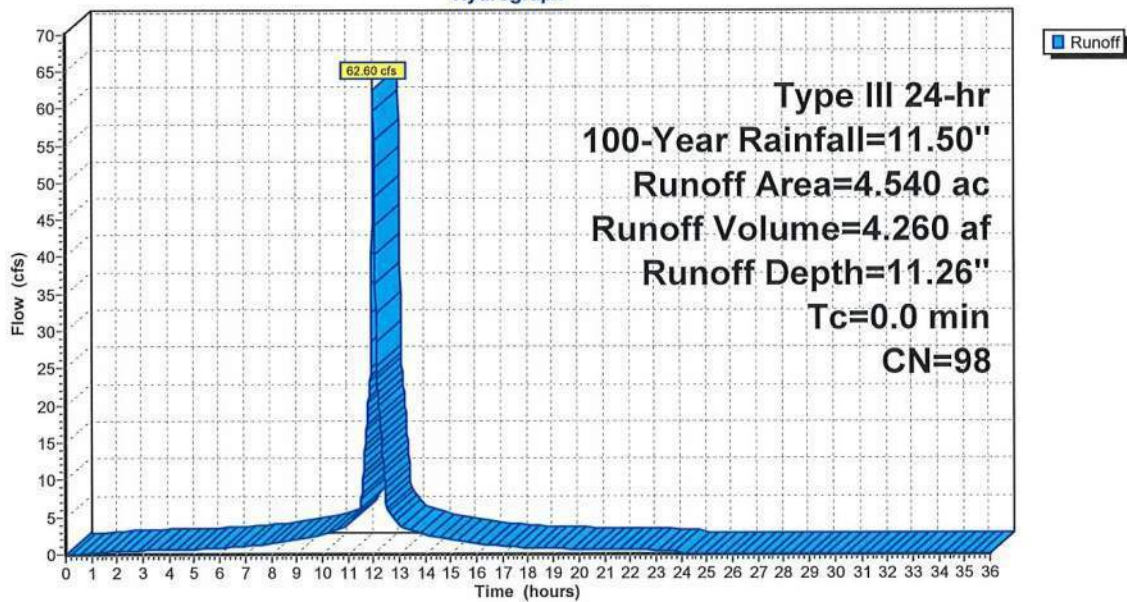
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100-Year Rainfall=11.50"

Area (ac)	CN	Description
4.540	98	Water Surface, 0% imp, HSG C
4.540		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry, Rainfall at Pond C

**Subcatchment PCR: PC Rainfall Area**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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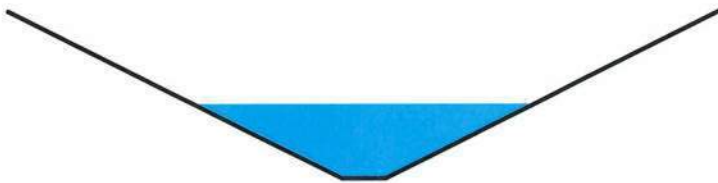
**Summary for Reach 1CC: 1CC Collector Channel**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 301.75 cfs @ 12.17 hrs, Volume= 27.992 af  
 Outflow = 300.25 cfs @ 12.20 hrs, Volume= 27.992 af, Atten= 0%, Lag= 1.6 min

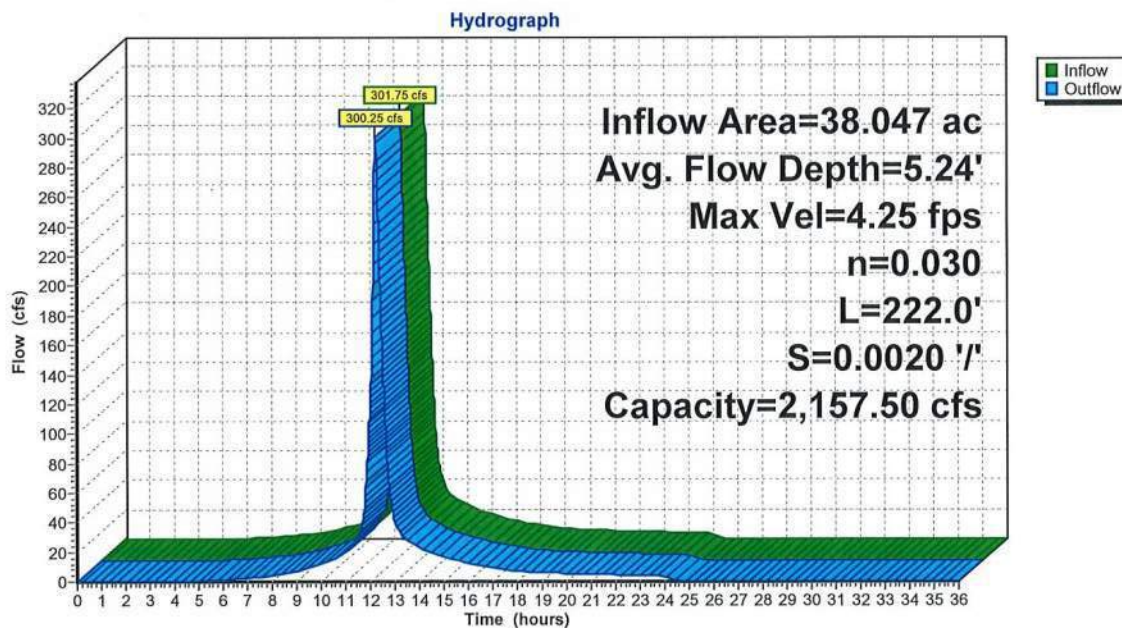
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.25 fps, Min. Travel Time= 0.9 min  
 Avg. Velocity = 1.43 fps, Avg. Travel Time= 2.6 min

Peak Storage= 15,702 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 5.24'  
 Bank-Full Depth= 11.73' Flow Area= 310.4 sf, Capacity= 2,157.50 cfs

3.00' x 11.73' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 49.92'  
 Length= 222.0' Slope= 0.0020 '/'  
 Inlet Invert= 53.89', Outlet Invert= 53.45'



**Reach 1CC: 1CC Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach 2CC: 2CC Collector Channel**

Inflow Area = 1.480 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 12.98 cfs @ 12.14 hrs, Volume= 1.089 af  
 Outflow = 11.11 cfs @ 12.30 hrs, Volume= 1.089 af, Atten= 14%, Lag= 10.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.74 fps, Min. Travel Time= 6.2 min  
 Avg. Velocity = 0.56 fps, Avg. Travel Time= 19.4 min

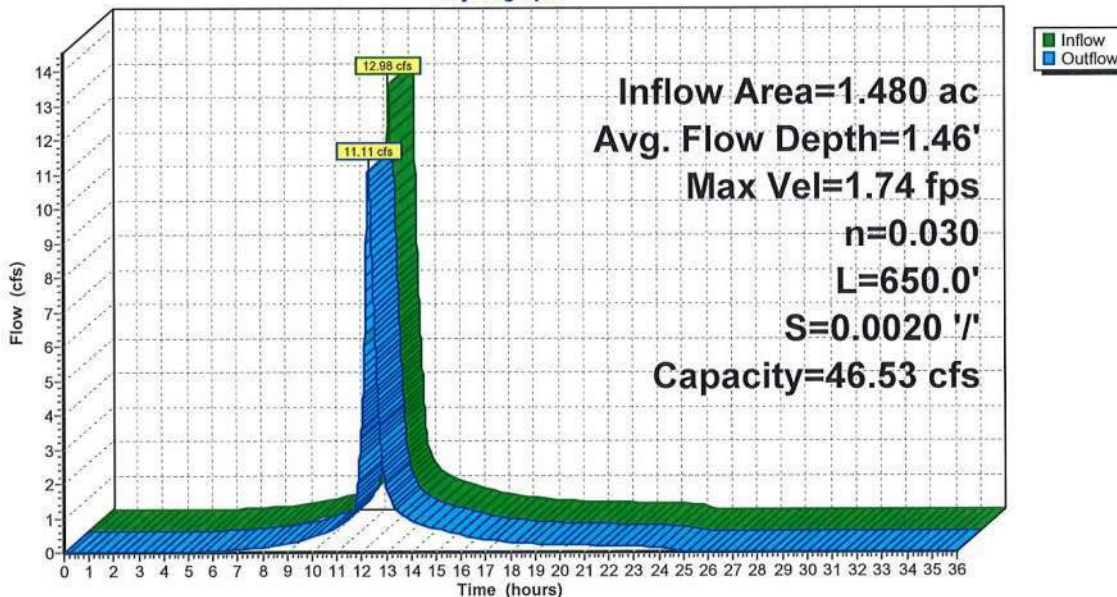
Peak Storage= 4,166 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 1.46'  
 Bank-Full Depth= 2.50' Flow Area= 18.8 sf, Capacity= 46.53 cfs

0.00' x 2.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 3.0 ' / ' Top Width= 15.00'  
 Length= 650.0' Slope= 0.0020 ' / '  
 Inlet Invert= 54.50', Outlet Invert= 53.20'



**Reach 2CC: 2CC Collector Channel**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach 5CC: A2 Collector Channel**

Inflow Area = 1.000 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af  
 Outflow = 7.45 cfs @ 12.31 hrs, Volume= 0.736 af, Atten= 15%, Lag= 10.5 min

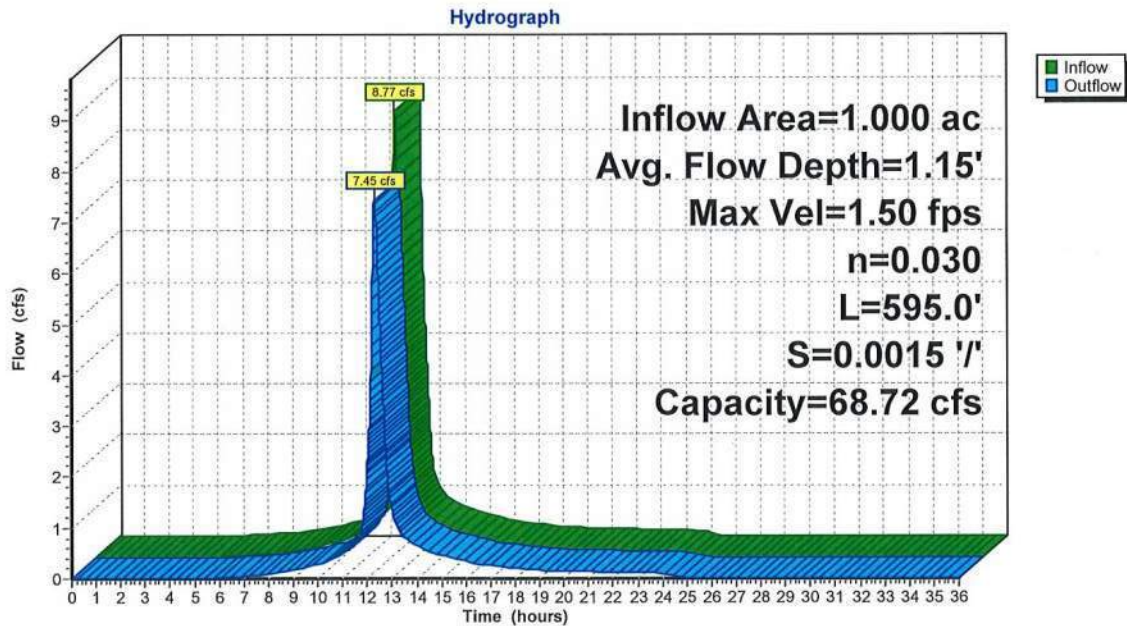
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.50 fps, Min. Travel Time= 6.6 min  
 Avg. Velocity = 0.46 fps, Avg. Travel Time= 21.6 min

Peak Storage= 2,954 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 1.15'  
 Bank-Full Depth= 3.14' Flow Area= 26.0 sf, Capacity= 68.72 cfs

2.00' x 3.14' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 14.56'  
 Length= 595.0' Slope= 0.0015 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.61'



**Reach 5CC: A2 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach 6CC: A3 Collector Channel**

Inflow Area = 1.000 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 8.77 cfs @ 12.14 hrs, Volume= 0.736 af  
 Outflow = 7.67 cfs @ 12.29 hrs, Volume= 0.736 af, Atten= 13%, Lag= 9.2 min

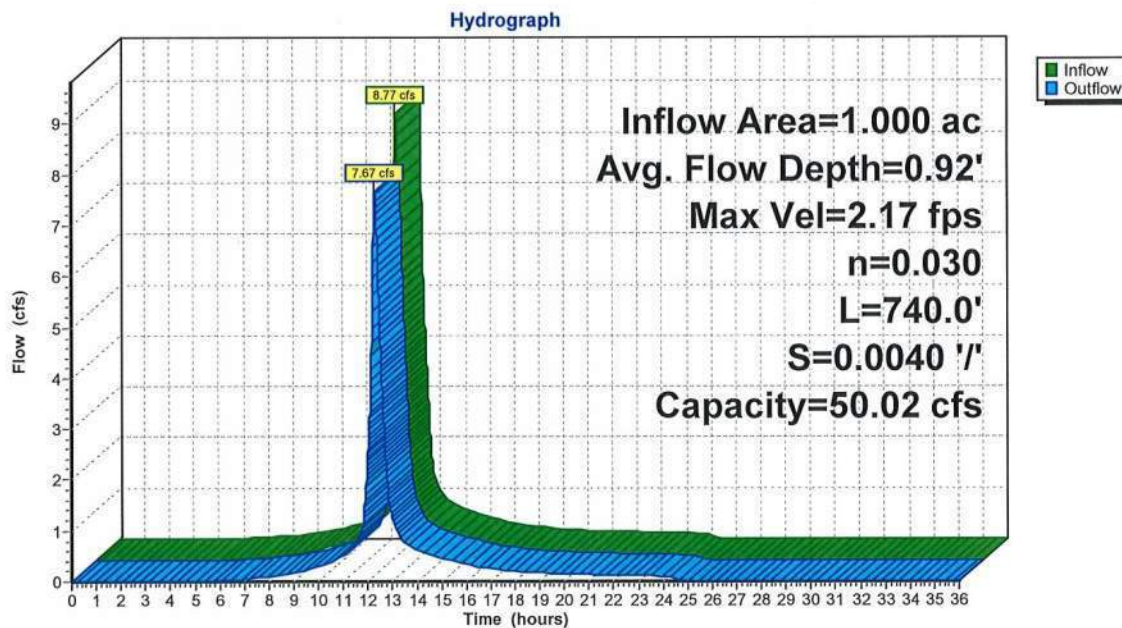
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 2.17 fps, Min. Travel Time= 5.7 min  
 Avg. Velocity = 0.64 fps, Avg. Travel Time= 19.2 min

Peak Storage= 2,614 cf @ 12.19 hrs  
 Average Depth at Peak Storage= 0.92'  
 Bank-Full Depth= 2.21' Flow Area= 14.2 sf, Capacity= 50.02 cfs

2.00' x 2.21' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 10.84'  
 Length= 740.0' Slope= 0.0040 '/'  
 Inlet Invert= 59.50', Outlet Invert= 56.54'



**Reach 6CC: A3 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach A2-1: A2-1 Channel**

Inflow Area = 2.000 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 12.75 cfs @ 12.25 hrs, Volume= 1.471 af  
 Outflow = 12.71 cfs @ 12.31 hrs, Volume= 1.471 af, Atten= 0%, Lag= 3.5 min

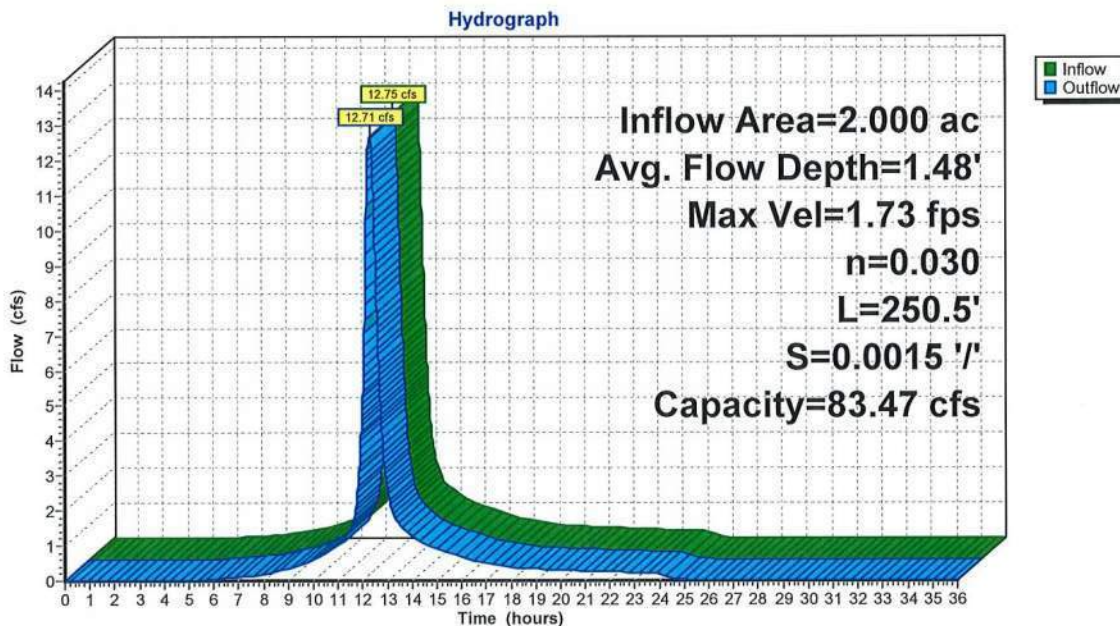
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.73 fps, Min. Travel Time= 2.4 min  
 Avg. Velocity = 0.56 fps, Avg. Travel Time= 7.5 min

Peak Storage= 1,837 cf @ 12.27 hrs  
 Average Depth at Peak Storage= 1.48'  
 Bank-Full Depth= 3.40' Flow Area= 29.9 sf, Capacity= 83.47 cfs

2.00' x 3.40' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 15.60'  
 Length= 250.5' Slope= 0.0015 '/'  
 Inlet Invert= 57.61', Outlet Invert= 57.23'



**Reach A2-1: A2-1 Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach A2-2: A2-2 Channel**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 162.11 cfs @ 12.15 hrs, Volume= 14.244 af  
 Outflow = 160.83 cfs @ 12.18 hrs, Volume= 14.244 af, Atten= 1%, Lag= 1.8 min

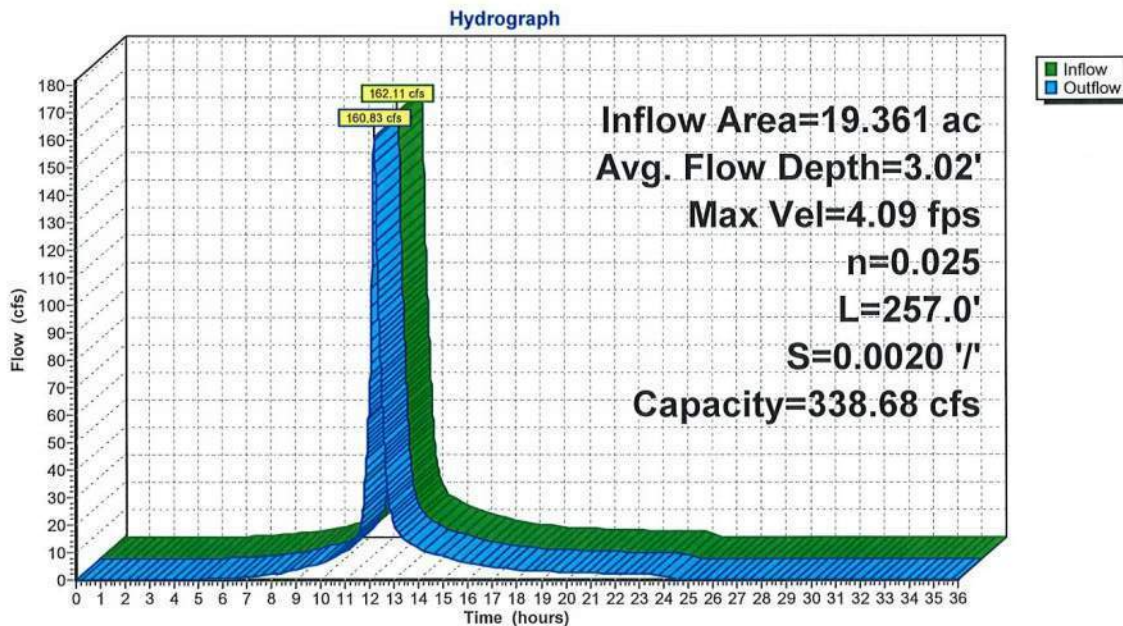
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.09 fps, Min. Travel Time= 1.0 min  
 Avg. Velocity = 1.11 fps, Avg. Travel Time= 3.9 min

Peak Storage= 10,114 cf @ 12.16 hrs  
 Average Depth at Peak Storage= 3.02'  
 Bank-Full Depth= 4.34' Flow Area= 68.1 sf, Capacity= 338.68 cfs

7.00' x 4.34' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 2.0 '/ Top Width= 24.36'  
 Length= 257.0' Slope= 0.0020 '/  
 Inlet Invert= 55.84', Outlet Invert= 55.33'



**Reach A2-2: A2-2 Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach A2-3: A2-3 Channel**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 160.83 cfs @ 12.18 hrs, Volume= 14.244 af  
 Outflow = 154.07 cfs @ 12.26 hrs, Volume= 14.244 af, Atten= 4%, Lag= 4.8 min

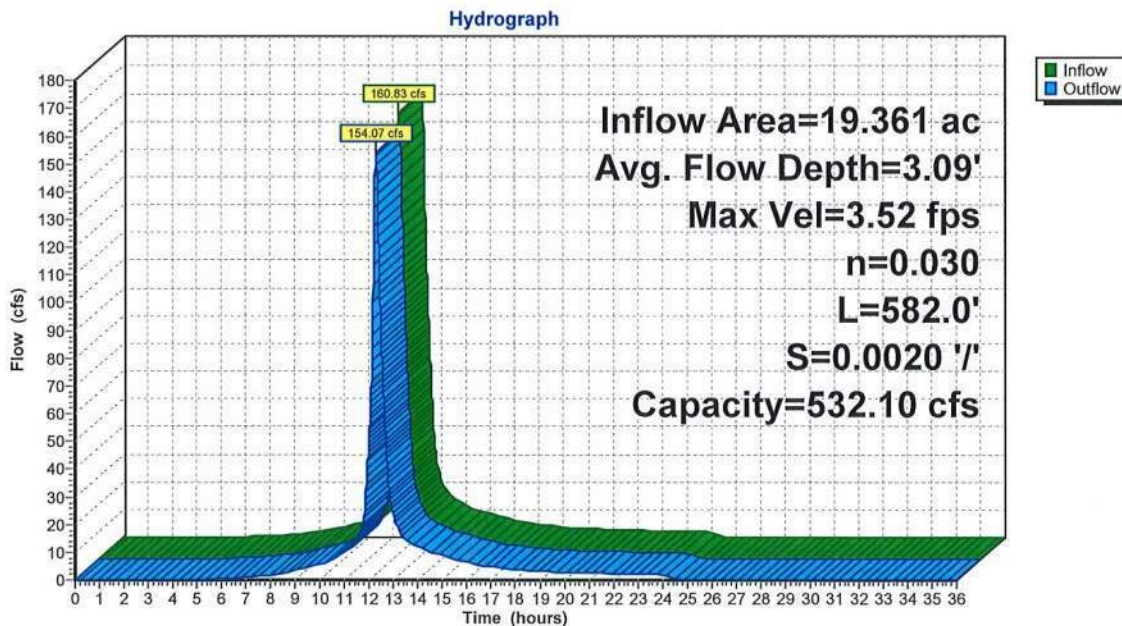
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.52 fps, Min. Travel Time= 2.8 min  
 Avg. Velocity = 0.95 fps, Avg. Travel Time= 10.2 min

Peak Storage= 25,497 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 3.09'  
 Bank-Full Depth= 5.65' Flow Area= 109.0 sf, Capacity= 532.10 cfs

8.00' x 5.65' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/ Top Width= 30.60'  
 Length= 582.0' Slope= 0.0020 '/  
 Inlet Invert= 55.33', Outlet Invert= 54.17'



**Reach A2-3: A2-3 Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach A2-4: Chute-Concrete Block Open Cell**

Inflow Area = 19.361 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 154.07 cfs @ 12.26 hrs, Volume= 14.244 af  
 Outflow = 153.86 cfs @ 12.27 hrs, Volume= 14.244 af, Atten= 0%, Lag= 0.6 min

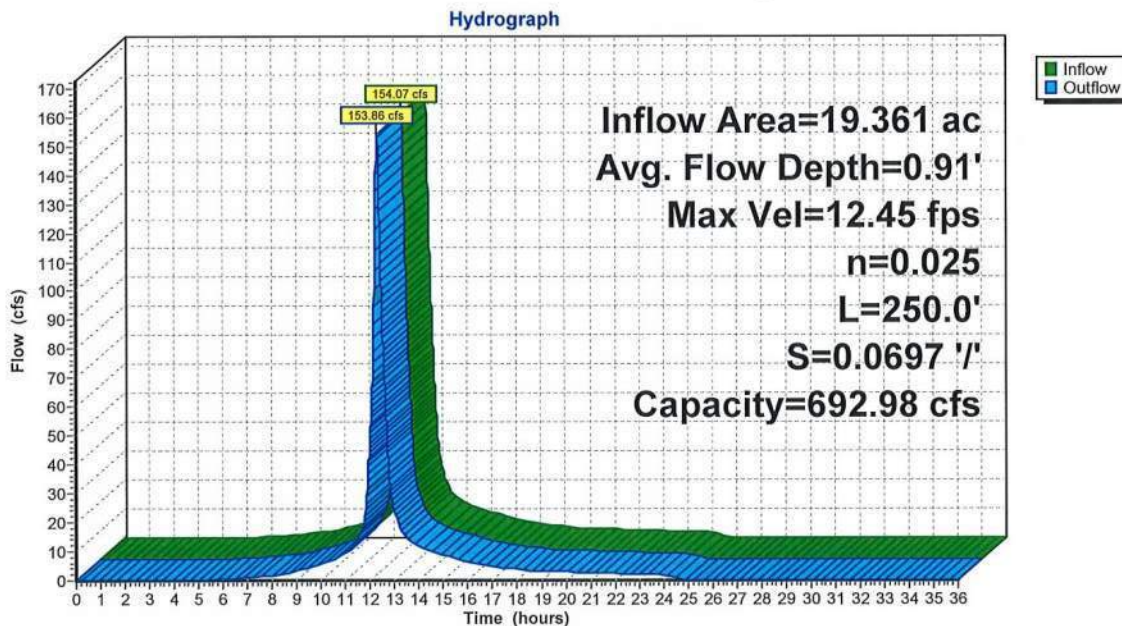
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 12.45 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity = 3.12 fps, Avg. Travel Time= 1.3 min

Peak Storage= 3,091 cf @ 12.26 hrs  
 Average Depth at Peak Storage= 0.91'  
 Bank-Full Depth= 2.00' Flow Area= 36.0 sf, Capacity= 692.98 cfs

10.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 26.00'  
 Length= 250.0' Slope= 0.0697 '/'  
 Inlet Invert= 54.17', Outlet Invert= 36.75'



**Reach A2-4: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach A2-5: Concrete Block-Channel Transition**

Inflow Area = 2.000 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 12.71 cfs @ 12.31 hrs, Volume= 1.471 af  
 Outflow = 12.71 cfs @ 12.31 hrs, Volume= 1.471 af, Atten= 0%, Lag= 0.0 min

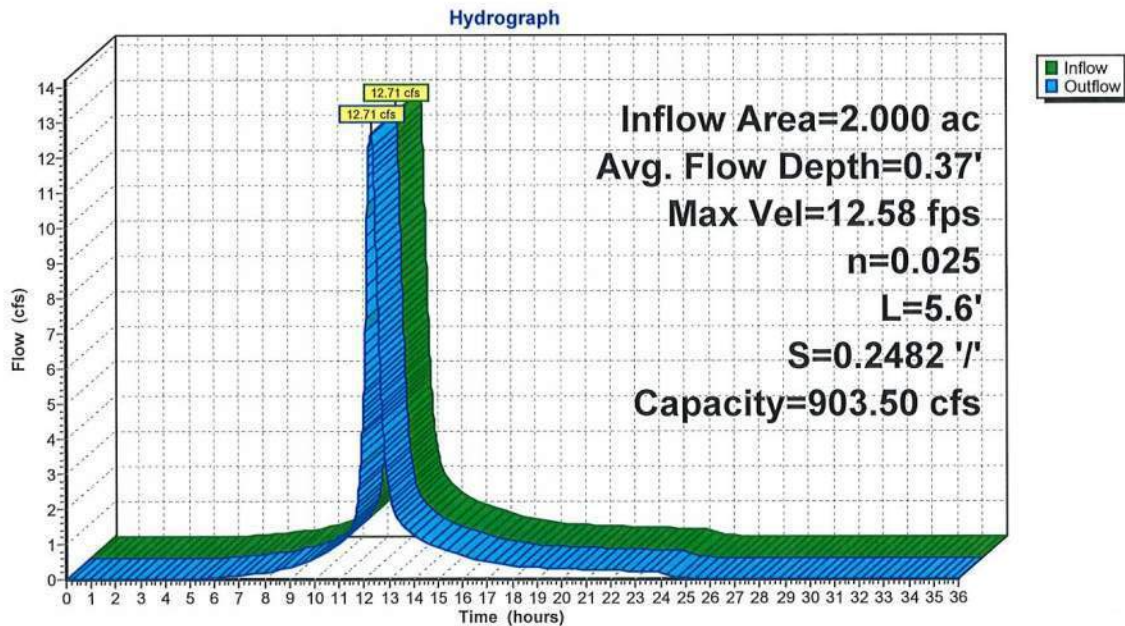
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 12.58 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 4.06 fps, Avg. Travel Time= 0.0 min

Peak Storage= 6 cf @ 12.31 hrs  
 Average Depth at Peak Storage= 0.37'  
 Bank-Full Depth= 2.93' Flow Area= 23.0 sf, Capacity= 903.50 cfs

2.00' x 2.93' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 2.0 '/' Top Width= 13.72'  
 Length= 5.6' Slope= 0.2482 '/'  
 Inlet Invert= 57.23', Outlet Invert= 55.84'



**Reach A2-5: Concrete Block-Channel Transition**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach B1: 5' x 4' Box Culvert**

Inflow Area = 19.249 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 146.99 cfs @ 12.17 hrs, Volume= 14.162 af  
 Outflow = 146.52 cfs @ 12.19 hrs, Volume= 14.162 af, Atten= 0%, Lag= 1.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 10.42 fps, Min. Travel Time= 0.7 min  
 Avg. Velocity = 2.94 fps, Avg. Travel Time= 2.6 min

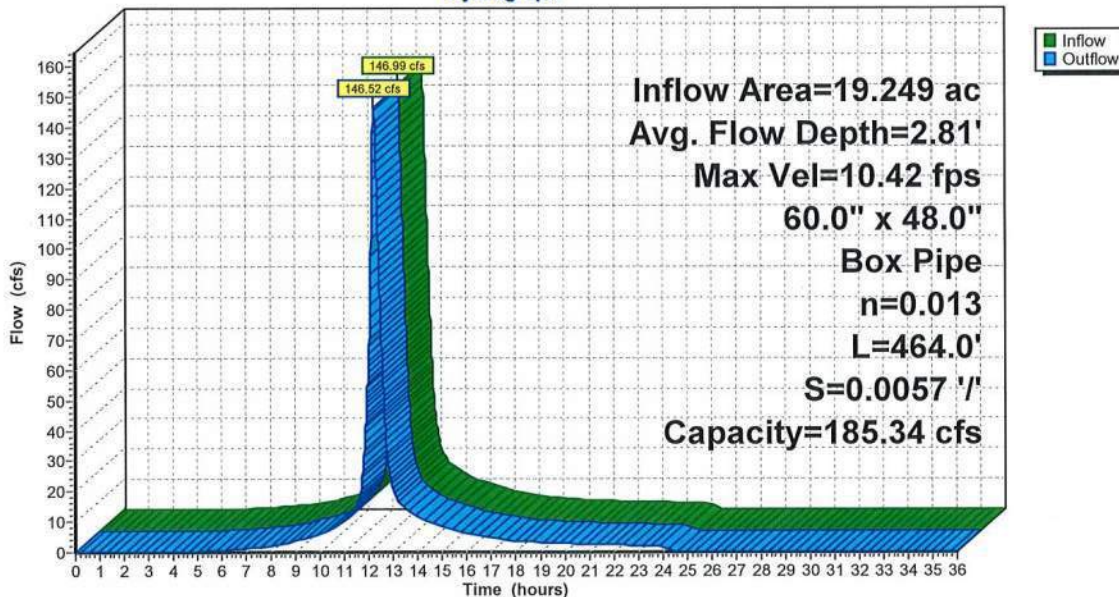
Peak Storage= 6,530 cf @ 12.18 hrs  
 Average Depth at Peak Storage= 2.81'  
 Bank-Full Depth= 4.00' Flow Area= 20.0 sf, Capacity= 185.34 cfs

60.0" W x 48.0" H Box Pipe  
 n= 0.013 Concrete pipe, bends & connections  
 Length= 464.0' Slope= 0.0057 '/'  
 Inlet Invert= 56.54', Outlet Invert= 53.89'



**Reach B1: 5' x 4' Box Culvert**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach B2: 5' x 4' Box Culvert**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 300.25 cfs @ 12.20 hrs, Volume= 27.992 af  
 Outflow = 300.01 cfs @ 12.20 hrs, Volume= 27.992 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.22 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 5.48 fps, Avg. Travel Time= 0.6 min

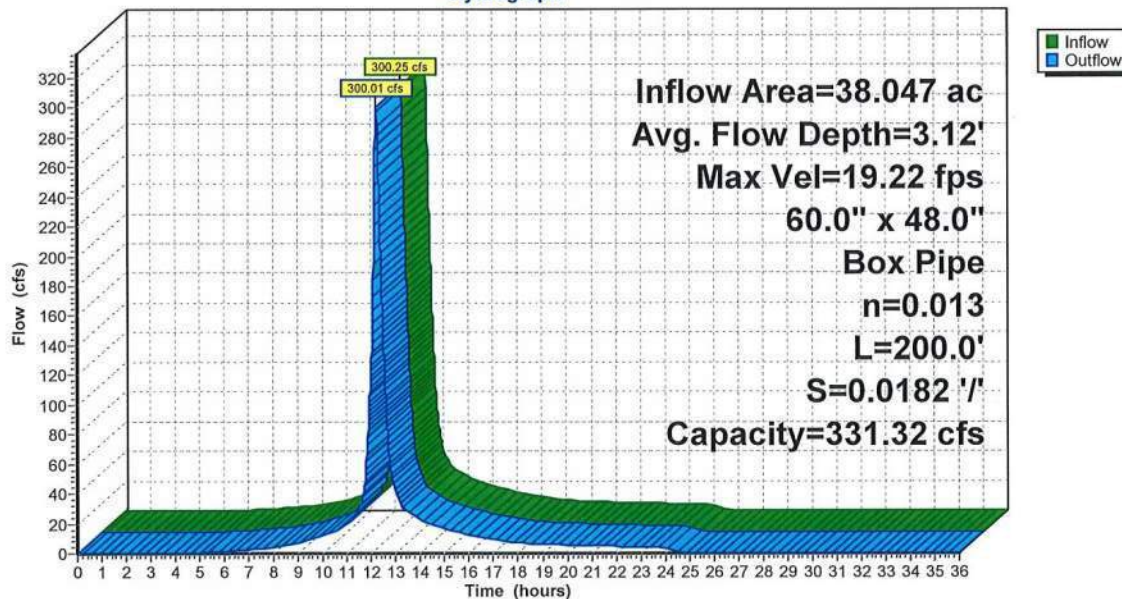
Peak Storage= 3,124 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 3.12'  
 Bank-Full Depth= 4.00' Flow Area= 20.0 sf, Capacity= 331.32 cfs

60.0" W x 48.0" H Box Pipe  
 n= 0.013 Concrete pipe, bends & connections  
 Length= 200.0' Slope= 0.0182 '/'  
 Inlet Invert= 53.45', Outlet Invert= 49.80'



**Reach B2: 5' x 4' Box Culvert**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C1-4: Chute-Concrete Block Open Cell**

Inflow Area = 38.047 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 300.01 cfs @ 12.20 hrs, Volume= 27.992 af  
 Outflow = 299.94 cfs @ 12.20 hrs, Volume= 27.992 af, Atten= 0%, Lag= 0.1 min

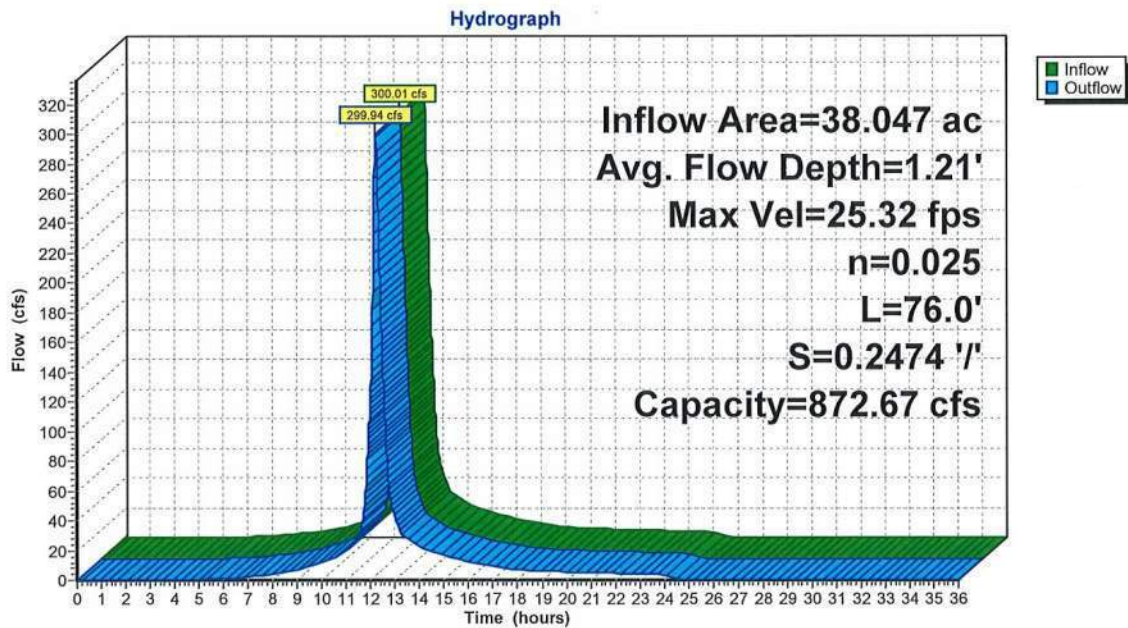
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 25.32 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 7.50 fps, Avg. Travel Time= 0.2 min

Peak Storage= 900 cf @ 12.20 hrs  
 Average Depth at Peak Storage= 1.21'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 872.67 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 76.0' Slope= 0.2474 '/'  
 Inlet Invert= 49.80', Outlet Invert= 31.00'



**Reach C1-4: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C1SCCN1: C1SCCN1 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af  
 Outflow = 2.06 cfs @ 12.23 hrs, Volume= 0.184 af, Atten= 6%, Lag= 5.8 min

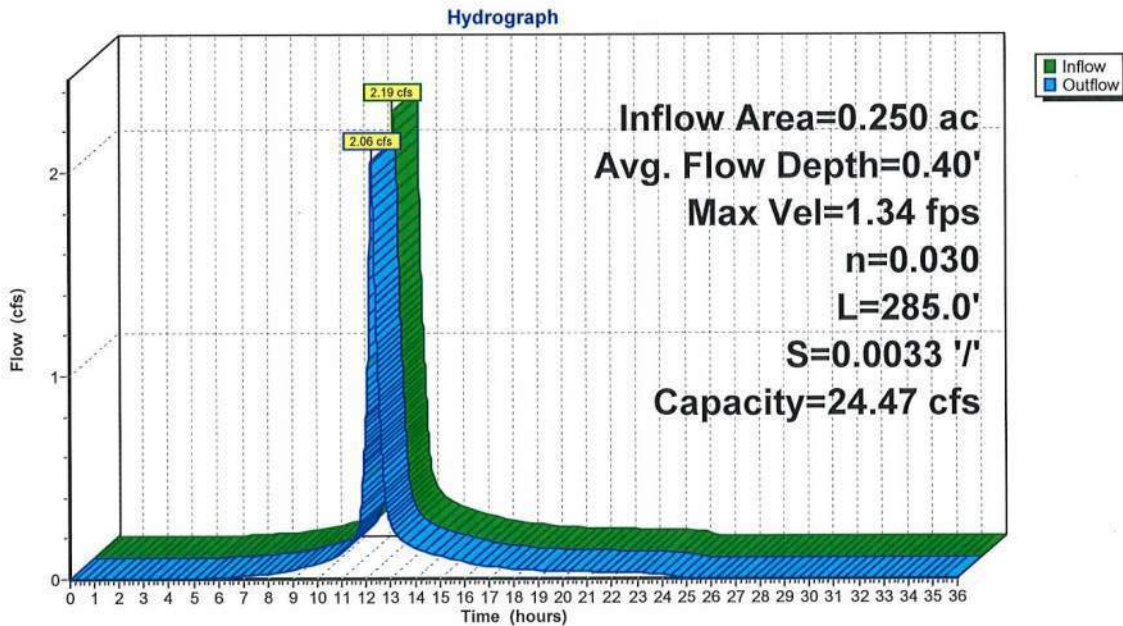
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.34 fps, Min. Travel Time= 3.5 min  
 Avg. Velocity = 0.36 fps, Avg. Travel Time= 13.0 min

Peak Storage= 439 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 0.40'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.47 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 9.00'  
 Length= 285.0' Slope= 0.0033 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.55'



**Reach C1SCCN1: C1SCCN1 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C1SCCN2: C1SCCN2 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af  
 Outflow = 2.06 cfs @ 12.23 hrs, Volume= 0.184 af, Atten= 6%, Lag= 5.9 min

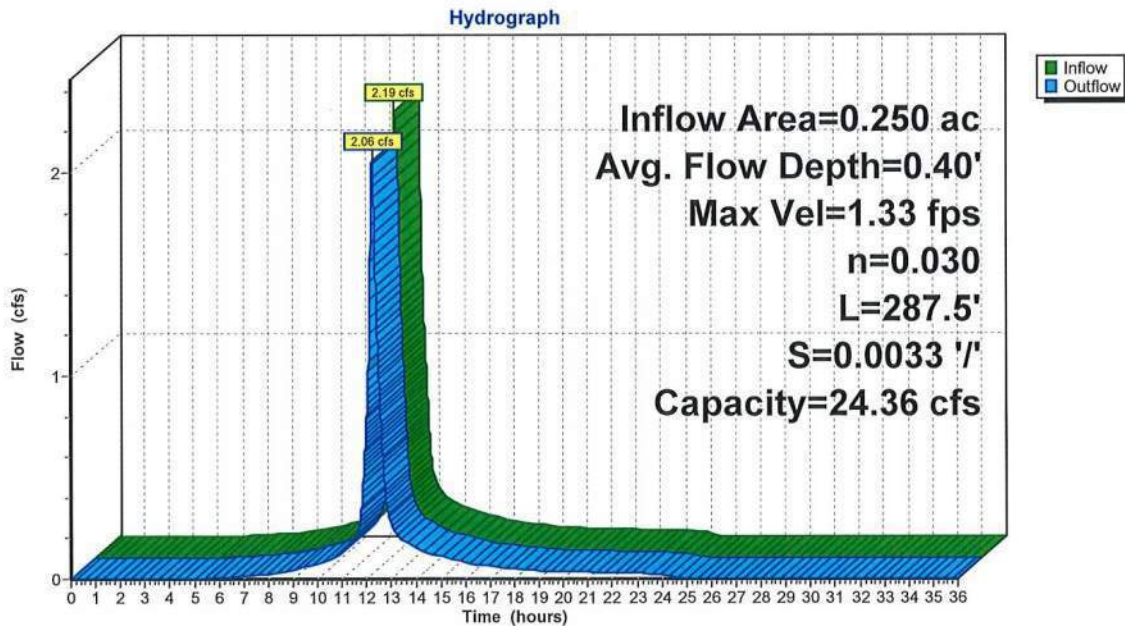
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.33 fps, Min. Travel Time= 3.6 min  
 Avg. Velocity = 0.36 fps, Avg. Travel Time= 13.2 min

Peak Storage= 443 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 0.40'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.36 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' Top Width= 9.00'  
 Length= 287.5' Slope= 0.0033 '/'  
 Inlet Invert= 58.50', Outlet Invert= 57.55'



**Reach C1SCCN2: C1SCCN2 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C1SCCS1: C1SCCS1 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af  
 Outflow = 2.06 cfs @ 12.23 hrs, Volume= 0.184 af, Atten= 6%, Lag= 5.8 min

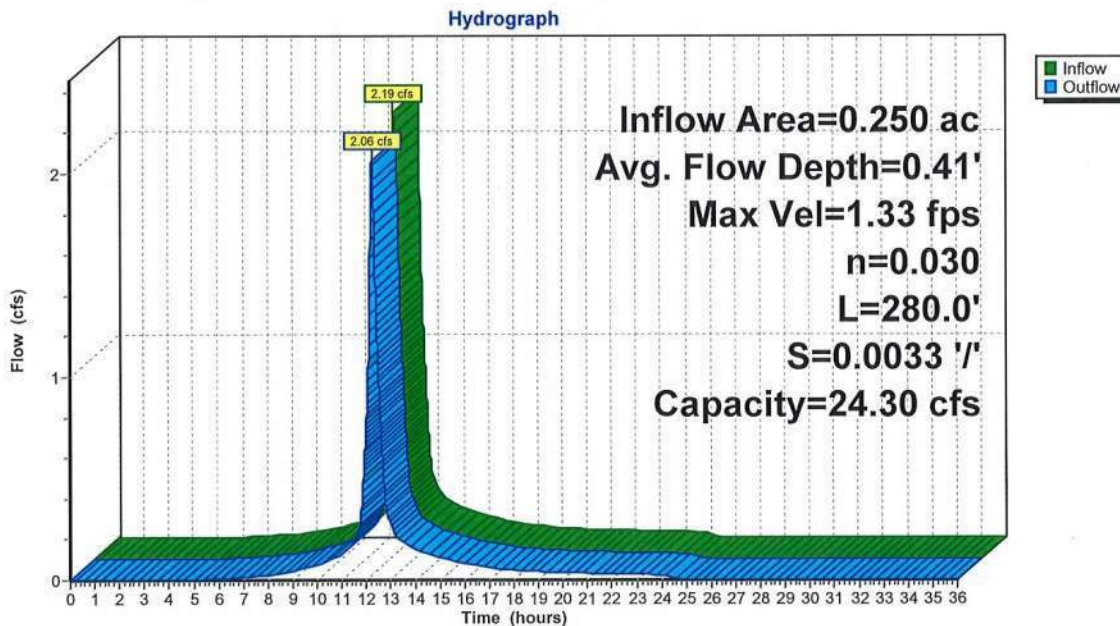
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.33 fps, Min. Travel Time= 3.5 min  
 Avg. Velocity = 0.36 fps, Avg. Travel Time= 12.9 min

Peak Storage= 433 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 0.41'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.30 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 9.00'  
 Length= 280.0' Slope= 0.0033 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.58'



**Reach C1SCCS1: C1SCCS1 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C1SCCS2: C1SCCS2 Collector Channel**

Inflow Area = 0.250 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 2.19 cfs @ 12.14 hrs, Volume= 0.184 af  
 Outflow = 2.06 cfs @ 12.23 hrs, Volume= 0.184 af, Atten= 6%, Lag= 5.8 min

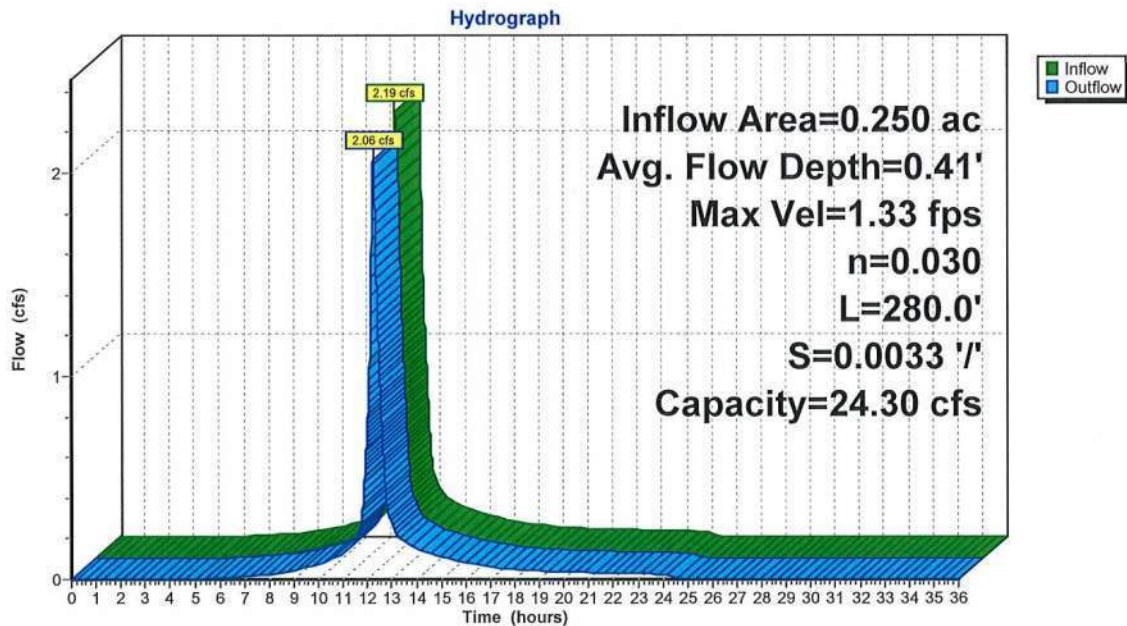
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.33 fps, Min. Travel Time= 3.5 min  
 Avg. Velocity = 0.36 fps, Avg. Travel Time= 12.9 min

Peak Storage= 433 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 0.41'  
 Bank-Full Depth= 1.50' Flow Area= 9.0 sf, Capacity= 24.30 cfs

3.00' x 1.50' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 ' / ' Top Width= 9.00'  
 Length= 280.0' Slope= 0.0033 ' / '  
 Inlet Invert= 58.50', Outlet Invert= 57.58'



**Reach C1SCCS2: C1SCCS2 Collector Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C2-3: C2-3 Channel**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 129.45 cfs @ 12.16 hrs, Volume= 11.247 af  
 Outflow = 118.51 cfs @ 12.28 hrs, Volume= 11.247 af, Atten= 8%, Lag= 7.4 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.35 fps, Min. Travel Time= 4.4 min  
 Avg. Velocity = 0.96 fps, Avg. Travel Time= 15.3 min

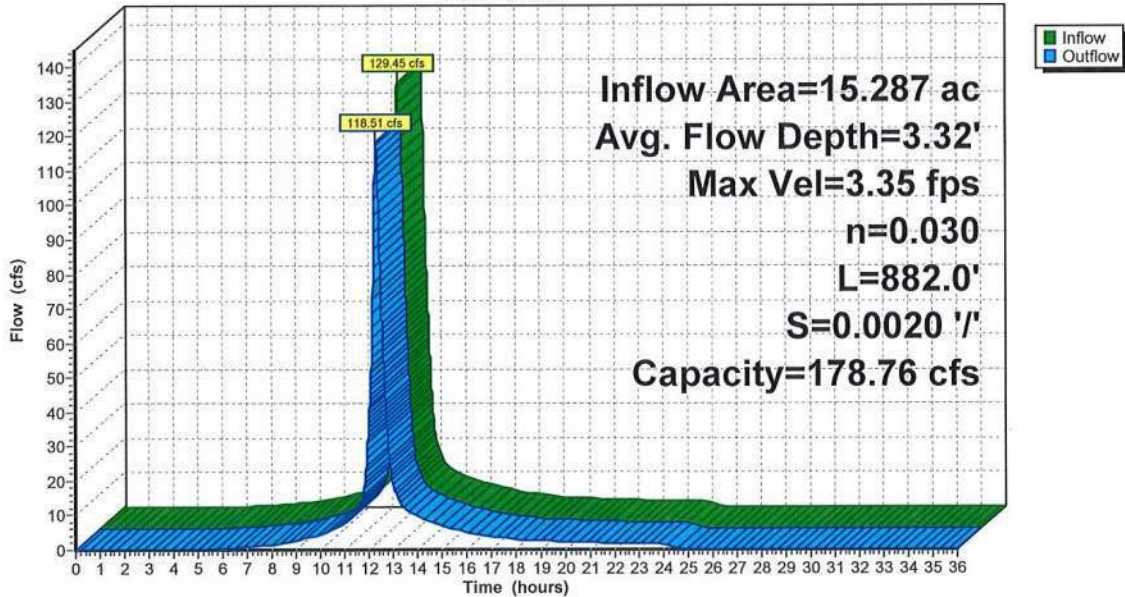
Peak Storage= 31,176 cf @ 12.21 hrs  
 Average Depth at Peak Storage= 3.32'  
 Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 178.76 cfs

4.00' x 4.00' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 2.0 '/' Top Width= 20.00'  
 Length= 882.0' Slope= 0.0020 '/'  
 Inlet Invert= 53.50', Outlet Invert= 51.75'



**Reach C2-3: C2-3 Channel**

**Hydrograph**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C2-4: Chute-Concrete Block Open Cell**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 118.38 cfs @ 12.29 hrs, Volume= 11.247 af  
 Outflow = 118.36 cfs @ 12.29 hrs, Volume= 11.247 af, Atten= 0%, Lag= 0.1 min

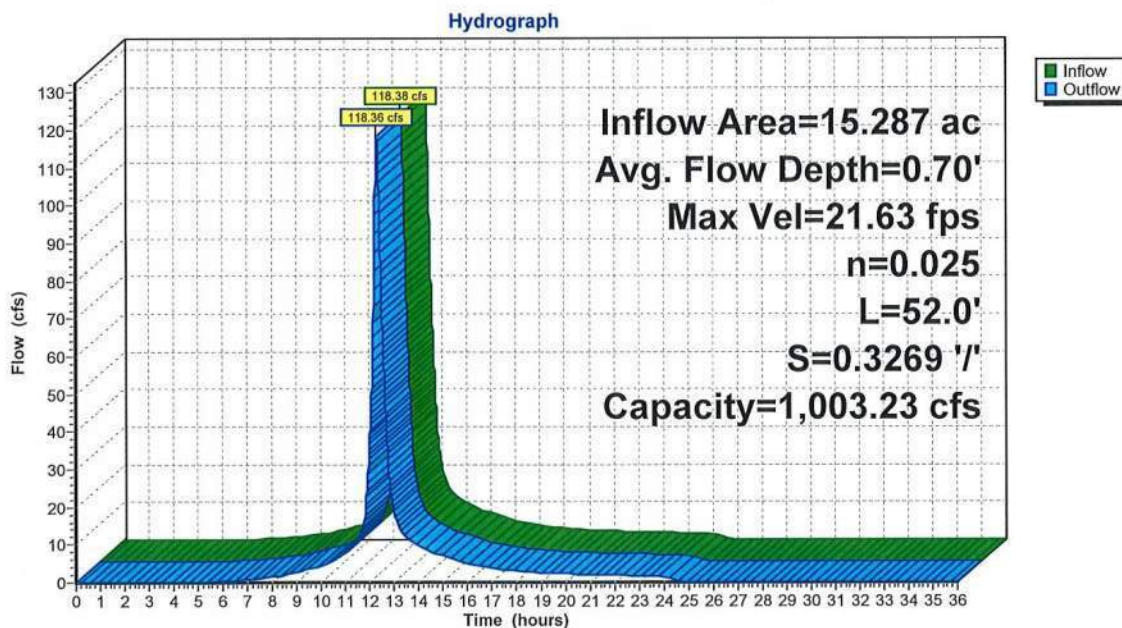
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 21.63 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity= 5.92 fps, Avg. Travel Time= 0.1 min

Peak Storage= 285 cf @ 12.29 hrs  
 Average Depth at Peak Storage= 0.70'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 1,003.23 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 52.0' Slope= 0.3269 '/'  
 Inlet Invert= 48.00', Outlet Invert= 31.00'



**Reach C2-4: Chute-Concrete Block Open Cell**





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach C2-5: C2-5 Channel**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 118.48 cfs @ 12.28 hrs, Volume= 11.247 af  
 Outflow = 118.38 cfs @ 12.29 hrs, Volume= 11.247 af, Atten= 0%, Lag= 0.3 min

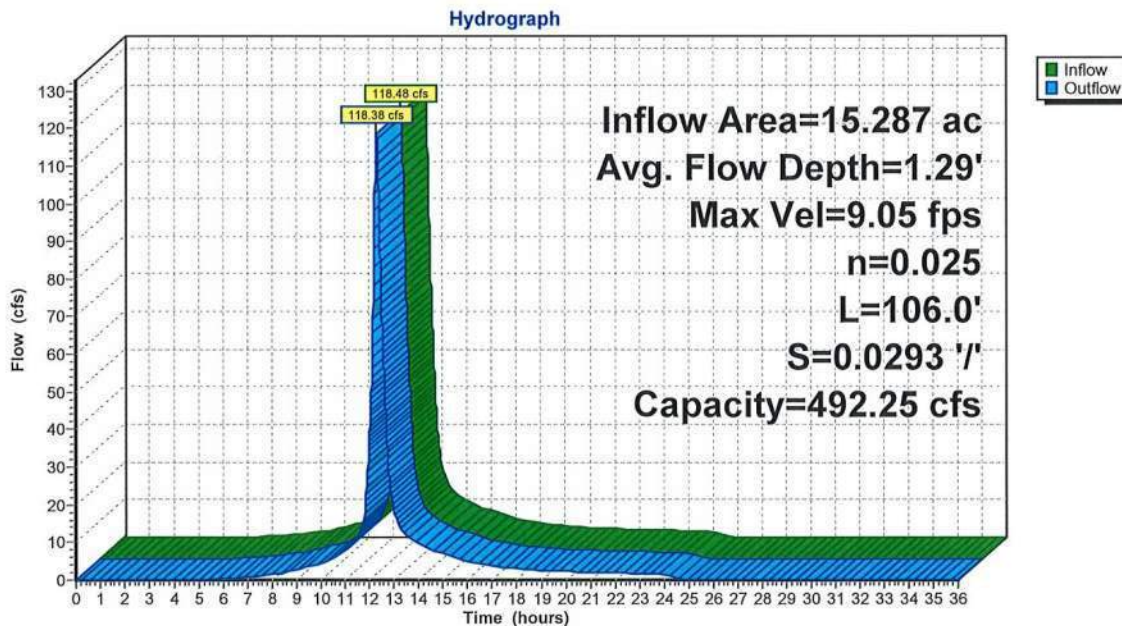
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 9.05 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 2.55 fps, Avg. Travel Time= 0.7 min

Peak Storage= 1,388 cf @ 12.28 hrs  
 Average Depth at Peak Storage= 1.29'  
 Bank-Full Depth= 2.50' Flow Area= 37.5 sf, Capacity= 492.25 cfs

5.00' x 2.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 25.00'  
 Length= 106.0' Slope= 0.0293 '/'  
 Inlet Invert= 51.11', Outlet Invert= 48.00'



**Reach C2-5: C2-5 Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach CC: Chute-Concrete Block Open Cell**

Inflow Area = 1.480 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 11.11 cfs @ 12.30 hrs, Volume= 1.089 af  
 Outflow = 11.10 cfs @ 12.31 hrs, Volume= 1.089 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.99 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 2.01 fps, Avg. Travel Time= 1.3 min

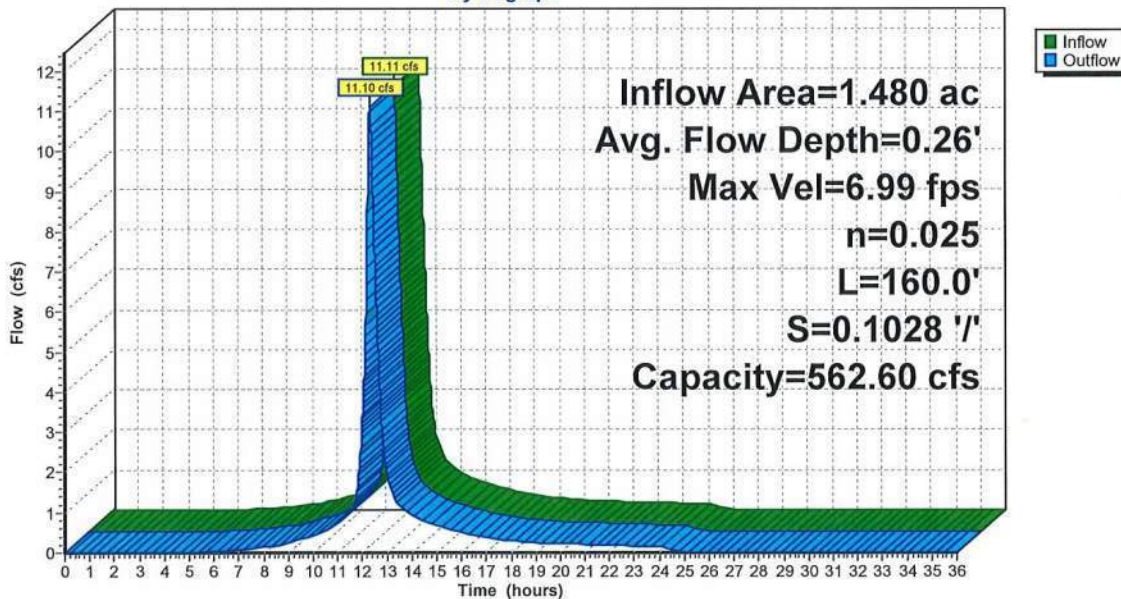
Peak Storage= 254 cf @ 12.31 hrs  
 Average Depth at Peak Storage= 0.26'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 562.60 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 160.0' Slope= 0.1028 ' / '  
 Inlet Invert= 53.20', Outlet Invert= 36.75'



**Reach CC: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach E: Chute-Concrete Block Open Cell**

Inflow Area = 17.798 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 150.87 cfs @ 12.14 hrs, Volume= 13.094 af  
 Outflow = 150.58 cfs @ 12.16 hrs, Volume= 13.094 af, Atten= 0%, Lag= 0.6 min

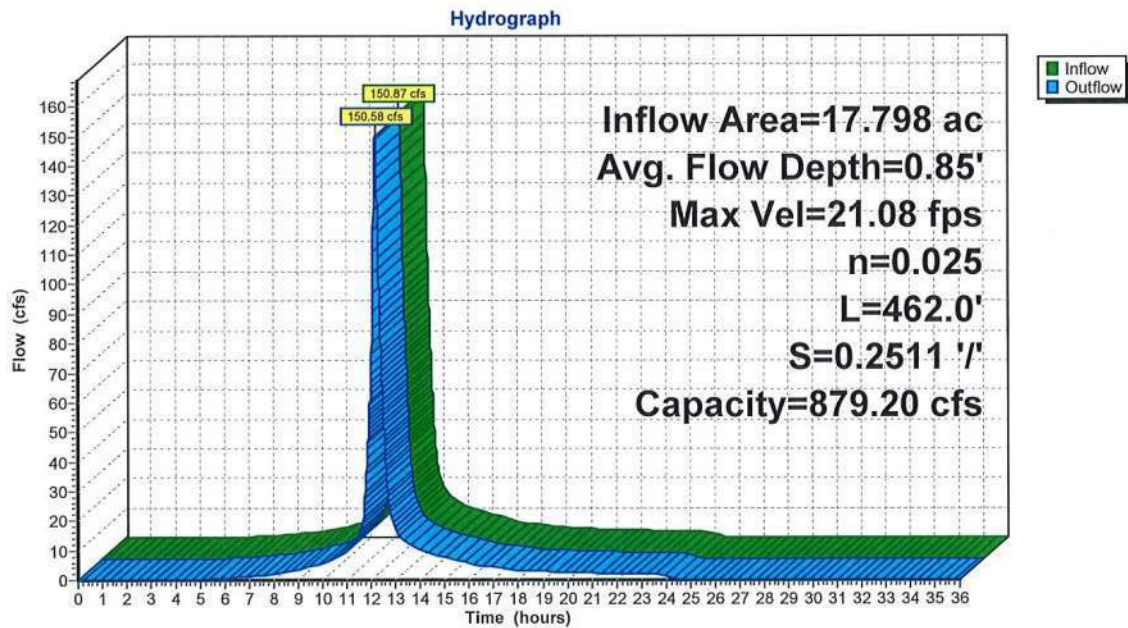
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 21.08 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 6.60 fps, Avg. Travel Time= 1.2 min

Peak Storage= 3,305 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.85'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 879.20 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 462.0' Slope= 0.2511 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach E: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach NE: Chute-Concrete Block Open Cell**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 129.70 cfs @ 12.14 hrs, Volume= 11.247 af  
 Outflow = 129.45 cfs @ 12.16 hrs, Volume= 11.247 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 20.16 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 6.26 fps, Avg. Travel Time= 1.2 min

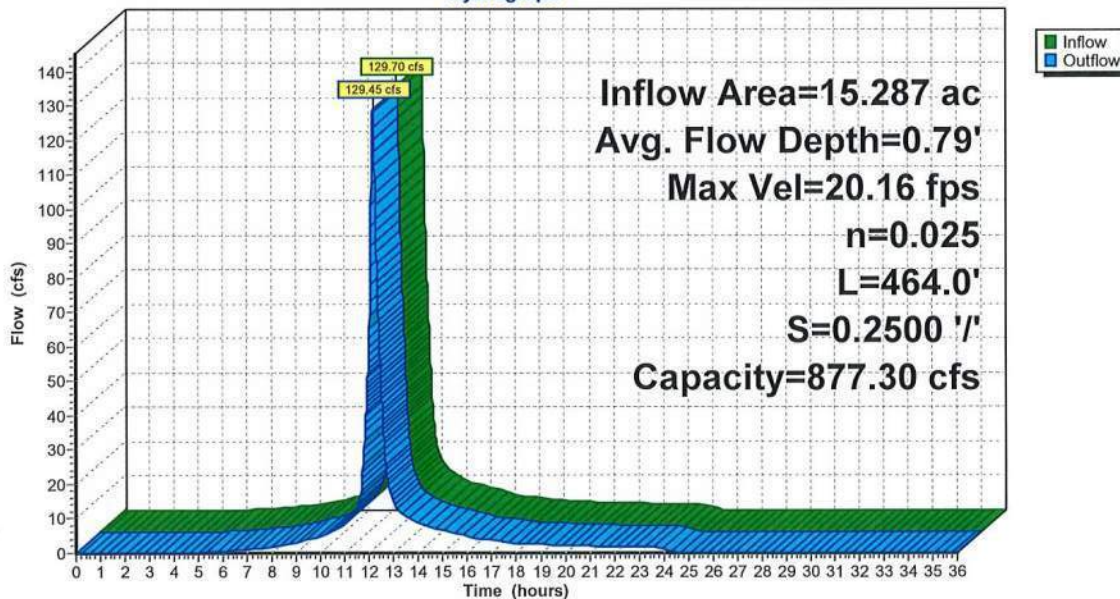
Peak Storage= 2,982 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.79'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach NE: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach NW: Chute-Concrete Block Open Cell**

Inflow Area = 13.115 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 109.40 cfs @ 12.15 hrs, Volume= 9.649 af  
 Outflow = 109.21 cfs @ 12.16 hrs, Volume= 9.649 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.21 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 5.93 fps, Avg. Travel Time= 1.3 min

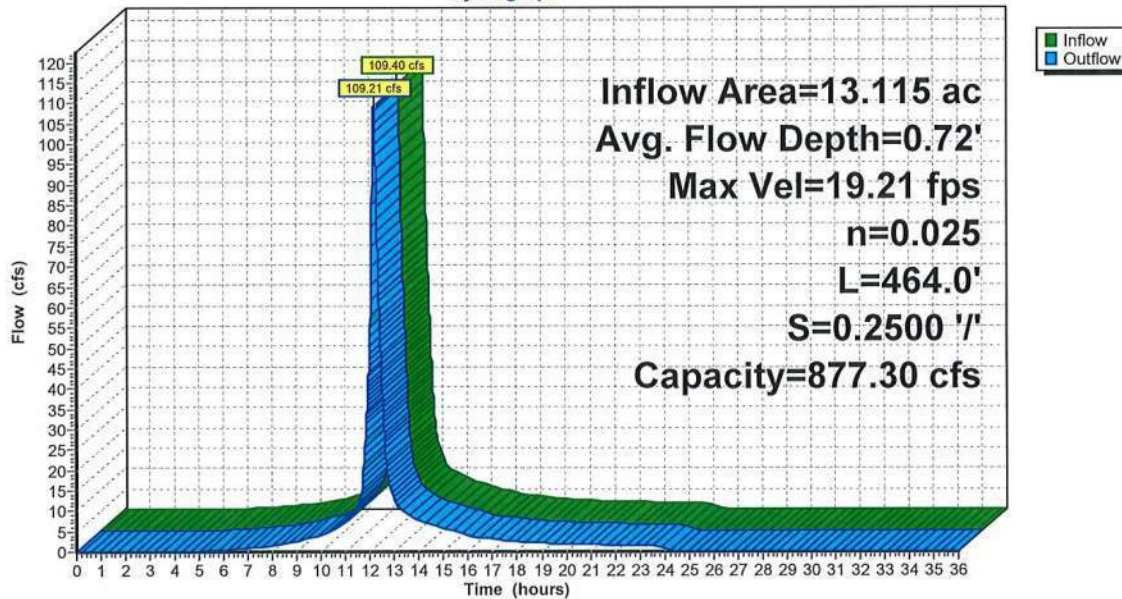
Peak Storage= 2,640 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.72'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach NW: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach OC: Existing Offsite Channel**

Inflow Area = 42.338 ac, 0.00% Impervious, Inflow Depth > 8.85" for 100-Year event  
 Inflow = 42.26 cfs @ 12.98 hrs, Volume= 31.217 af  
 Outflow = 41.59 cfs @ 14.06 hrs, Volume= 31.108 af, Atten= 2%, Lag= 64.9 min

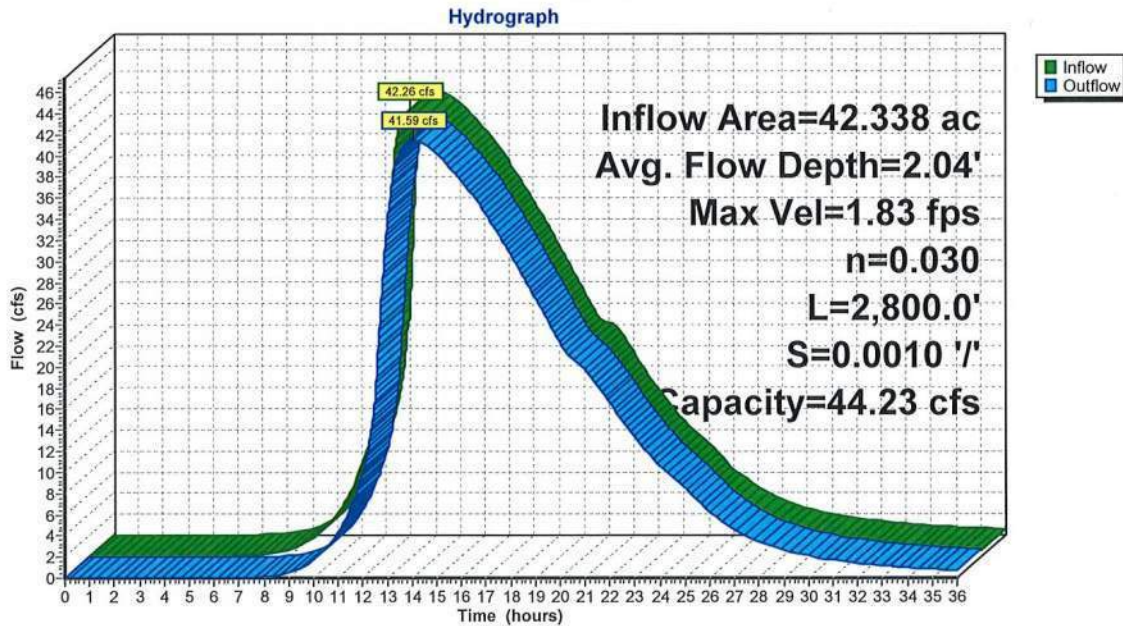
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 1.83 fps, Min. Travel Time= 25.4 min  
 Avg. Velocity= 0.95 fps, Avg. Travel Time= 49.3 min

Peak Storage= 63,491 cf @ 13.64 hrs  
 Average Depth at Peak Storage= 2.04'  
 Bank-Full Depth= 2.10' Flow Area= 23.7 sf, Capacity= 44.23 cfs

5.00' x 2.10' deep channel, n= 0.030 Earth, grassed & winding  
 Side Slope Z-value= 3.0 '/' Top Width= 17.60'  
 Length= 2,800.0' Slope= 0.0010 '/'  
 Inlet Invert= 46.66', Outlet Invert= 43.86'



**Reach OC: Existing Offsite Channel**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach P1: Culvert**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 118.51 cfs @ 12.28 hrs, Volume= 11.247 af  
 Outflow = 118.48 cfs @ 12.28 hrs, Volume= 11.247 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 14.61 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity= 4.39 fps, Avg. Travel Time= 0.2 min

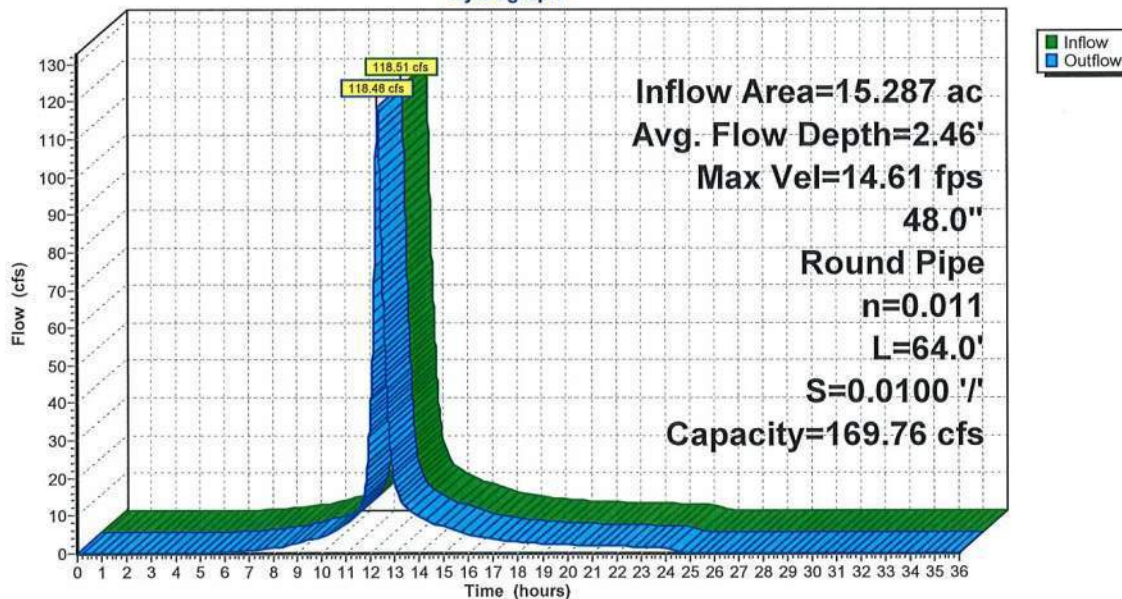
Peak Storage= 519 cf @ 12.28 hrs  
 Average Depth at Peak Storage= 2.46'  
 Bank-Full Depth= 4.00' Flow Area= 12.6 sf, Capacity= 169.76 cfs

48.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 64.0' Slope= 0.0100 '/'  
 Inlet Invert= 51.75', Outlet Invert= 51.11'



**Reach P1: Culvert**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach P2: Culvert**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 4.12 cfs @ 12.23 hrs, Volume= 0.368 af  
 Outflow = 4.11 cfs @ 12.24 hrs, Volume= 0.368 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.31 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity= 2.37 fps, Avg. Travel Time= 0.5 min

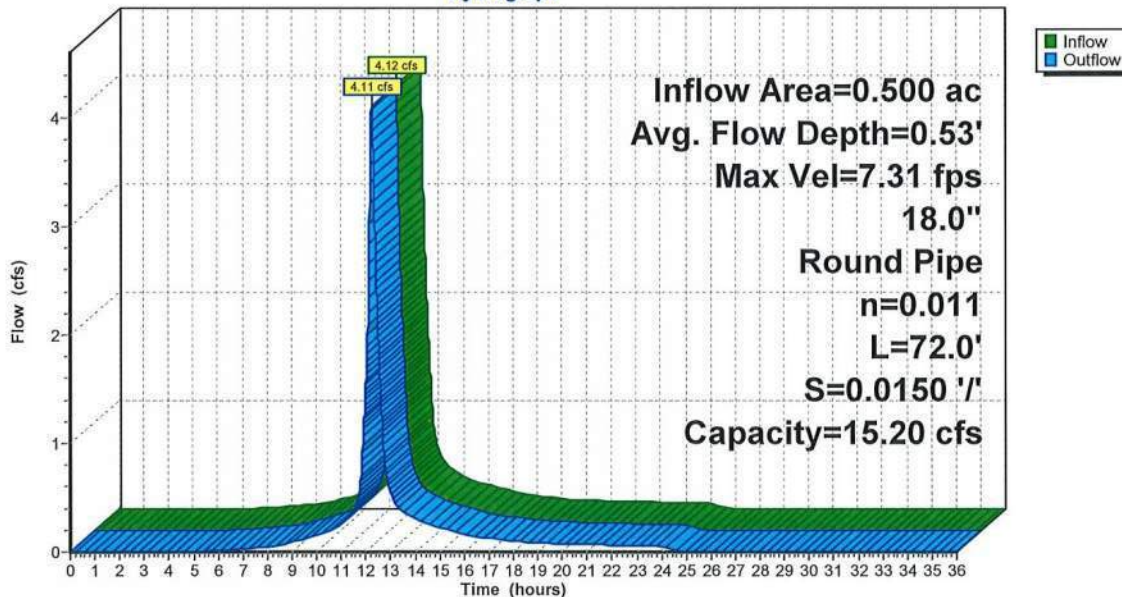
Peak Storage= 41 cf @ 12.24 hrs  
 Average Depth at Peak Storage= 0.53'  
 Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.20 cfs

18.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 72.0' Slope= 0.0150 '/'  
 Inlet Invert= 54.39', Outlet Invert= 53.31'



**Reach P2: Culvert**

Hydrograph





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach P2-1: Chute-Concrete Block Open Cell**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 4.11 cfs @ 12.24 hrs, Volume= 0.368 af  
 Outflow = 4.11 cfs @ 12.24 hrs, Volume= 0.368 af, Atten= 0%, Lag= 0.2 min

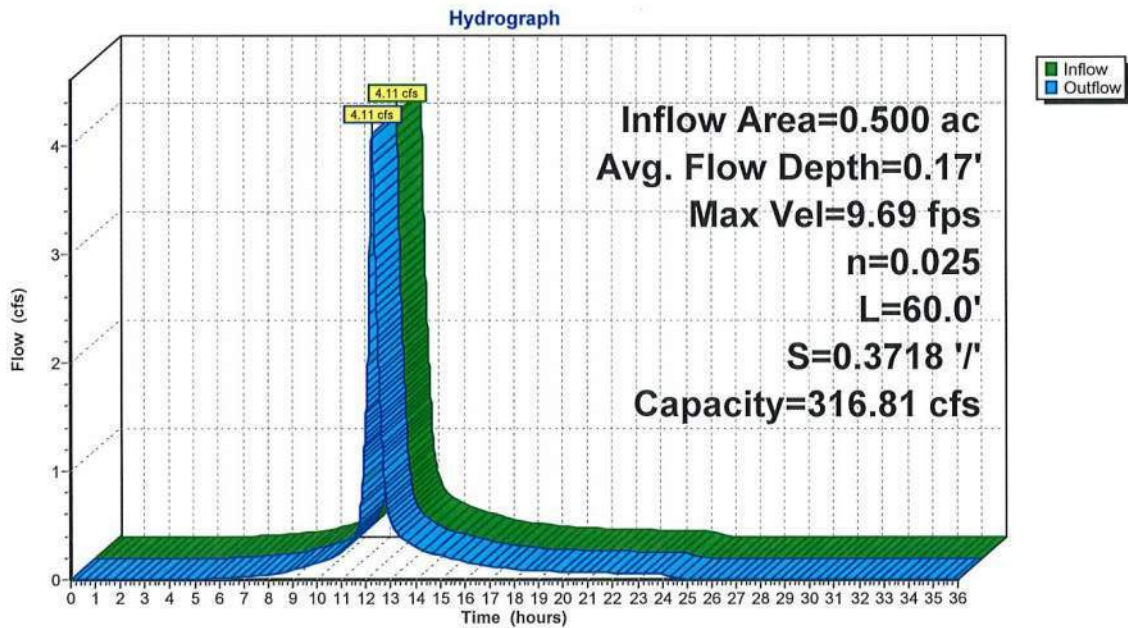
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 9.69 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.91 fps, Avg. Travel Time= 0.3 min

Peak Storage= 25 cf @ 12.24 hrs  
 Average Depth at Peak Storage= 0.17'  
 Bank-Full Depth= 1.50' Flow Area= 9.8 sf, Capacity= 316.81 cfs

2.00' x 1.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 3.0 ' / ' Top Width= 11.00'  
 Length= 60.0' Slope= 0.3718 ' / '  
 Inlet Invert= 53.31', Outlet Invert= 31.00'



**Reach P2-1: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach P3: Culvert**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 4.12 cfs @ 12.23 hrs, Volume= 0.368 af  
 Outflow = 4.12 cfs @ 12.24 hrs, Volume= 0.368 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.31 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 2.38 fps, Avg. Travel Time= 0.5 min

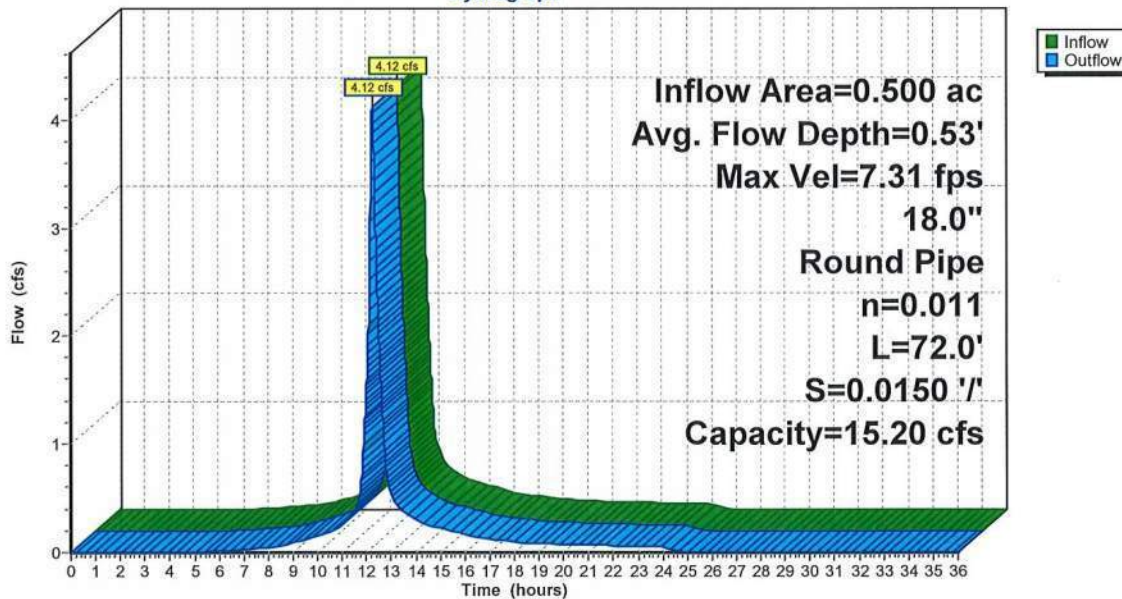
Peak Storage= 41 cf @ 12.23 hrs  
 Average Depth at Peak Storage= 0.53'  
 Bank-Full Depth= 1.50' Flow Area= 1.8 sf, Capacity= 15.20 cfs

18.0" Round Pipe  
 n= 0.011 Concrete pipe, straight & clean  
 Length= 72.0' Slope= 0.0150 '/'  
 Inlet Invert= 55.41', Outlet Invert= 54.33'



**Reach P3: Culvert**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach P3-1: Chute-Concrete Block Open Cell**

Inflow Area = 0.500 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 4.12 cfs @ 12.24 hrs, Volume= 0.368 af  
 Outflow = 4.12 cfs @ 12.24 hrs, Volume= 0.368 af, Atten= 0%, Lag= 0.2 min

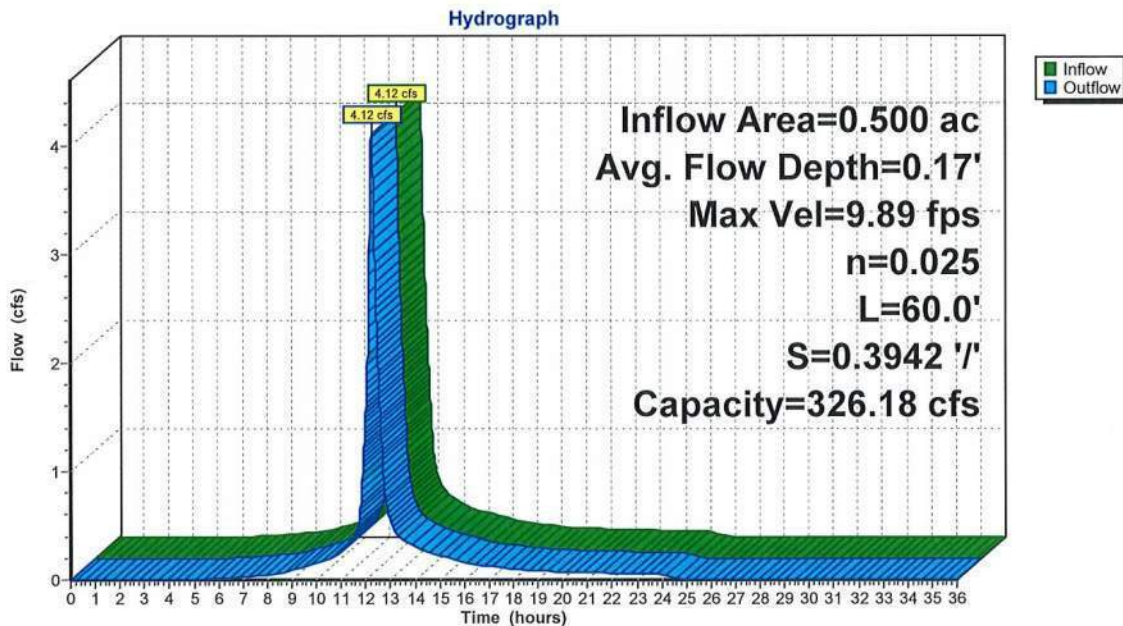
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 9.89 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity= 2.98 fps, Avg. Travel Time= 0.3 min

Peak Storage= 25 cf @ 12.24 hrs  
 Average Depth at Peak Storage= 0.17'  
 Bank-Full Depth= 1.50' Flow Area= 9.8 sf, Capacity= 326.18 cfs

2.00' x 1.50' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 3.0 '/' Top Width= 11.00'  
 Length= 60.0' Slope= 0.3942 '/'  
 Inlet Invert= 54.65', Outlet Invert= 31.00'



**Reach P3-1: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach S: Chute-Concrete Block Open Cell**

Inflow Area = 17.361 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 152.24 cfs @ 12.14 hrs, Volume= 12.773 af  
 Outflow = 151.93 cfs @ 12.15 hrs, Volume= 12.773 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 21.09 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 6.55 fps, Avg. Travel Time= 1.2 min

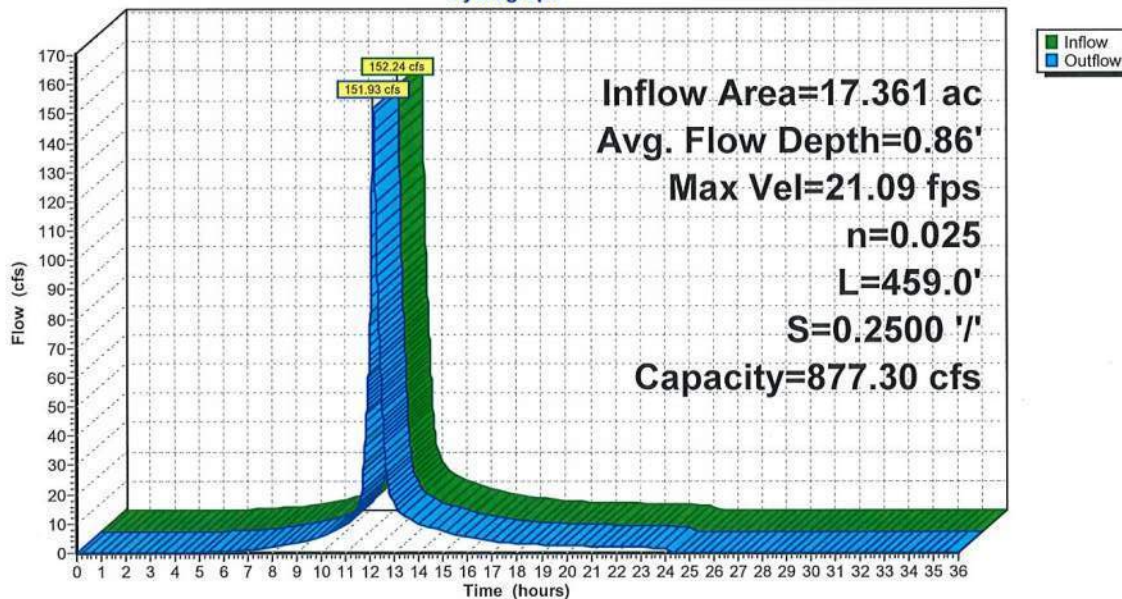
Peak Storage= 3,309 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.86'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 459.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 59.25'



**Reach S: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach SE: Chute-Concrete Block Open Cell**

Inflow Area = 18.249 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 142.28 cfs @ 12.15 hrs, Volume= 13.426 af  
 Outflow = 142.07 cfs @ 12.17 hrs, Volume= 13.426 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 20.70 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 6.61 fps, Avg. Travel Time= 1.1 min

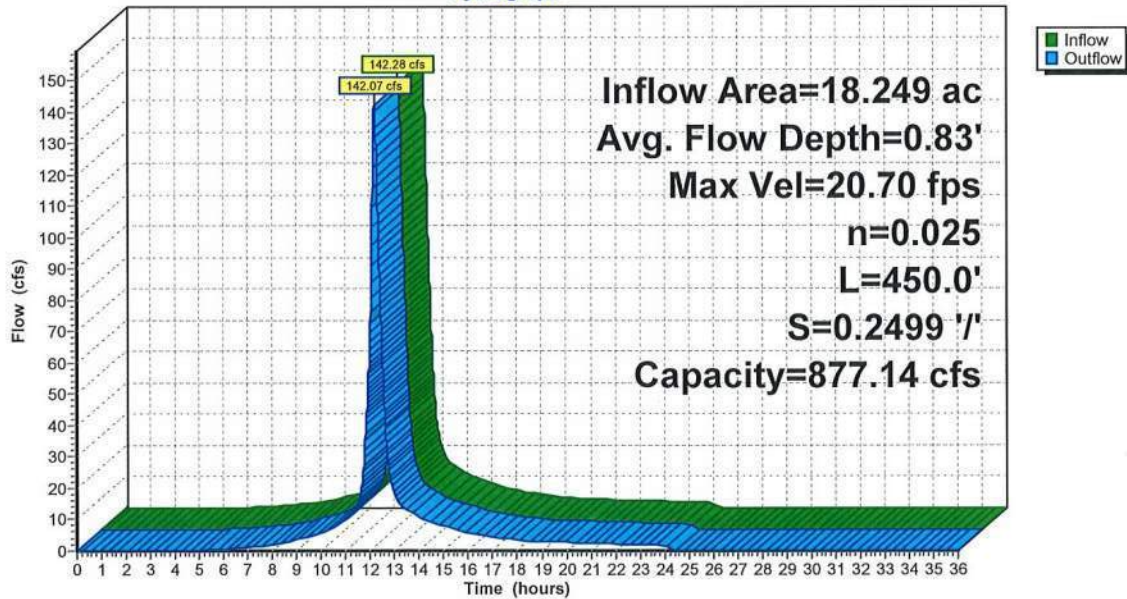
Peak Storage= 3,091 cf @ 12.16 hrs  
 Average Depth at Peak Storage= 0.83'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.14 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 450.0' Slope= 0.2499 '/'  
 Inlet Invert= 174.00', Outlet Invert= 61.54'



**Reach SE: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach SE1: Chute-Concrete Block Open Cell**

Inflow Area = 18.249 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 142.07 cfs @ 12.17 hrs, Volume= 13.426 af  
 Outflow = 142.01 cfs @ 12.17 hrs, Volume= 13.426 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 13.74 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity= 4.54 fps, Avg. Travel Time= 0.2 min

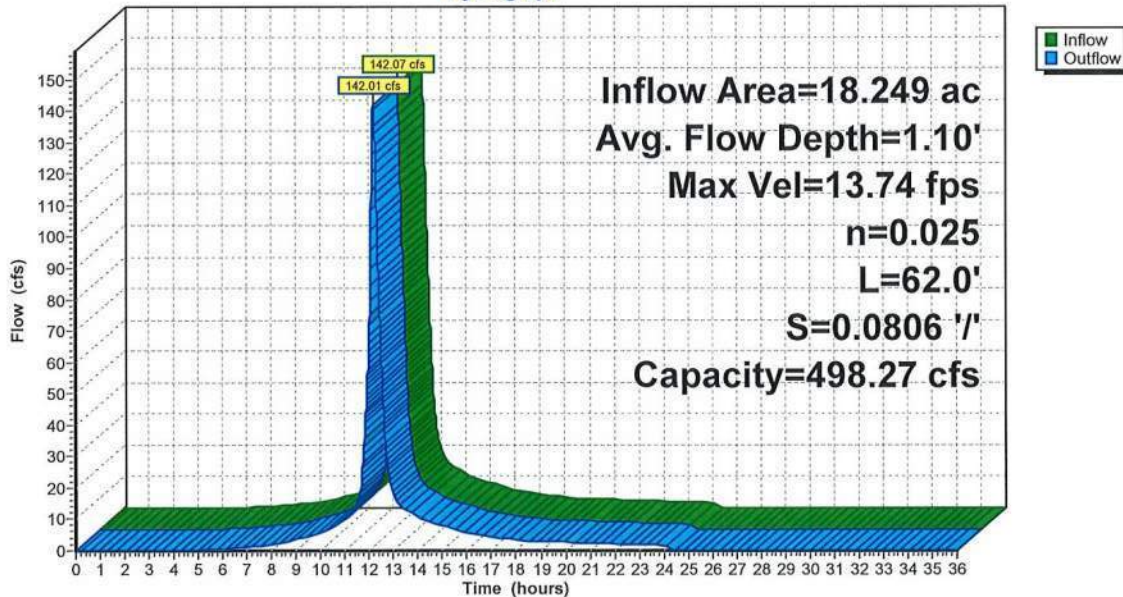
Peak Storage= 641 cf @ 12.17 hrs  
 Average Depth at Peak Storage= 1.10'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 498.27 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 62.0' Slope= 0.0806 '/'  
 Inlet Invert= 61.54', Outlet Invert= 56.54'



**Reach SE1: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach SW: Chute-Concrete Block Open Cell**

Inflow Area = 15.434 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 135.35 cfs @ 12.14 hrs, Volume= 11.355 af  
 Outflow = 135.10 cfs @ 12.14 hrs, Volume= 11.355 af, Atten= 0%, Lag= 0.5 min

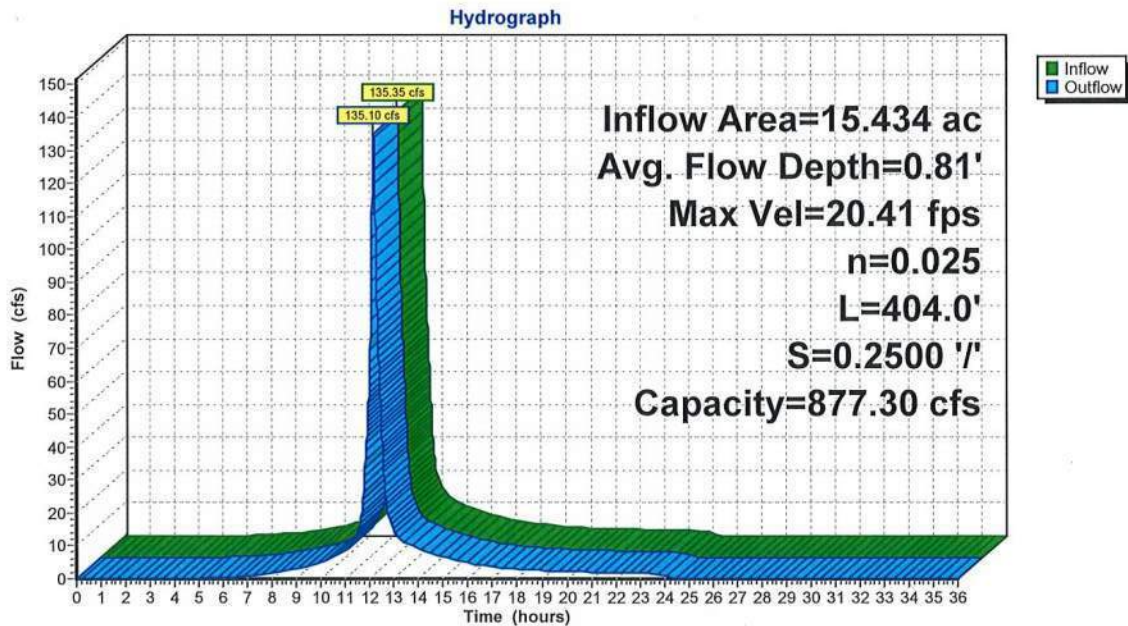
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 20.41 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity= 6.30 fps, Avg. Travel Time= 1.1 min

Peak Storage= 2,677 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.81'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 404.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 73.00'



**Reach SW: Chute-Concrete Block Open Cell**



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach SW-1: Chute-Concrete Block Open Cell**

Inflow Area = 15.434 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 135.10 cfs @ 12.14 hrs, Volume= 11.355 af  
 Outflow = 134.87 cfs @ 12.15 hrs, Volume= 11.355 af, Atten= 0%, Lag= 0.5 min

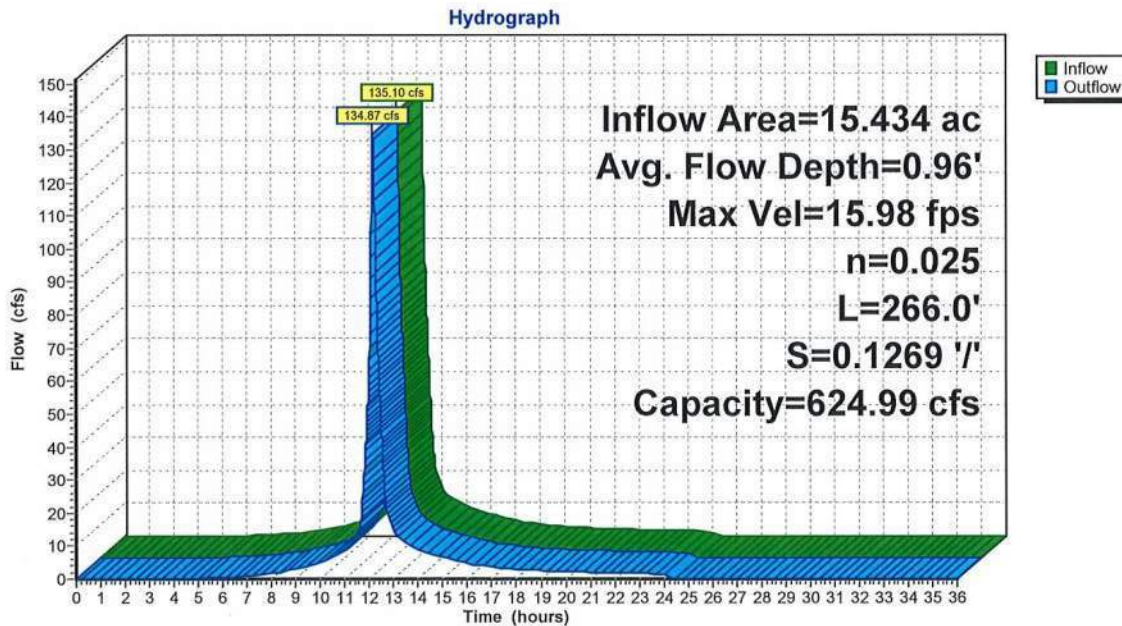
Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 15.98 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity= 5.02 fps, Avg. Travel Time= 0.9 min

Peak Storage= 2,248 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.96'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 624.99 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 266.0' Slope= 0.1269 '/'  
 Inlet Invert= 70.50', Outlet Invert= 36.75'



**Reach SW-1: Chute-Concrete Block Open Cell**





**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Reach W: Chute-Concrete Block Open Cell**

Inflow Area = 22.383 ac, 0.00% Impervious, Inflow Depth = 8.83" for 100-Year event  
 Inflow = 179.96 cfs @ 12.15 hrs, Volume= 16.468 af  
 Outflow = 179.70 cfs @ 12.16 hrs, Volume= 16.468 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 22.10 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity = 7.09 fps, Avg. Travel Time= 1.1 min

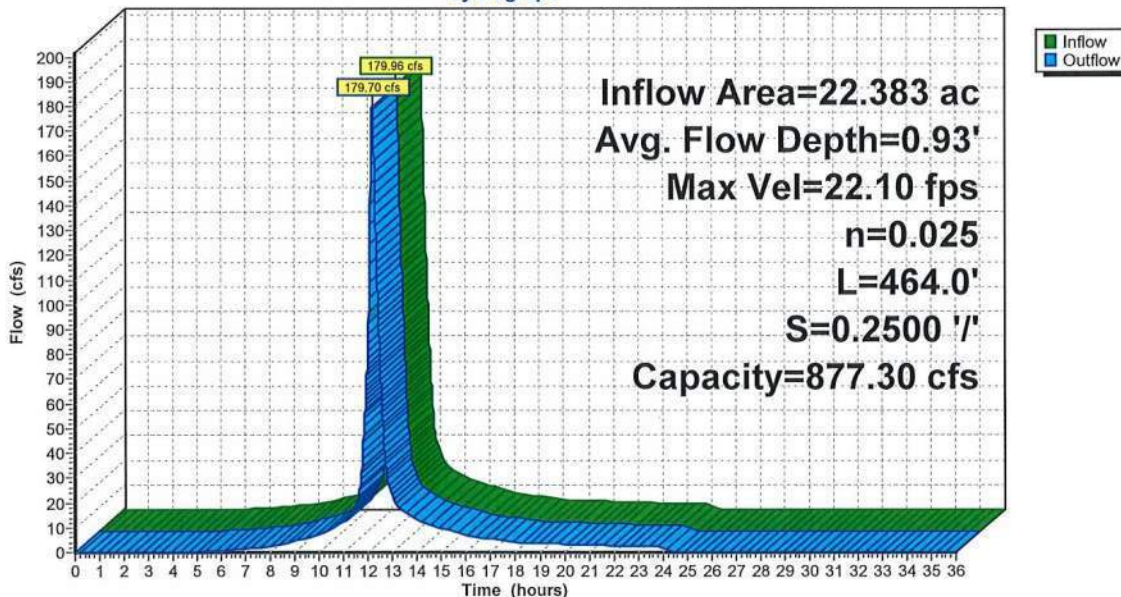
Peak Storage= 3,776 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.93'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 464.0' Slope= 0.2500 '/'  
 Inlet Invert= 174.00', Outlet Invert= 58.00'



**Reach W: Chute-Concrete Block Open Cell**

Hydrograph



**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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**Summary for Pond PA: Retention Pond A**

No Discharge. Reshaping of Existing Pond A Bottom Required.

Inflow Area = 47.697 ac, 0.00% Impervious, Inflow Depth = 9.28" for 100-Year event  
 Inflow = 324.39 cfs @ 12.21 hrs, Volume= 36.905 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 49.73' @ 36.00 hrs Surf.Area= 4.915 ac Storage= 36.905 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description		
#1	36.75'	82.379 af	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (acres)	Perim. (feet)	Inc.Store (acre-feet)	Cum.Store (acre-feet)	Wet.Area (acres)
36.75	1.340	1,049.8	0.000	0.000	1.340
37.00	1.380	1,064.9	0.340	0.340	1.399
38.00	1.540	1,125.4	1.459	1.799	1.642
39.00	1.720	1,171.5	1.629	3.428	1.837
40.00	1.890	1,216.8	1.804	5.233	2.037
41.00	2.120	1,292.5	2.004	7.237	2.385
42.00	2.360	1,370.6	2.239	9.476	2.766
43.00	2.620	1,447.9	2.489	11.964	3.166
44.00	2.900	1,537.3	2.759	14.723	3.654
45.00	3.210	1,623.3	3.054	17.777	4.152
46.00	3.550	1,699.4	3.379	21.156	4.616
47.00	3.910	1,769.6	3.729	24.884	5.062
48.00	4.270	1,832.8	4.089	28.973	5.480
49.00	4.640	1,894.6	4.454	33.426	5.903
50.00	5.020	1,956.1	4.829	38.255	6.338
51.00	5.450	2,024.3	5.234	43.489	6.836
52.00	5.860	2,075.6	5.654	49.143	7.223
53.00	6.180	2,125.3	6.019	55.162	7.608
54.00	6.490	2,167.2	6.334	61.496	7.940
55.00	6.800	2,209.1	6.644	68.141	8.279
56.00	7.120	2,250.9	6.959	75.100	8.623
57.00	7.440	2,292.6	7.279	82.379	8.973

**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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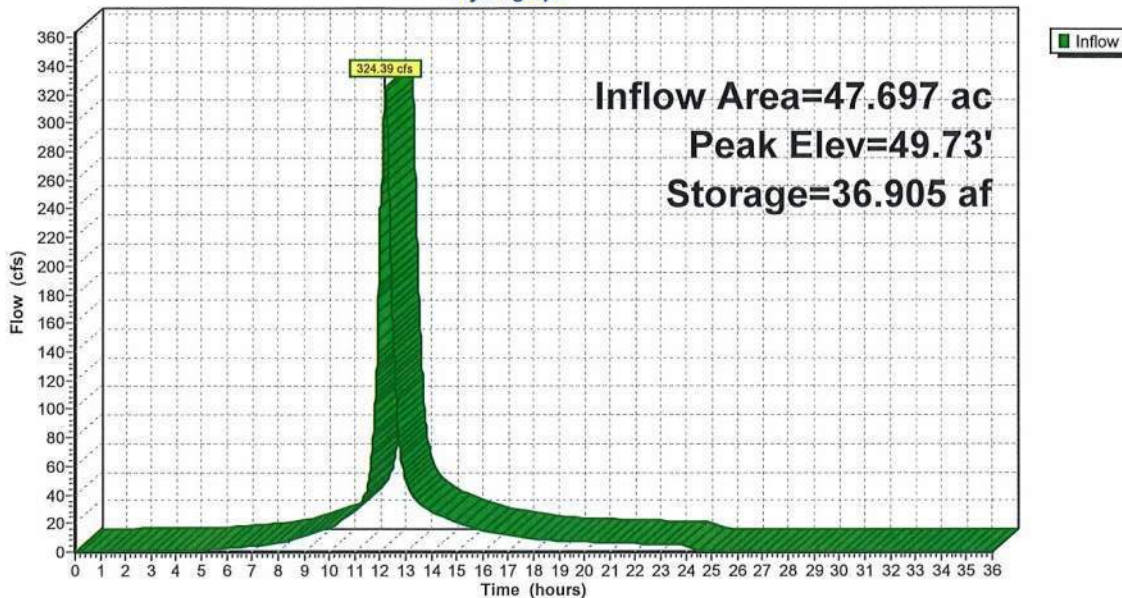
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**Pond PA: Retention Pond A**

Hydrograph



**Post Development 100 Yr Drainage**

*Type III 24-hr 100-Year Rainfall=11.50"*

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**Summary for Pond PB: Detention Pond B**

Inflow Area = 42.338 ac, 0.00% Impervious, Inflow Depth = 9.07" for 100-Year event  
 Inflow = 331.73 cfs @ 12.16 hrs, Volume= 32.018 af  
 Outflow = 42.26 cfs @ 12.98 hrs, Volume= 31.217 af, Atten= 87%, Lag= 49.7 min  
 Primary = 42.26 cfs @ 12.98 hrs, Volume= 31.217 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 52.22' @ 12.98 hrs Surf.Area= 3.914 ac Storage= 16.607 af

Plug-Flow detention time= 253.1 min calculated for 31.217 af (97% of inflow)  
 Center-of-Mass det. time= 237.9 min ( 1,027.8 - 789.9 )

Volume	Invert	Avail. Storage	Storage Description		
#1	47.00'	19.739 af	<b>Custom Stage Data (Irregular) Listed below (Recalc)</b>		
Elevation (feet)	Surf.Area (acres)	Perim. (feet)	Inc.Store (acre-feet)	Cum.Store (acre-feet)	Wet.Area (acres)
47.00	2.450	3,998.7	0.000	0.000	2.450
48.00	2.730	4,022.7	2.589	2.589	2.814
49.00	3.010	4,046.7	2.869	5.458	3.179
50.00	3.290	4,070.7	3.149	8.607	3.547
51.00	3.570	4,094.6	3.429	12.036	3.916
52.00	3.850	4,118.8	3.709	15.745	4.291
53.00	4.140	4,158.1	3.994	19.739	4.893

Device	Routing	Invert	Outlet Devices
#1	Primary	47.00'	<b>21.0" Round RCP_Round 21"</b> L= 128.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 47.00' / 46.75' S= 0.0020' / Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 2.41 sf
#2	Primary	47.00'	<b>21.0" Round RCP_Round 21"</b> L= 128.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 47.00' / 46.75' S= 0.0020' / Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 2.41 sf

**Primary OutFlow Max=42.26 cfs @ 12.98 hrs HW=52.22' (Free Discharge)**

- 1=RCP\_Round 21" (Barrel Controls 21.13 cfs @ 8.78 fps)
- 2=RCP\_Round 21" (Barrel Controls 21.13 cfs @ 8.78 fps)

**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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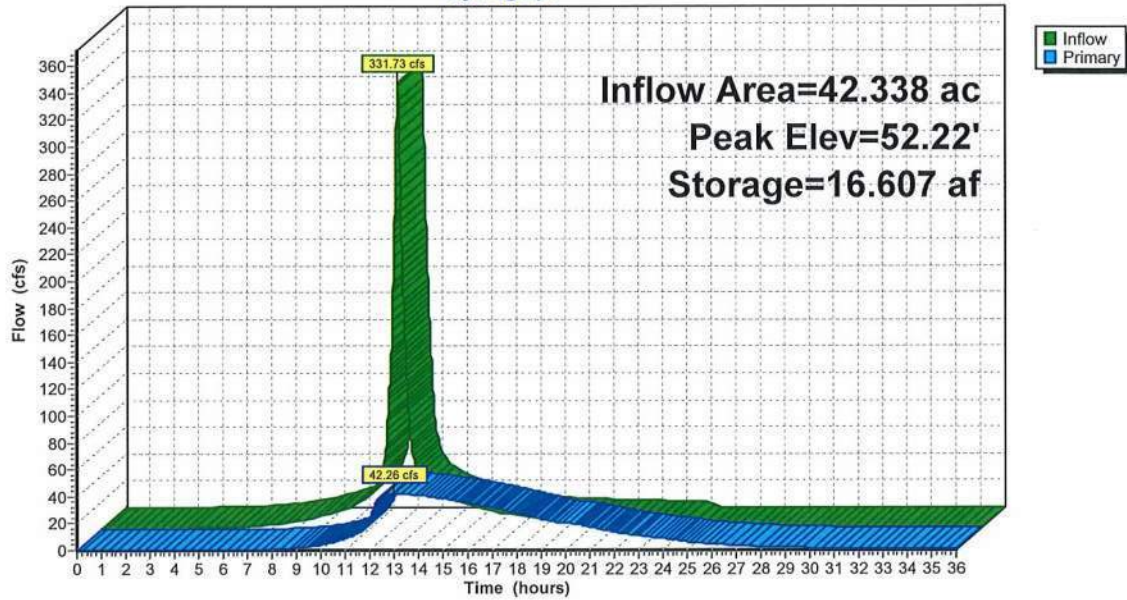
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**Pond PB: Detention Pond B**

Hydrograph



**Post Development 100 Yr Drainage**

*Type III 24-hr 100-Year Rainfall=11.50"*

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**Summary for Pond PC: Retention Pond C**

No Discharge. Construction of Perimeter Berm to Elevation 48 ft. Required.

Inflow Area = 61.564 ac, 0.00% Impervious, Inflow Depth = 9.05" for 100-Year event  
 Inflow = 446.58 cfs @ 12.22 hrs, Volume= 46.421 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Peak Elev= 45.81' @ 36.00 hrs Surf.Area= 4.259 ac Storage= 46.421 af

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description		
#1	31.00'	56.115 af	Custom Stage Data (Irregular) Listed below (Recalc)		
Elevation (feet)	Surf.Area (acres)	Perim. (feet)	Inc.Store (acre-feet)	Cum.Store (acre-feet)	Wet.Area (acres)
31.00	2.060	2,014.1	0.000	0.000	2.060
32.00	2.200	2,032.9	2.130	2.130	2.207
33.00	2.340	2,051.7	2.270	4.399	2.354
34.00	2.480	2,070.5	2.410	6.809	2.504
35.00	2.630	2,089.2	2.555	9.364	2.654
36.00	2.770	2,108.0	2.700	12.063	2.806
37.00	2.920	2,126.8	2.845	14.908	2.959
38.00	3.060	2,145.6	2.990	17.898	3.114
39.00	3.210	2,164.4	3.135	21.032	3.270
40.00	3.360	2,183.2	3.285	24.317	3.427
41.00	3.510	2,201.9	3.435	27.752	3.585
42.00	3.660	2,220.7	3.585	31.337	3.745
43.00	3.820	2,239.5	3.740	35.076	3.907
44.00	3.970	2,258.3	3.895	38.971	4.070
45.00	4.130	2,277.1	4.050	43.021	4.234
46.00	4.290	2,295.9	4.210	47.230	4.400
47.00	4.440	2,314.6	4.365	51.595	4.566
48.00	4.600	2,333.4	4.520	56.115	4.734

**Post Development 100 Yr Drainage**

Type III 24-hr 100-Year Rainfall=11.50"

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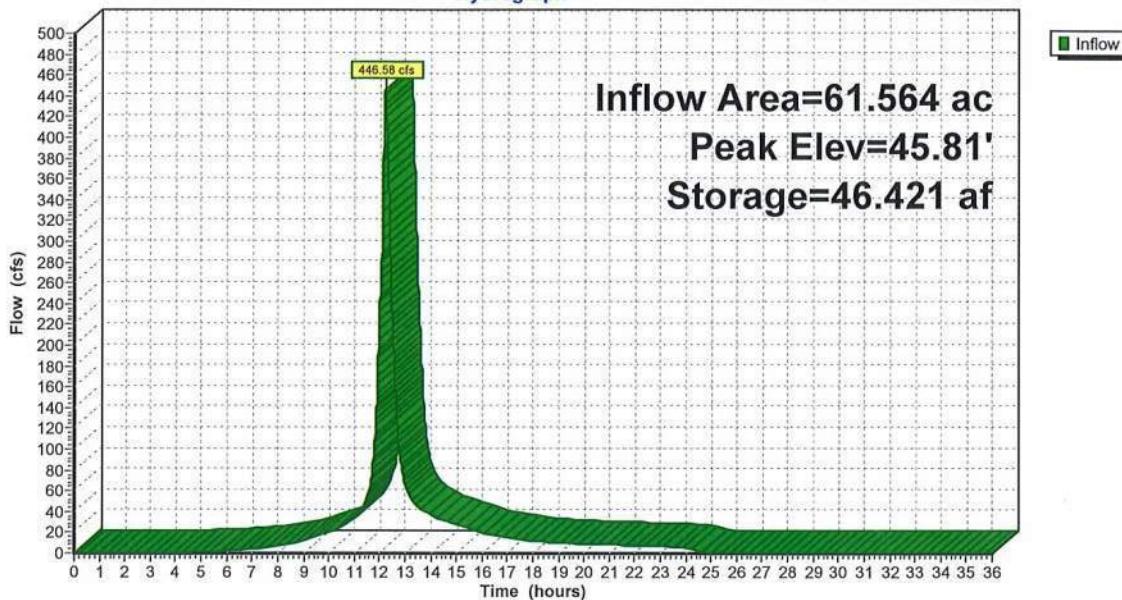
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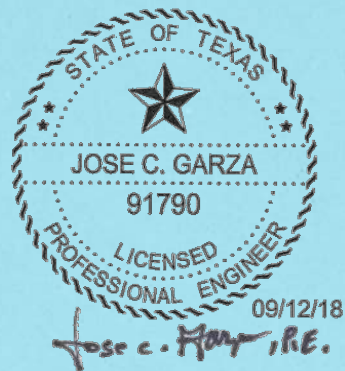
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**Pond PC: Retention Pond C**

Hydrograph



APPENDIX 6B.6  
HYDROCAD MODEL POST DEVELOPMENT 25 YEAR POND  
SUMMARY





25 YEAR POND SUMMARY

Retention Pond A (Irregular Shape)

Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
36.75	58430.13	1.34	1049.83	0.00
37	60148.48	1.38	1064.95	0.34
38	67269.32	1.54	1125.40	1.80
39	74737.41	1.72	1171.54	3.43
40	82487.17	1.89	1216.78	5.23
41	92350.92	2.12	1292.54	7.24
42	102766.37	2.36	1370.62	9.48
43	114109.20	2.62	1447.92	11.96
44	126406.25	2.90	1537.27	14.72
45	139784.84	3.21	1623.30	17.78
46	154666.98	3.55	1699.39	21.16
47	170157.85	3.91	1769.61	24.88
48	185990.18	4.27	1832.75	28.97
49	201992.64	4.64	1894.58	33.43
50	218522.96	5.02	1956.10	38.26
51	237214.05	5.45	2024.29	43.49
52	255380.19	5.86	2075.63	49.14
53	268998.35	6.18	2125.30	55.16
54	282587.03	6.49	2167.18	61.50
55	296319.75	6.80	2209.05	68.14
56	310196.38	7.12	2250.89	75.10
57	324212.86	7.44	2292.64	82.38

Summary

Pond Depth = 20.25 ft  
 Peak Elevation = 47.33 ft  
 Peak Inflow = 225.75 cfs  
 Peak Outflow = No Discharge  
 Peak Storage = 26.20 Ac-ft  
 Freeboard = 9.67 ft

Retention Pond B (Irregular Shape)

Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
47	106908.62	2.45	3998.70	0.00
48	118939.02	2.73	4022.70	2.59
49	131040.75	3.01	4046.70	5.46
50	143213.79	3.29	4070.70	8.61
51	155458.15	3.57	4094.60	12.04
52	167773.82	3.85	4118.80	15.75
53	180160.81	4.14	4158.10	19.74

Summary

Pond Depth = 6 ft  
 Peak Elevation = 50.87 ft  
 Peak Inflow = 235.89 cfs  
 Peak Outflow = 33.70 cfs  
 Peak Storage = 11.56 Ac-ft  
 Culvert size = 2 X 21 in x 128 ft RCP  
 Culvert Slope = 0.20%  
 Freeboard = 2.13 ft

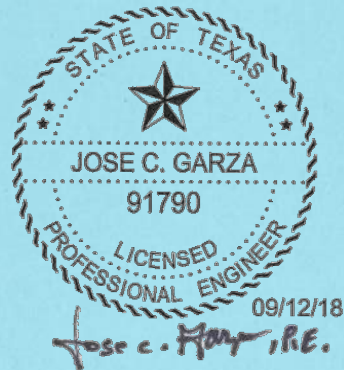
Retention Pond C (Irregular Shape)

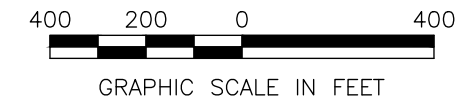
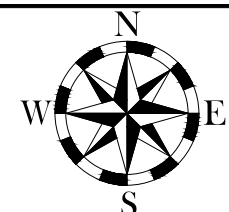
Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
31	89848.61	2.06	2014.10	0.00
32	95917.31	2.20	2032.90	2.13
33	102041.29	2.34	2051.70	4.40
34	108220.56	2.48	2070.50	6.81
35	114455.12	2.63	2089.20	9.36
36	120744.98	2.77	2108.00	12.06
37	127090.14	2.92	2126.80	14.91
38	133490.60	3.06	2145.60	17.90
39	139946.35	3.21	2164.40	21.03
40	146457.40	3.36	2183.20	24.32
41	153023.74	3.51	2201.90	27.75
42	159645.38	3.66	2220.70	31.34
43	166322.32	3.82	2239.50	35.08
44	173054.56	3.97	2258.30	38.97
45	179842.09	4.13	2277.10	43.02
46	186684.91	4.29	2295.90	47.23
47	193583.04	4.44	2314.60	51.60
48	200536.46	4.60	2333.40	56.12

Summary

Pond Depth = 17 ft  
 Peak Elevation = 42.36 ft  
 Peak Inflow = 313.19 cfs  
 Peak Outflow = No Discharge  
 Peak Storage = 32.68 Ac-ft  
 Freeboard = 5.64 ft

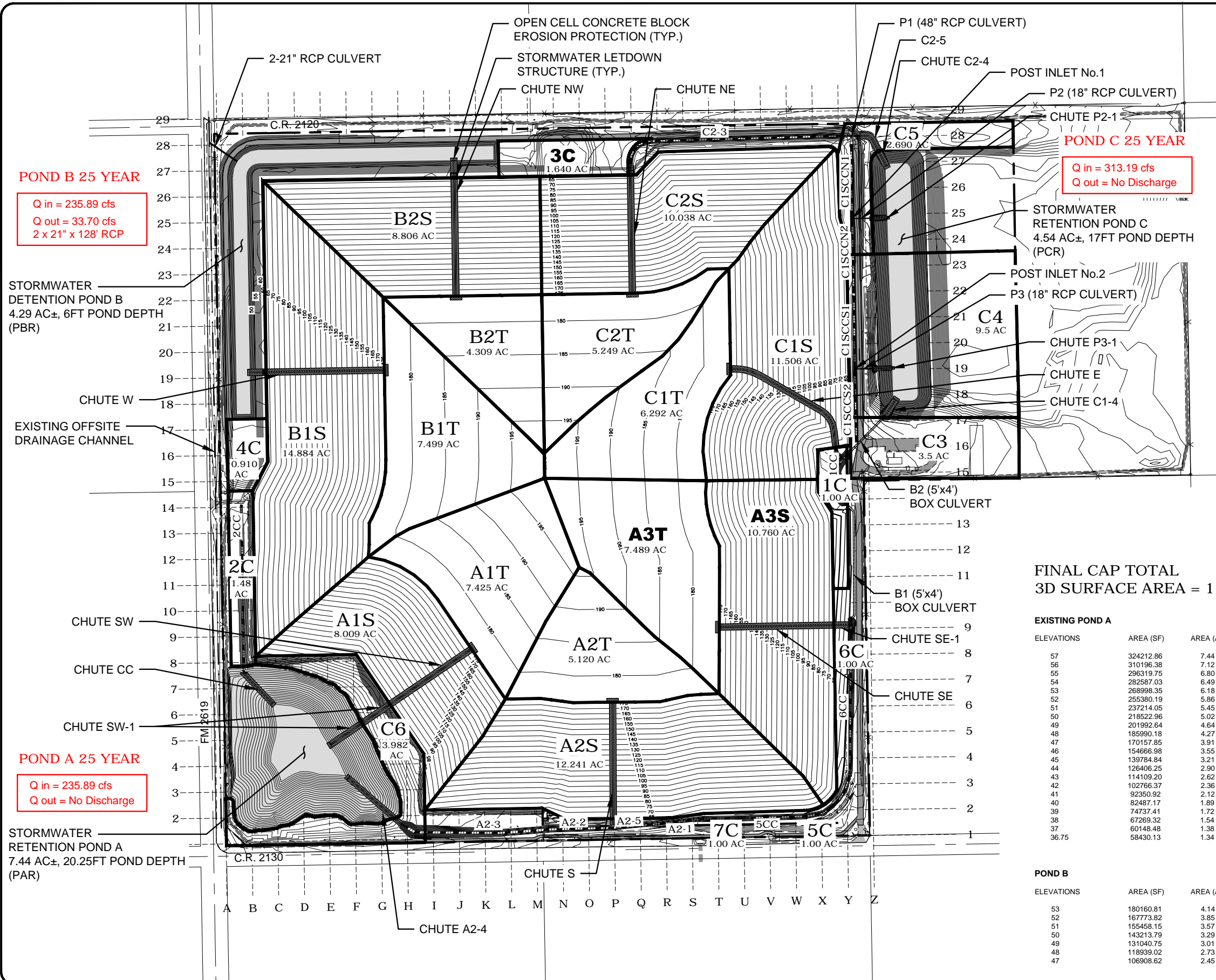
**APPENDIX 6B.6.1**  
**POST DEVELOPMENT DRAINAGE PLAN-25 YEAR**





**LEGEND:**

- EXISTING FENCE CORNER
- X — EXISTING FENCE
- 65.00 — EXISTING CONTOUR
- — — EXISTING ROAD
- — — PERMIT BOUNDARY LIMITS
- 200 — FINAL COVER CONTOURS
- — — PROPOSED ROAD
- ▬ PROPOSED STORMWATER LETDOWN STRUCTURE
- ▭ PROPOSED STORMWATER PONDS
- — — PROPOSED STORMWATER COLLECTOR CHANNELS



**POND B 25 YEAR**  
 Q in = 235.89 cfs  
 Q out = 33.70 cfs  
 2 x 21" x 128' RCP

**POND C 25 YEAR**  
 Q in = 313.19 cfs  
 Q out = No Discharge

**POND A 25 YEAR**  
 Q in = 235.89 cfs  
 Q out = No Discharge

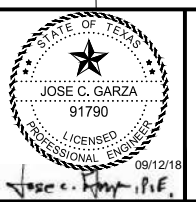
**FINAL CAP TOTAL  
 3D SURFACE AREA = 119.63 AC**

EXISTING POND A				EXISTING POND C			
ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER	ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER
57	324212.86	7.44	2292.64	48	200536.46	4.60	2333.43
56	310196.38	7.12	2250.89	47	193583.04	4.44	2314.65
55	296319.75	6.80	2209.05	46	186684.91	4.29	2295.86
54	282587.03	6.49	2167.18	45	179842.09	4.13	2277.08
53	268998.35	6.18	2125.30	44	173054.56	3.97	2258.30
52	255380.19	5.86	2075.63	43	166322.32	3.82	2239.51
51	237214.05	5.45	2024.29	42	159645.38	3.66	2220.73
50	218522.96	5.02	1956.10	41	153023.74	3.51	2201.94
49	201992.64	4.64	1894.58	40	146457.40	3.36	2183.16
48	185990.18	4.27	1832.75	39	139946.35	3.21	2164.38
47	170157.85	3.91	1769.61	38	133490.60	3.06	2145.59
46	154666.98	3.55	1699.39	37	127090.14	2.92	2126.81
45	139784.84	3.21	1623.30	36	120744.98	2.77	2108.02
44	125406.25	2.90	1537.27	35	114445.12	2.63	2089.24
43	111099.20	2.62	1447.92	34	108220.56	2.48	2070.46
42	102766.37	2.36	1370.62	33	102041.29	2.34	2051.67
41	92350.92	2.12	1292.54	32	95917.31	2.20	2032.89
40	82487.17	1.89	1216.78	31	89848.61	2.06	2014.10
39	74737.41	1.72	1171.54				
38	67269.32	1.54	1125.40				
37	60148.48	1.38	1064.95				
36.75	58430.13	1.34	1049.83				

POND B			
ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER
53	180160.81	4.14	4158.15
52	167773.82	3.85	4118.62
51	155458.15	3.57	4094.65
50	143213.79	3.29	4070.67
49	131040.75	3.01	4046.70
48	118939.02	2.73	4022.72
47	106908.62	2.45	3998.75

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DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

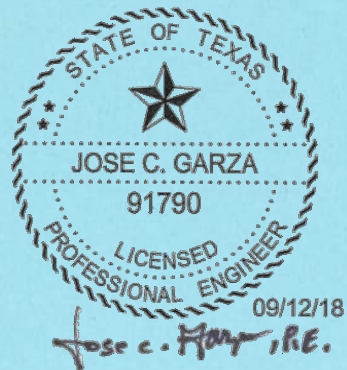
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PART III, ATTACHMENT 6, APPENDIX 6B.6.1  
 POST DEVELOPMENT DRAINAGE PLAN-25 YEAR  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

FIGURE:  
 III.6-6B.6.1

**APPENDIX 6B.7**  
**HYDROCAD MODEL POST DEVELOPMENT 100 YEAR POND**  
**SUMMARY**



100 YEAR POND SUMMARY

Retention Pond A (Irregular Shape)

Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
36.75	58430.13	1.34	1049.83	0.00
37	60148.48	1.38	1064.95	0.34
38	67269.32	1.54	1125.40	1.80
39	74737.41	1.72	1171.54	3.43
40	82487.17	1.89	1216.78	5.23
41	92350.92	2.12	1292.54	7.24
42	102766.37	2.36	1370.62	9.48
43	114109.20	2.62	1447.92	11.96
44	126406.25	2.90	1537.27	14.72
45	139784.84	3.21	1623.30	17.78
46	154666.98	3.55	1699.39	21.16
47	170157.85	3.91	1769.61	24.88
48	185990.18	4.27	1832.75	28.97
49	201992.64	4.64	1894.58	33.43
50	218522.96	5.02	1956.10	38.26
51	237214.05	5.45	2024.29	43.49
52	255380.19	5.86	2075.63	49.14
53	268998.35	6.18	2125.30	55.16
54	282587.03	6.49	2167.18	61.50
55	296319.75	6.80	2209.05	68.14
56	310196.38	7.12	2250.89	75.10
57	324212.86	7.44	2292.64	82.38

Summary

Pond Depth = 20.25 ft  
 Peak Elevation = 49.73 ft  
 Peak Inflow = 324.39 cfs  
 Peak Outflow = No Discharge  
 Peak Storage = 36.90 Ac-ft  
 Freeboard = 7.27 ft

Detention Pond B (Irregular Shape)

Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
47	106908.62	2.45	3998.70	0.00
48	118939.02	2.73	4022.70	2.59
49	131040.75	3.01	4046.70	5.46
50	143213.79	3.29	4070.70	8.61
51	155458.15	3.57	4094.60	12.04
52	167773.82	3.85	4118.80	15.75
53	180160.81	4.14	4158.10	19.74

Summary

Pond Depth = 6 ft  
 Peak Elevation = 52.22 ft  
 Peak Inflow = 331.73 cfs  
 Peak Outflow = 42.46 cfs  
 Peak Storage = 16.607 Ac-ft  
 Culvert size = 2 X 21 in x 128 ft RCP  
 Culvert Slope = 0.20%  
 Freeboard = 0.78 ft

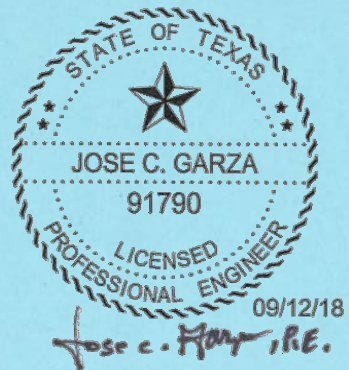
Retention Pond C (Irregular Shape)

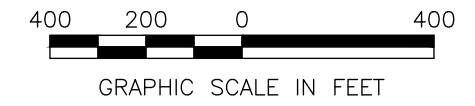
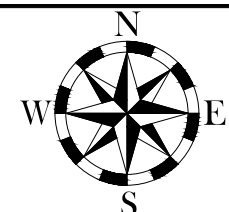
Elevation (ft)	Surface Area (sf)	Surface Area (acres)	Perimeter (ft)	Cum. Store (Ac-ft)
31	89848.61	2.06	2014.10	0.00
32	95917.31	2.20	2032.90	2.13
33	102041.29	2.34	2051.70	4.40
34	108220.56	2.48	2070.50	6.81
35	114455.12	2.63	2089.20	9.36
36	120744.98	2.77	2108.00	12.06
37	127090.14	2.92	2126.80	14.91
38	133490.60	3.06	2145.60	17.90
39	139946.35	3.21	2164.40	21.03
40	146457.40	3.36	2183.20	24.32
41	153023.74	3.51	2201.90	27.75
42	159645.38	3.66	2220.70	31.34
43	166322.32	3.82	2239.50	35.08
44	173054.56	3.97	2258.30	38.97
45	179842.09	4.13	2277.10	43.02
46	186684.91	4.29	2295.90	47.23
47	193583.04	4.44	2314.60	51.60
48	200536.46	4.60	2333.40	56.12

Summary

Pond Depth = 17 ft  
 Peak Elevation = 45.81 ft  
 Peak Inflow = 446.58 cfs  
 Peak Outflow = No Discharge  
 Peak Storage = 46.42 Ac-ft  
 Freeboard = 2.19 ft

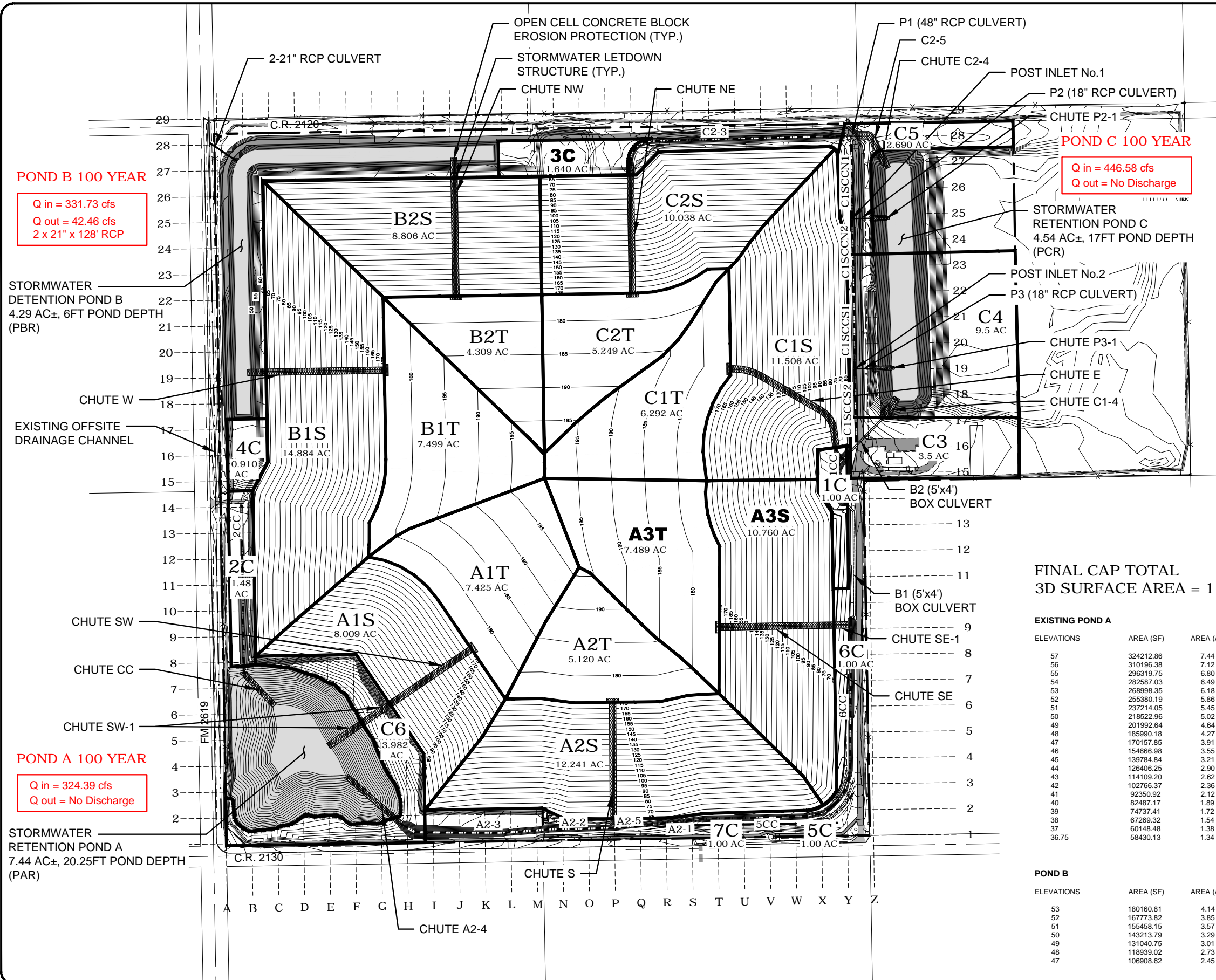
**APPENDIX 6B.7.1**  
**POST DEVELOPMENT DRAINAGE PLAN-100 YEAR**





**LEGEND:**

- EXISTING FENCE CORNER
- X — EXISTING FENCE
- 65.00 — EXISTING CONTOUR
- — EXISTING ROAD
- - - PERMIT BOUNDARY LIMITS
- 200 — FINAL COVER CONTOURS
- — PROPOSED ROAD
- ▬ PROPOSED STORMWATER LETDOWN STRUCTURE
- ▭ PROPOSED STORMWATER PONDS
- - - PROPOSED STORMWATER COLLECTOR CHANNELS



**POND B 100 YEAR**  
 Q in = 331.73 cfs  
 Q out = 42.46 cfs  
 2 x 21" x 128' RCP

**POND C 100 YEAR**  
 Q in = 446.58 cfs  
 Q out = No Discharge

**POND A 100 YEAR**  
 Q in = 324.39 cfs  
 Q out = No Discharge

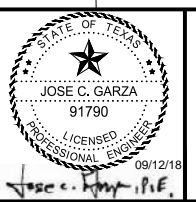
**FINAL CAP TOTAL  
 3D SURFACE AREA = 119.63 AC**

EXISTING POND A				EXISTING POND C			
ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER	ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER
57	324212.86	7.44	2292.64	48	200536.46	4.60	2333.43
56	310196.38	7.12	2250.89	47	193583.04	4.44	2314.65
55	296319.75	6.80	2209.05	46	186684.91	4.29	2295.86
54	282587.03	6.49	2167.18	45	179842.09	4.13	2277.08
53	268998.35	6.18	2125.30	44	173054.56	3.97	2258.30
52	255380.19	5.86	2075.63	43	166322.32	3.82	2239.51
51	237214.05	5.45	2024.29	42	159645.38	3.66	2220.73
50	218522.96	5.02	1956.10	41	153023.74	3.51	2201.94
49	201992.64	4.64	1894.58	40	146457.40	3.36	2183.16
48	185990.18	4.27	1832.75	39	139946.35	3.21	2164.38
47	170157.85	3.91	1769.61	38	133490.60	3.06	2145.59
46	154666.98	3.55	1699.39	37	127090.14	2.92	2126.81
45	139784.84	3.21	1623.30	36	120744.98	2.77	2108.02
44	125406.25	2.90	1537.27	35	114455.12	2.63	2089.24
43	111099.20	2.62	1447.92	34	108220.56	2.48	2070.46
42	102766.37	2.36	1370.62	33	102041.29	2.34	2051.67
41	92350.92	2.12	1292.54	32	95917.31	2.20	2032.89
40	82487.17	1.89	1216.78	31	89848.61	2.06	2014.10
39	74737.41	1.72	1171.54				
38	67269.32	1.54	1125.40				
37	60148.48	1.38	1064.95				
36.75	58430.13	1.34	1049.83				

POND B			
ELEVATIONS	AREA (SF)	AREA (AC)	PERIMETER
53	180160.81	4.14	4158.15
52	167773.82	3.85	4118.62
51	155458.15	3.57	4094.65
50	143213.79	3.29	4070.67
49	131040.75	3.01	4046.70
48	118939.02	2.73	4022.72
47	106908.62	2.45	3998.75

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Hanson No.	1610438
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Scale	AS SHOWN
Date	09/12/2018
LAYOUT	DT 09/12/2018
DRAWN	DT 09/12/2018
REVIEWED	JMR 09/12/2018

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PART III, ATTACHMENT 6, APPENDIX 6B.7.1  
 POST DEVELOPMENT DRAINAGE PLAN-100 YEAR  
 CITY OF KINGSVILLE LANDFILL  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:  
 III.6-6B.7.1**

**APPENDIX 6B.8**  
**KINGSVILLE LANDFILL PERMIT AMENDMENT 235-B**



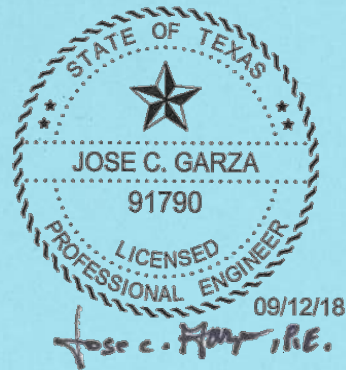
**KINGSVILLE LANDFILL PERMIT AMENDMENT 235-B**

**PORTION OF ATTACHMENT 6 GROUNDWATER AND SURFACEWATER  
PROTECTION PLAN (PRE-DEVELOPMENT/POST DEVELOPMENT  
DRAINAGE CONDITIONS & DESIGN)**

**PORTION OF APPENDIX 6A-PRE-DEVELOPMENT CONDITIONS  
(FIGURE A-1 PRE-DEVELOPMENT DRAINAGE MAP)**

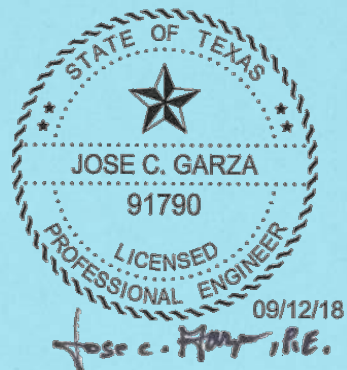
**PORTION OF APPENDIX 6B-FINAL DEVELOPMENT CONDITIONS  
(FIGURE B-1 FINAL DEVELOPMENT DRAINAGE MAP)**

**PORTION OF APPENDIX 6C DETENTION PONDS AND DISCHARGE  
CULVERTS (25-YEAR STORM STRATEGY/COMPARATIVE SUMMARY OF  
PEAK FLOWS)**



APPENDIX 6B.8.1

PORTION OF ATTACHMENT 6 GROUNDWATER AND SURFACE  
WATER PROTECTION PLAN (PRE-DEVELOPMENT/POST  
DEVELOPMENT DRAINAGE CONDITIONS AND DESIGN  
[ANNOTATED]



# Attachment 6

## Groundwater and Surface Water Protection Plan

### City of Kingsville Municipal Landfill Facility Permit Amendment Application 235-B

Prepared by: Alpha Engineering

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- Appendix 6A Pre-Development Conditions
- Appendix 6B Final Development Conditions
- Appendix 6C Detention Ponds and Discharge Culverts
- Appendix 6D Drainage Channel Profiles and Cross-Sections
- Appendix 6E Erosion Control Plan
- Appendix 6F Offsite Drainage System
- Appendix 6G References



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 May 1998

City of Kingsville MSW 235-B  
 Attachment 6 Groundwater and Surface Water Protection Plan

are as follows. **From 2.0 Pre-Development Drainage Conditions**

Watershed	Drainage Area Name	25-Year Peak Flow (cfs)
A	PA1	27.3
	PA2	22.0
	PA3	13.7
B	PB1	19.0
	PB2	4.3
	PB3	5.4
C	PC1	39.6
	PC2	15.7
	PC3	3.1

**3.0 POST-DEVELOPMENT DRAINAGE CONDITIONS AND DESIGN**

The post-development peak discharge analysis defines the hydrologic conditions for the final landfill development. The method for calculating the 25-year peak discharge flows also follows the TR-55 worksheets and is shown in Appendix 6B. Since the composition of the final cover material and slopes are different from the pre-existing conditions, the CN values also change to reflect an increase runoff, and are shown below.

Description	CN
Unimproved, 0 – 7% slope	60
Unimproved, greater than 7% slope	70

Appendix 6B includes final development contour maps, drainage area boundaries, slope map, and each worksheet necessary to calculate the post-development peak discharges for the strategic points. Although the landfill facility changes the storm water drainage patterns from the site pre-development conditions, the surrounding natural drainage patterns will not be adversely affected. The peak discharge flows **before detention** are as follows.

Watershed	Drainage Area Name	25-Year Peak Flow (cfs)
A	FA	87.3
B	FB	68.0
C	FC	71.7

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 Revision 3

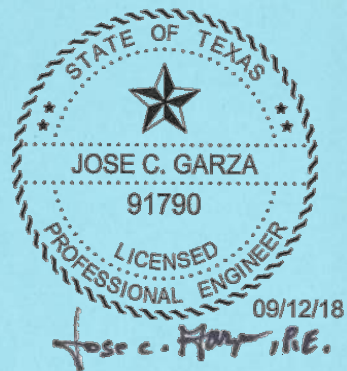
Kingsville Landfill Permit Amendment 235-B  
Attachment 6**Appendix 6A  
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Figure A-2	Pre-Development Slope Map

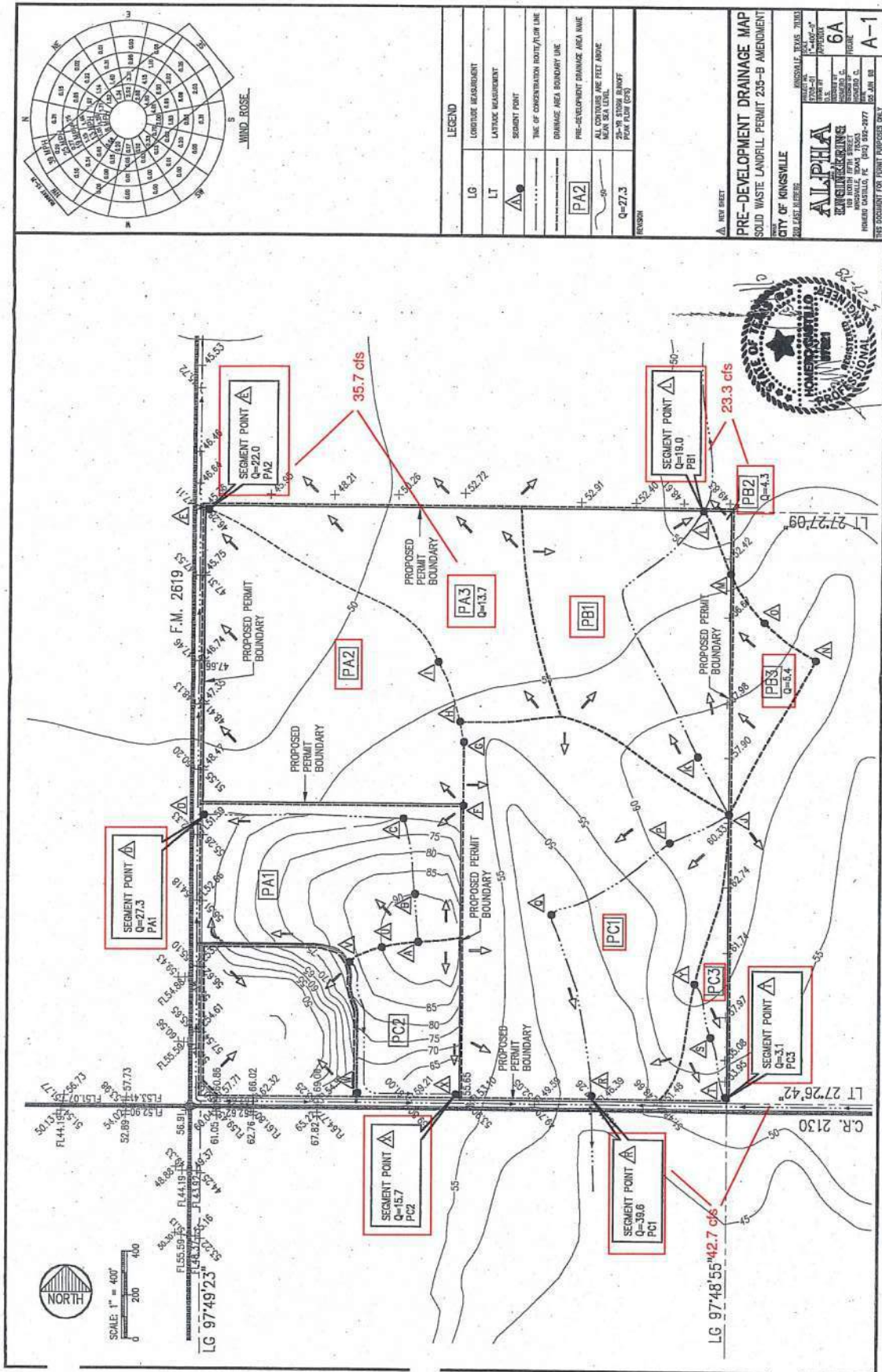
May 1998  
Revision 1

APPENDIX 6B.8.2

PORTION OF APPENDIX 6A-PRE-DEVELOPMENT CONDITIONS  
(FIGURE A-1 PRE-DEVELOPMENT DRAINAGE MAP) [ANNOTATED]



FOR PERMIT PURPOSES ONLY



Kingsville Landfill Permit Amendment 235-B  
Attachment 6**Appendix 6B**  
**Final Development Conditions****TABLE OF CONTENTS**

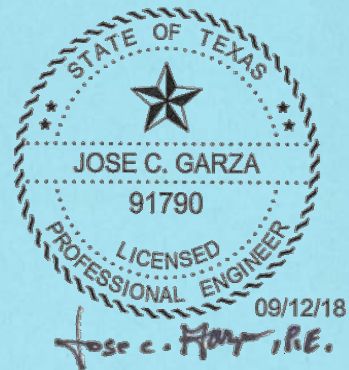
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Berm B3	13
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Figure B-1	Final Development Drainage Map
Figure B-2	Final Development Slope Map
Figure B-3	Final Cover Phase 1
Figure B-4	Perimeter Road and Berm Sections

May 1998  
Revision 1

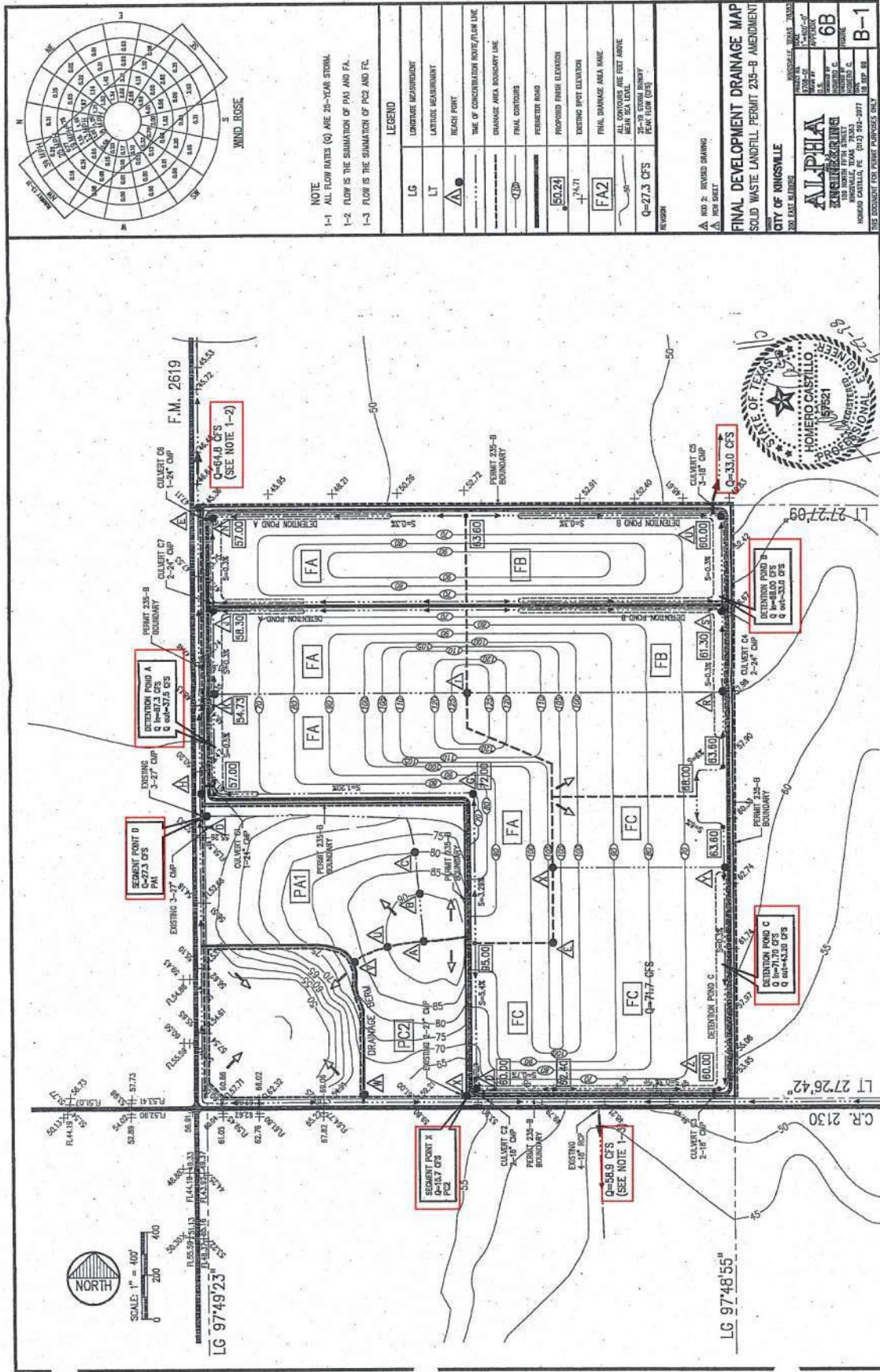


APPENDIX 6B.8.3

PORTION OF APPENDIX 6B-FINAL DEVELOPMENT CONDITIONS  
(FIGURE B-1 FINAL DEVELOPMENT DRAINAGE MAP) [ANNOTATED]



FOR PERMIT PURPOSES ONLY



**NOTE**  
 1-1 ALL FLOW RATES (Q) ARE 25-YEAR STORM.  
 1-2 FLOW IS THE SIMULATION OF PA1 AND FA.  
 1-3 FLOW IS THE SIMULATION OF PC2 AND FC.

LEGEND	
LG	LATITUDE MEASUREMENT
LT	LATITUDE MEASUREMENT
△	REACH POINT
---	LINE OF CONCENTRATION BOUNDARY/FORM LINE
---	DRAINAGE AREA BOUNDARY LINE
---	FINAL CONTOUR
---	PROPOSED ROAD
50.24	PROPOSED FINISH ELEVATION
7.471	EXISTING SPOT ELEVATION
FA2	FINAL DRAINAGE AREA WIDE
---	ALL CONTOURS ARE FEET ABOVE MEAN SEA LEVEL
Q=27.3 CFS	PERMIT FLOW CAPACITY
REVISION	

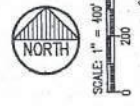
A NO. 2: REVISED DRAWING  
 A: NEW SHEET

**FINAL DEVELOPMENT DRAINAGE MAP**  
 SOLID WASTE LANDFILL PERMIT 235-B AMENDMENT  
 CITY OF KINGSVILLE  
 202 EAST SAUNDERS

**ALPHA ENGINEERING**  
 100 SOUTH 17TH STREET  
 HOUSTON, TEXAS 77058  
 HOMERO CASTILLO, P.E. (043) 994-2077  
 LICENSE NO. 10000

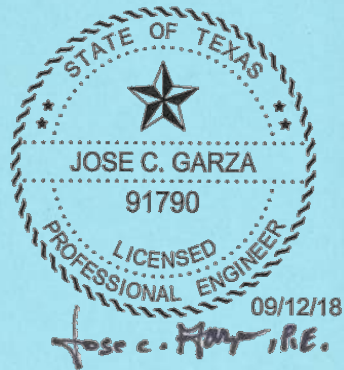
PROFESSIONAL ENGINEER  
 STATE OF TEXAS  
 109221

PROJECT NO. 235-B  
 SHEET NO. 6B  
 TOTAL SHEETS 6B-1



**APPENDIX 6B.8.4**

**PORTION OF APPENDIX 6C DETENTION PONDS AND DISCHARGE  
CULVERTS (25-YEAR STORM STRATEGY/COMPARATIVE SUMMARY  
OF PEAK FLOWS) [ANNOTATED]**



Kingsville Landfill Permit Amendment 235-B  
Attachment 6

## Appendix 6C Detention Ponds and Discharge Culverts

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Figure C-1 Detention Pond A  
Figure C-2 Detention Pond B  
Figure C-3 Detention Pond C



May 1998  
Revision 1

Kingsville Landfill Permit 235-B  
 Attachment 6

### 25-Year Stormwater Detention Strategy

**Watershed A**

Pre-Development Conditions	
Area No.	Peak Flow (cfs)
PA2	22.0
PA3	13.7
<b>Total</b>	<b>35.7</b>

Final Development Conditions (before detention)	
Area No.	Peak Flow (cfs)
FA	87.3
<b>Total</b>	<b>87.3</b>

Maximum Final Development discharge for Watershed A shall not exceed 35.7 cfs

**Watershed B**

Pre-Development Conditions	
Area No.	Peak Flow (cfs)
PB1	19.0
PB2	4.3
<b>Total</b>	<b>23.3</b>

Final Development Conditions (before detention)	
Area No.	Peak Flow (cfs)
FB	68.0
<b>Total</b>	<b>68.0</b>

Maximum Final Development discharge for Watershed B shall not exceed 23.3 cfs

**Watershed C**

Pre-Development Conditions	
Area No.	Peak Flow (cfs)
PC1	39.6
PC3	3.1
<b>Total</b>	<b>42.7</b>

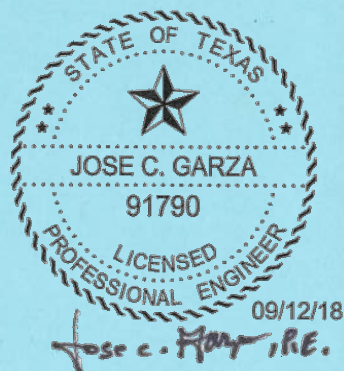
Final Development Conditions (before detention)	
Area No.	Peak Flow (cfs)
FC	71.7
<b>Total</b>	<b>71.7</b>

Maximum Final Development discharge for Watershed ~~B~~ shall not exceed 42.7 cfs  
 C

#### Comparative Summary of Peak Flows

	Pre-Development 25-Year Peak Flow	Final Development 25-Year Peak Flow (after detention)
Watershed A	35.7 cfs	37.5 cfs
Watershed B	23.3 cfs	33.0 cfs
Watershed C	42.7 cfs	43.2 cfs

**APPENDIX 6B.9**  
**PERIMETER CHANNELS, COLLECTOR CHANNELS, AND CHUTES-25**  
**YEAR SUMMARY TABLE**



FOR PERMIT PURPOSES ONLY

25 Year Perimeter Channels, Collector Channels, & Chutes Summary Table

Channel ID	Length (FT)	Beginning			Ending				Trapezoidal, Triangular, Box, & Pipe Channels													
		Existing NG Elev	Depth (FT)	FL	Existing NG Elev	Slope (FT/FT)	FL	Depth (FT)	Base Width (FT)	Avg Channel Depth (FT)	**Avg Channel Flow Depth (FT)	***Hydraulic Grade Elev	Freeboard (FT)	Bottom Slope (FT/FT)	Side Slope	Top Width (FT)	Manning n	Wetted Perimeter (FT)	Area (SF)	Hydraulic Radius	Velocity (FPS)	Qp (CFS)
<b>EAST</b>																						
6CC	740.00	61.71	2.21	59.50	62.36	0.0040	56.54	5.82	2.00	4.02	0.77	60.27	1.4	0.0040	2.00	10.84	0.030	5.44	2.73	0.50	1.98	5.40
B1	464.00	62.36	4.00	56.54	65.59	0.0057	53.89	4.00	5.00	4.00	2.17	58.71	1.8	0.0057	0.00	5.00	0.013	9.34	10.85	1.16	9.57	103.85
1CC	222.00	65.59	11.70	53.89	61.74	0.0020	53.45	8.29	3.00	10.00	4.52	58.41	7.2	0.0020	2.00	49.80	0.030	23.21	54.42	2.34	3.90	212.35
B2	200.00	61.74	4.00	53.45	59.30	0.0183	49.80	4.00	5.00	4.00	2.44	55.85	1.6	0.0183	0.00	5.00	0.013	9.88	12.20	1.23	17.82	217.42
<b>SOUTH</b>																						
5CC	595.00	61.64	3.14	58.50	61.01	0.0015	57.61	3.40	2.00	3.27	0.97	59.47	2.2	0.0015	2.00	14.56	0.030	6.34	3.82	0.60	1.37	5.24
A2-1	250.50	61.01	3.40	57.61	60.16	0.0015	57.23	2.93	2.00	3.17	1.24	58.85	2.2	0.0015	2.00	15.60	0.030	7.55	5.56	0.74	1.58	8.76
A2-5	5.60	60.16	2.93	57.23	60.18	0.2482	55.84	4.34	2.00	3.64	0.30	57.53	2.6	0.2482	2.00	13.72	0.025	3.34	0.78	0.23	11.26	8.78
A2-2	257.00	60.18	4.34	55.84	60.98	0.0020	55.33	5.65	7.00	5.00	2.54	58.37	1.8	0.0020	2.00	24.36	0.025	18.36	30.68	1.67	3.74	114.73
A2-3	582.00	60.98	5.65	55.33	60.40	0.0020	54.17	6.23	8.00	5.94	2.58	57.90	3.1	0.0020	2.00	30.60	0.030	19.54	33.95	1.74	3.20	108.82
<b>NORTH</b>																						
C2-3	882.00	57.50	4.00	53.50	57.50	0.0020	51.75	5.75	4.00	4.88	2.82	56.32	1.2	0.0020	2.00	20.00	0.030	16.61	27.18	1.64	3.07	83.52
P1	64.00	57.50	4.00	51.75	57.50	0.0100	51.11	4.00	4.00	4.00	1.97	53.72	2.0	0.0100	NA	4.00	0.011	6.22	6.16	0.99	13.46	82.95
C2-5	106.00	53.61	2.50	51.11	50.50	0.0293	48.00	2.50	5.00	2.50	1.08	52.19	1.4	0.0293	4.00	25.00	0.025	13.91	10.07	0.72	8.23	82.84
C1SCCN1	285.00	60.00	1.50	58.50	60.00	0.0033	57.55	2.45	3.00	1.98	0.33	58.83	1.2	0.0033	2.00	9.00	0.030	4.48	1.21	0.27	1.20	1.45
C1SCCN2	287.50	60.00	1.50	58.50	60.00	0.0033	57.55	2.45	3.00	1.98	0.33	58.83	1.2	0.0033	2.00	9.00	0.030	4.48	1.21	0.27	1.19	1.44
P2	72.00	60.00	1.50	54.39	60.00	0.0150	53.31	1.50	1.50	1.50	0.44	54.83	1.1	0.0150	NA	1.50	0.011	1.72	0.43	0.25	6.61	2.86
C1SCCS1	280.00	60.00	1.50	58.50	60.00	0.0033	57.58	2.42	3.00	1.96	0.33	58.83	1.2	0.0033	2.00	9.00	0.030	4.48	1.21	0.27	1.19	1.44
C1SCCS2	280.00	60.00	1.50	58.50	60.00	0.0033	57.58	2.42	3.00	1.96	0.33	58.83	1.2	0.0033	2.00	9.00	0.030	4.48	1.21	0.27	1.19	1.44
P3	72.00	60.00	1.50	55.41	60.00	0.0150	54.33	1.50	1.50	1.50	0.44	55.85	1.1	0.0150	NA	1.50	0.011	1.72	0.43	0.25	6.61	2.86
<b>WEST</b>																						
2CC	650.00	57.70	3.20	54.50	59.94	0.0020	53.20	6.74	0.00	4.97	1.28	55.78	1.9	0.0020	3.00	19.20	0.030	8.10	4.92	0.61	1.59	7.83

*Chute ID	Length (FT)	Beginning			Ending				Trapezoidal Channel													
		Existing Elev	Depth (FT)	FL	Existing Elev	Slope (FT/FT)	FL	Depth (FT)	Base Width (FT)	Avg Channel Depth	**Avg Channel Flow Depth (FT)	***Hydraulic Grade Elev	Freeboard (FT)	Bottom Slope (FT/FT)	Side Slope	Top Width (FT)	Manning n	Wetted Perimeter (FT)	Area (SF)	Hydraulic Radius	Velocity (FPS)	Qp (CFS)
SE	450.00	176.00	2.00	174.00	63.54	0.2500	61.54	2.00	5.00	2.00	0.69	174.69	1.3	0.2500	4.00	21.00	0.025	10.69	5.35	0.50	18.79	100.64
SE1	62.00	63.54	2.00	61.54	58.54	0.0806	56.54	2.00	5.00	2.00	0.92	62.46	1.1	0.0806	4.00	21.00	0.025	12.59	7.99	0.63	12.49	99.77
S	451.00	176.00	2.00	174.00	61.25	0.2500	61.25	0.00	5.00	1.00	0.72	174.72	1.3	0.2500	4.00	21.00	0.025	10.94	5.67	0.52	19.24	109.15
SW	404.00	176.00	2.00	174.00	77.00	0.2500	73.00	4.00	5.00	3.00	0.67	174.67	1.3	0.2500	4.00	21.00	0.025	10.52	5.15	0.49	18.49	95.16
W	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.78	174.78	1.2	0.2500	4.00	21.00	0.025	11.43	6.33	0.55	20.10	127.32
NW	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.60	174.60	1.4	0.2500	4.00	21.00	0.025	9.95	4.44	0.45	17.40	77.27
NE	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.66	174.66	1.3	0.2500	4.00	21.00	0.025	10.44	5.04	0.48	18.34	92.49
E	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.71	174.71	1.3	0.2500	4.00	21.00	0.025	10.85	5.57	0.51	19.09	106.27
C1-4	76.00	51.80	2.00	49.80	33.00	0.2474	31.00	2.00	5.00	2.50	1.01	50.81	1.0	0.2474	4.00	21.00	0.025	13.33	9.13	0.69	23.04	210.33
C2-4	52.00	50.00	2.00	48.00	33.00	0.3269	31.00	2.00	5.00	2.00	0.58	48.58	1.4	0.3269	4.00	21.00	0.025	9.78	4.25	0.43	19.53	82.93
P2-1	60.00	56.15	1.50	53.31	32.50	0.3718	31.00	1.50	2.00	1.50	0.14	53.45	1.4	0.3718	3.00	11.00	0.025	2.89	0.34	0.12	8.71	2.95
P3-1	60.00	56.15	1.50	54.65	32.50	0.3942	31.00	1.50	2.00	1.50	0.14	54.79	1.4	0.3942	3.00	11.00	0.025	2.89	0.34	0.12	8.97	3.04
A2-4	250.00	56.17	2.00	54.17	38.75	0.0697	36.75	2.00	10.00	2.00	0.75	54.92	1.3	0.0697	4.00	26.00	0.025	16.18	9.75	0.60	11.22	109.41
SW-1	266.00	72.50	2.00	70.50	38.75	0.1269	36.75	2.00	5.00	2.00	0.80	71.30	1.2	0.1269	4.00	21.00	0.025	11.60	6.56	0.57	14.52	95.26
CC	160.00	55.20	2.00	53.20	38.75	0.1028	36.75	2.00	5.00	2.00	0.21	53.41	1.8	0.1028	4.00	21.00	0.025	6.73	1.23	0.18	6.14	7.53

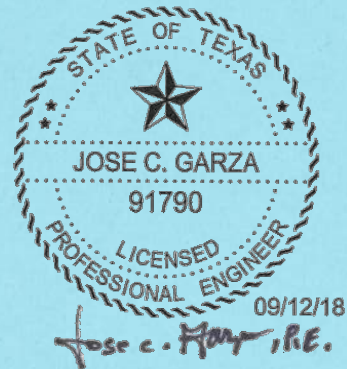
\*Chutes-Precast Interlocking Articulating Concrete Blocks

\*\* Avg Channel Flow Depth Determined by HydroCAD

\*\*\* Hydraulic Grade Elevation Determined by HydroCAD

PerimeterChannel JCG Post 25 Yr 08.20.18.xlsx

**APPENDIX 6B.10**  
**PERIMETER CHANNELS, COLLECTOR CHANNELS, AND CHUTES-100**  
**YEAR SUMMARY TABLE**





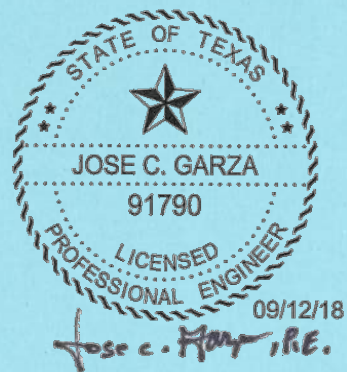
100 Year Perimeter Channels, Collector Channels, & Chutes Summary Table

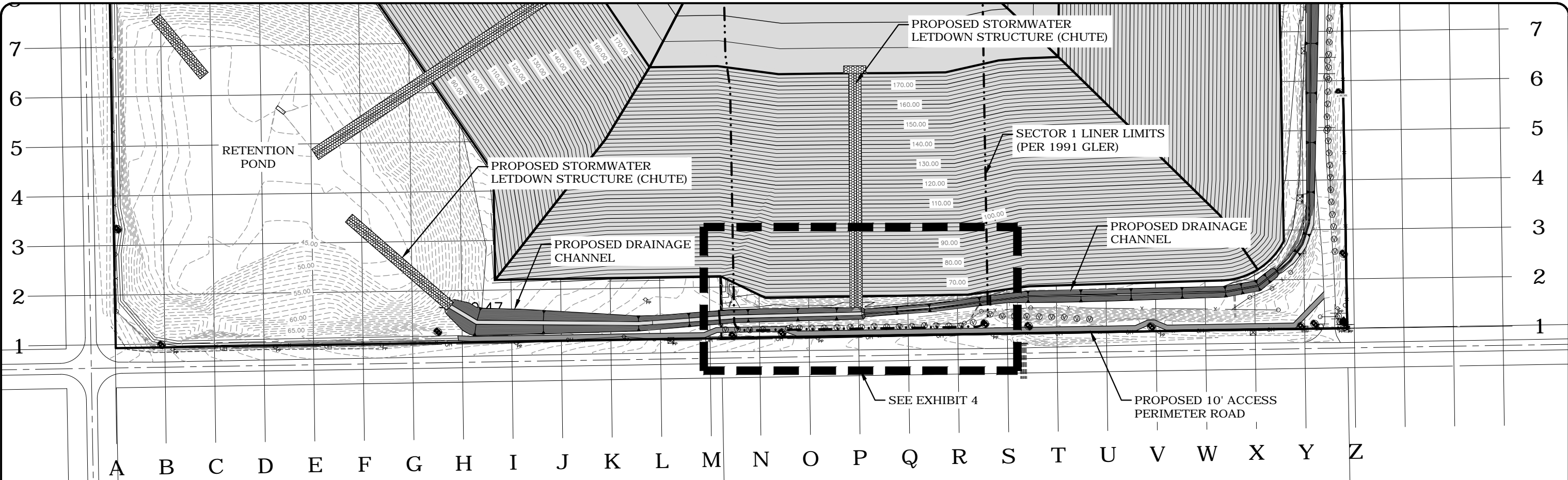
Channel ID	Length (FT)	Beginning			Ending				Trapezoidal, Triangular, Box, & Pipe Channels													
		Existing NG Elev	Depth (FT)	FL	Existing NG Elev	Slope (FT/FT)	FL	Depth (FT)	Base Width (Ft)	Avg Channel Depth (FT)	**Avg Channel Flow Depth (FT)	***Hydraulic Grade Elev	Freeboard (FT)	Bottom Slope (FT/FT)	Side Slope	Top Width (FT)	Manning n	Wetted Perimeter (FT)	Area (SF)	Hydraulic Radius	Velocity (FPS)	Qp (CFS)
<b>EAST</b>																						
6CC	740.00	61.71	2.21	59.50	62.36	0.0040	56.54	5.82	2.00	4.02	0.92	60.42	1.3	0.0040	2.00	10.84	0.030	6.11	3.53	0.58	2.18	7.70
B1	464.00	62.36	4.00	56.54	65.59	0.0057	53.89	4.00	5.00	4.00	2.81	59.35	1.2	0.0057	0.00	5.00	0.013	10.62	14.05	1.32	10.44	146.66
1CC	222.00	65.59	11.70	53.89	61.74	0.0020	53.45	8.29	3.00	10.00	5.24	59.13	6.5	0.0020	2.00	49.80	0.030	26.43	70.64	2.67	4.26	300.75
B2	200.00	61.74	4.00	53.45	59.30	0.0183	49.80	4.00	5.00	4.00	3.12	56.57	0.9	0.0183	0.00	5.00	0.013	11.24	15.60	1.39	19.27	300.54
<b>SOUTH</b>																						
5CC	595.00	61.64	3.14	58.50	61.01	0.0015	57.61	3.40	2.00	3.27	1.15	59.65	2.0	0.0015	2.00	14.56	0.030	7.14	4.95	0.69	1.50	7.43
A2-1	250.50	61.01	3.40	57.61	60.16	0.0015	57.23	2.93	2.00	3.17	1.48	59.09	1.9	0.0015	2.00	15.60	0.030	8.62	7.34	0.85	1.74	12.76
A2-5	5.60	60.16	2.93	57.23	60.18	0.2482	55.84	4.34	2.00	3.64	0.37	57.60	2.6	0.2482	2.00	13.72	0.025	3.65	1.01	0.28	12.63	12.80
A2-2	257.00	60.18	4.34	55.84	60.98	0.0020	55.33	5.65	7.00	5.00	3.02	58.86	1.3	0.0020	2.00	24.36	0.025	20.51	39.38	1.92	4.10	161.54
A2-3	582.00	60.98	5.65	55.33	60.40	0.0020	54.17	6.23	8.00	5.94	3.09	58.42	2.6	0.0020	2.00	30.60	0.030	21.82	43.82	2.01	3.53	154.64
<b>NORTH</b>																						
C2-3	882.00	57.50	4.00	53.50	57.50	0.0020	51.75	5.75	4.00	4.88	3.32	56.82	0.7	0.0020	2.00	20.00	0.030	18.85	35.32	1.87	3.36	118.80
P1	64.00	57.50	4.00	51.75	57.50	0.0100	51.11	4.00	4.00	4.00	2.46	54.21	1.5	0.0100	NA	4.00	0.011	7.21	8.11	1.12	14.64	118.72
C2-5	106.00	53.61	2.50	51.11	50.50	0.0293	48.00	2.50	5.00	2.50	1.29	52.40	1.2	0.0293	4.00	25.00	0.025	15.64	13.11	0.84	9.08	118.94
C1SCCN1	285.00	60.00	1.50	58.50	60.00	0.0033	57.55	2.45	3.00	1.98	0.40	58.90	1.1	0.0033	2.00	9.00	0.030	4.79	1.52	0.32	1.33	2.03
C1SCCN2	287.50	60.00	1.50	58.50	60.00	0.0033	57.55	2.45	3.00	1.98	0.40	58.90	1.1	0.0033	2.00	9.00	0.030	4.79	1.52	0.32	1.33	2.02
P2	72.00	60.00	1.50	54.39	60.00	0.0150	53.31	1.50	1.50	1.50	0.53	54.92	1.0	0.0150	NA	1.50	0.011	1.91	0.56	0.29	7.31	4.08
C1SCCS1	280.00	60.00	1.50	58.50	60.00	0.0033	57.58	2.42	3.00	1.96	0.41	58.91	1.1	0.0033	2.00	9.00	0.030	4.83	1.57	0.32	1.34	2.10
C1SCCS2	280.00	60.00	1.50	58.50	60.00	0.0033	57.58	2.42	3.00	1.96	0.41	58.91	1.1	0.0033	2.00	9.00	0.030	4.83	1.57	0.32	1.34	2.10
P3	72.00	60.00	1.50	55.41	60.00	0.0150	54.33	1.50	1.50	1.50	0.53	55.94	1.0	0.0150	NA	1.50	0.011	1.91	0.56	0.29	7.31	4.08
<b>WEST</b>																						
2CC	650.00	57.70	3.20	54.50	59.94	0.0020	53.20	6.74	0.00	4.97	1.46	55.96	1.7	0.0020	3.00	19.20	0.030	9.23	6.39	0.69	1.74	11.12

*Chute ID	Length (FT)	Beginning			Ending				Trapezoidal Channel													
		Existing Elev	Depth (FT)	FL	Existing Elev	Slope (FT/FT)	FL	Depth (FT)	Base Width (FT)	Avg Channel Depth	**Avg Channel Flow Depth (FT)	***Hydraulic Grade Elev	Freeboard (FT)	Bottom Slope (FT/FT)	Side Slope	Top Width (FT)	Manning n	Wetted Perimeter (FT)	Area (SF)	Hydraulic Radius	Velocity (FPS)	Qp (CFS)
SE	450.00	176.00	2.00	174.00	63.54	0.2500	61.54	2.00	5.00	2.00	0.83	174.83	1.2	0.2500	4.00	21.00	0.025	11.84	6.91	0.58	20.80	143.62
SE1	62.00	63.54	2.00	61.54	58.54	0.0806	56.54	2.00	5.00	2.00	1.10	62.64	0.9	0.0806	4.00	21.00	0.025	14.07	10.34	0.73	13.78	142.47
S	451.00	176.00	2.00	174.00	61.25	0.2500	61.25	0.00	5.00	1.00	0.86	174.86	1.1	0.2500	4.00	21.00	0.025	12.09	7.26	0.60	21.21	153.92
SW	404.00	176.00	2.00	174.00	77.00	0.2500	73.00	4.00	5.00	3.00	0.81	174.81	1.2	0.2500	4.00	21.00	0.025	11.68	6.67	0.57	20.52	136.97
W	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.93	174.93	1.1	0.2500	4.00	21.00	0.025	12.67	8.11	0.64	22.13	179.50
NW	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.72	174.72	1.3	0.2500	4.00	21.00	0.025	10.94	5.67	0.52	19.24	109.15
NE	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.79	174.79	1.2	0.2500	4.00	21.00	0.025	11.51	6.45	0.56	20.24	130.49
E	456.00	176.00	2.00	174.00	60.00	0.2500	60.00	0.00	5.00	1.00	0.85	174.85	1.2	0.2500	4.00	21.00	0.025	12.01	7.14	0.59	21.07	150.44
C1-4	76.00	51.80	2.00	49.80	33.00	0.2474	31.00	2.00	5.00	2.50	1.21	51.01	0.8	0.2474	4.00	21.00	0.025	14.98	11.91	0.79	25.44	302.89
C2-4	52.00	50.00	2.00	48.00	33.00	0.3269	31.00	2.00	5.00	2.00	0.70	48.70	1.3	0.3269	4.00	21.00	0.025	10.77	5.46	0.51	21.65	118.28
P2-1	60.00	56.15	1.50	53.31	32.50	0.3718	31.00	1.50	2.00	1.50	0.17	53.48	1.3	0.3718	3.00	11.00	0.025	3.08	0.43	0.14	9.74	4.16
P3-1	60.00	56.15	1.50	54.65	32.50	0.3942	31.00	1.50	2.00	1.50	0.17	54.82	1.3	0.3942	3.00	11.00	0.025	3.08	0.43	0.14	10.03	4.28
A2-4	250.00	56.17	2.00	54.17	38.75	0.0697	36.75	2.00	10.00	2.00	0.91	55.08	1.1	0.0697	4.00	26.00	0.025	17.50	12.41	0.71	12.51	155.29
SW-1	266.00	72.50	2.00	70.50	38.75	0.1269	36.75	2.00	5.00	2.00	0.96	71.46	1.0	0.1269	4.00	21.00	0.025	12.92	8.49	0.66	16.05	136.17
CC	160.00	55.20	2.00	53.20	38.75	0.1028	36.75	2.00	5.00	2.00	0.26	54.46	1.7	0.1028	4.00	21.00	0.025	7.14	1.57	0.22	6.96	10.93











\*Chutes-Precast Interlocking Articulating Concrete Blocks  
 \*\* Avg Channel Flow Depth Determined by HydroCAD  
 \*\*\* Hydraulic Grade Elevation Determined by HydroCAD

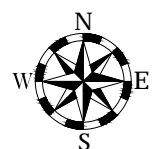
**APPENDIX 6B.11**  
**FIGURE 1 OVERALL SOUTHERN DRAINAGE PLAN**





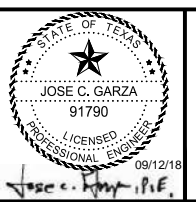
**LEGEND:**

-  EXISTING POWER POLE
-  EXISTING LANDFILL GAS VENT
-  EXISTING GROUND WATER MONITOR WELL
-  EXISTING FENCE
-  EXISTING CONTOUR
-  EXISTING PERMIT BOUNDARY LIMITS
-  PROPOSED FINAL COVER CONTOURS
-  PROPOSED STORMWATER LETDOWN STRUCTURE (CHUTE)
-  TOP OF SLOPE
-  TOE OF SLOPE



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NUMBER	REVISION	DATE	DRAWN	DESIGNED	REVIEWED



Hanson No. 16L0438		
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LAYOUT	DT	09/12/2018
DRAWN	DT	09/12/2018
REVIEWED	JMR	09/12/2018



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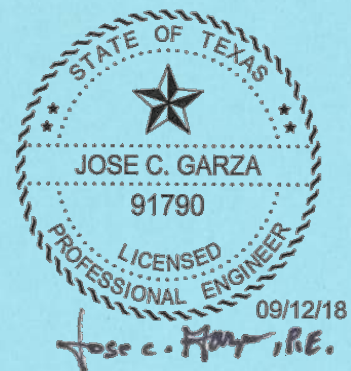
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TBPG F-50556  
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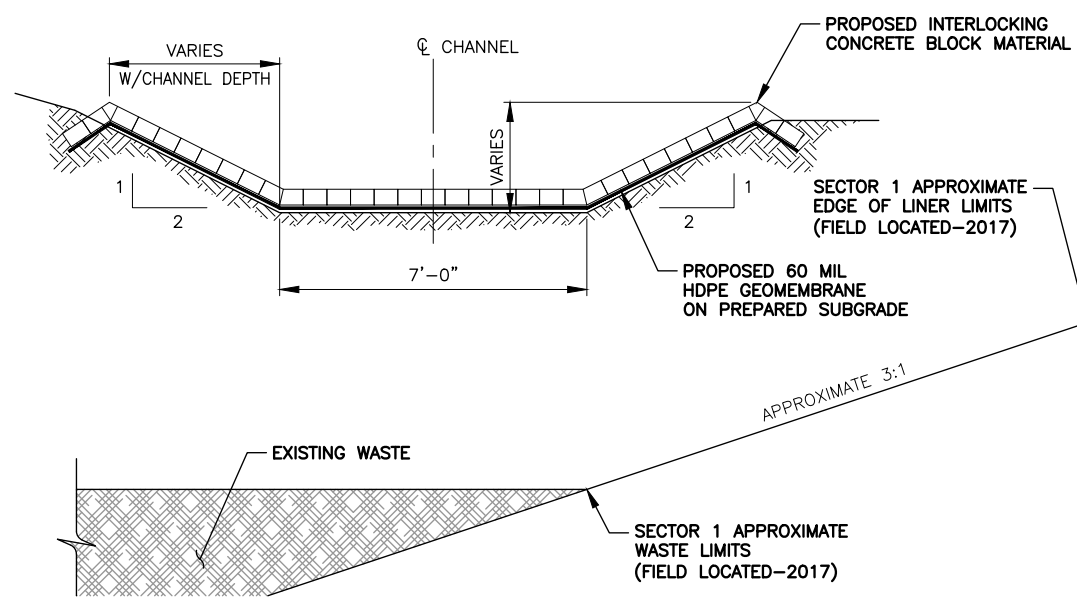
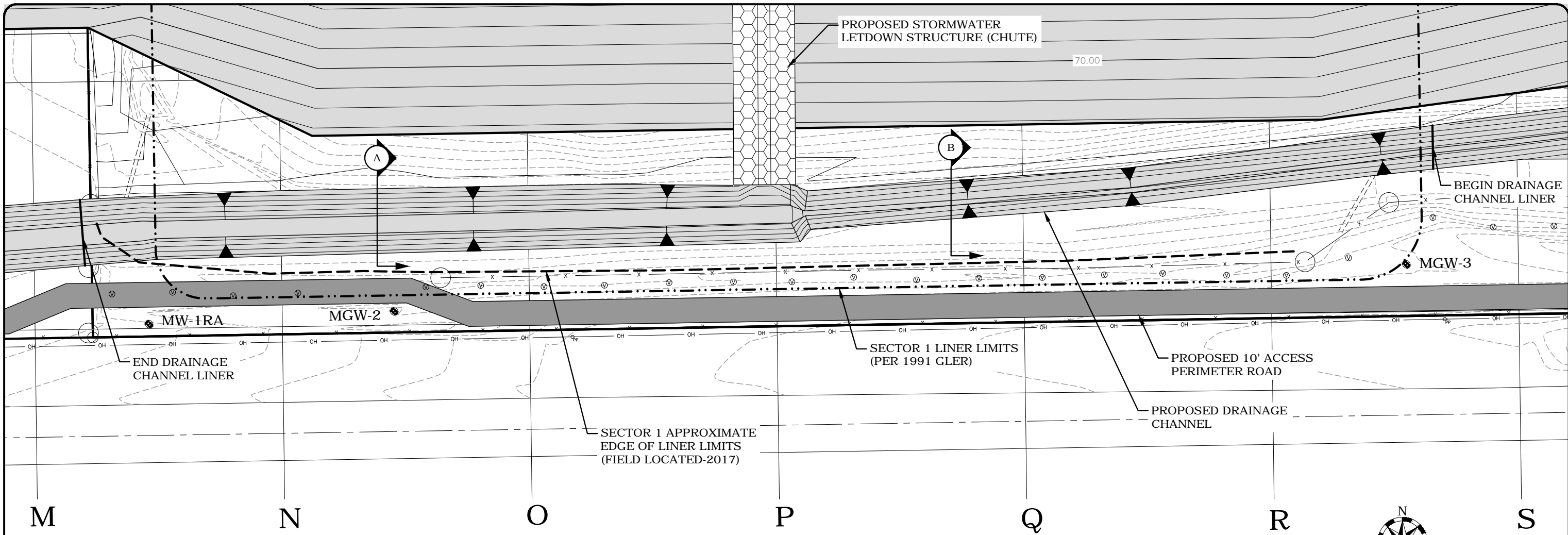
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PART III, ATTACHMENT 6, APPENDIX 6B.11  
OVERALL SOUTHERN DRAINAGE PLAN  
CITY OF KINGSVILLE LANDFILL  
MSW PERMIT No. 235-C  
KINGSVILLE, TEXAS  
KLEBERG COUNTY, TEXAS

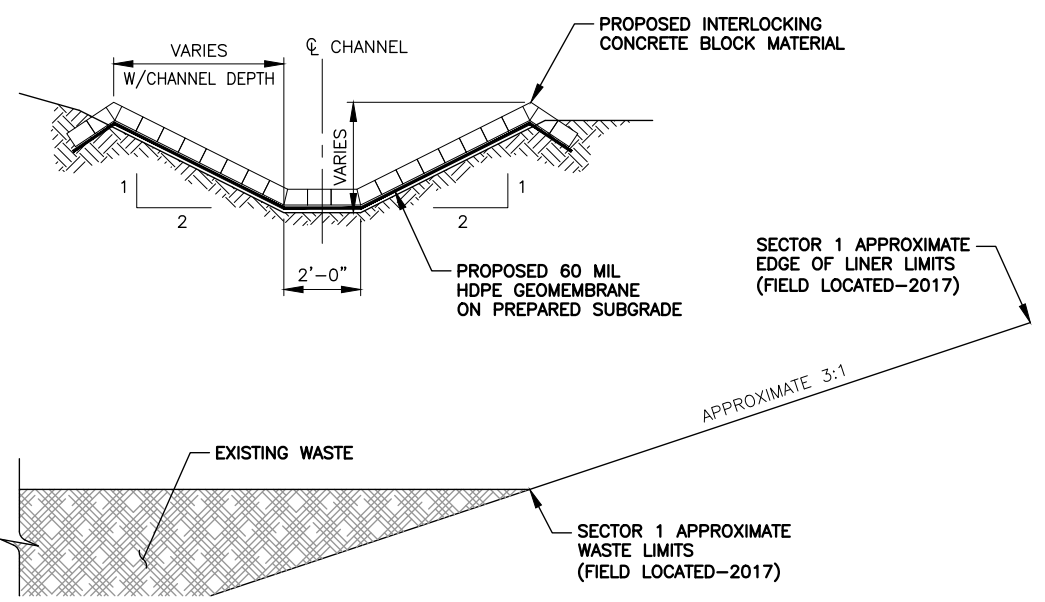
FIGURE:  
III.6-6B.11

APPENDIX 6B.11.1  
FIGURE 2 ENLARGED SOUTHERN DRAINAGE PLAN

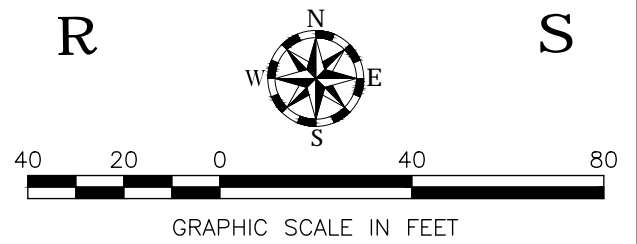




**SECTION A**  
SCALE: NT.S.



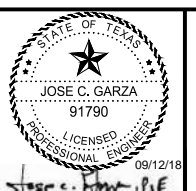
**SECTION B**  
SCALE: NT.S.



- LEGEND:**
- ⊕ EXISTING POWER POLE
  - ⊙ EXISTING LANDFILL GAS VENT
  - ⊗ EXISTING GROUND WATER MONITOR WELL
  - x — EXISTING FENCE
  - - - 60.00 - - - EXISTING CONTOUR
  - 150 — EXISTING PERMIT BOUNDARY LIMITS
  - ===== PROPOSED FINAL COVER CONTOURS
  - ===== PROPOSED STORMWATER LETDOWN STRUCTURE (CHUTE)
  - ▲ — TOP OF SLOPE
  - ▼ — TOE OF SLOPE

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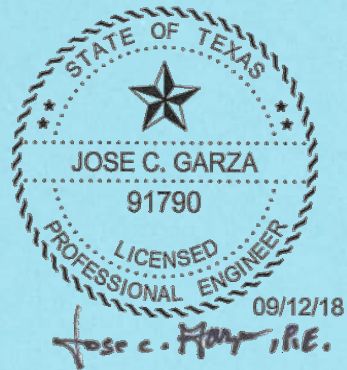
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PART III, ATTACHMENT 6, APPENDIX 6B.11.1  
**ENLARGED SOUTHERN DRAINAGE PLAN**  
**CITY OF KINGSVILLE LANDFILL**  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

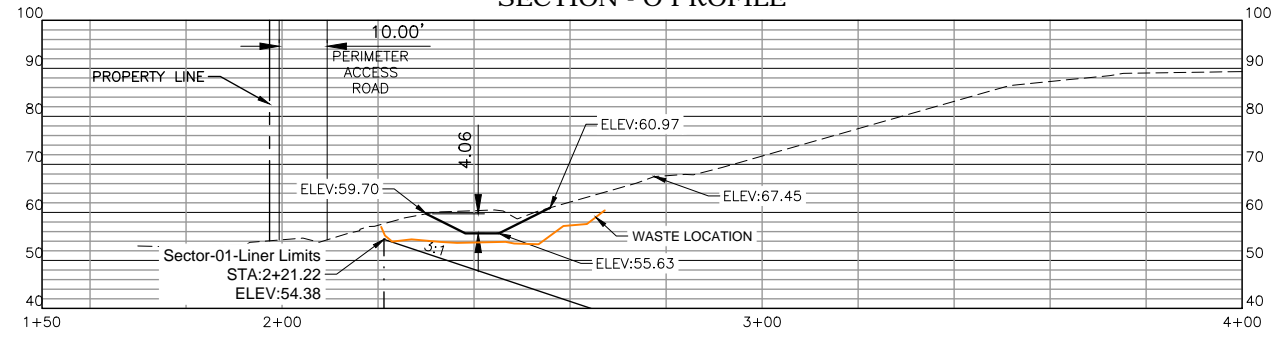
**FIGURE:**  
**III.6-6B.11.1**

APPENDIX 6B.11.2  
FIGURE 3 CROSS SECTIONS

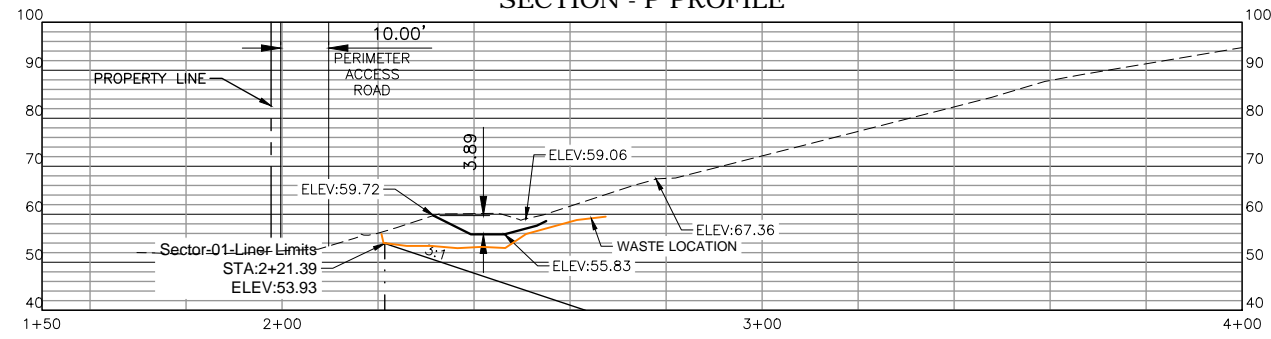


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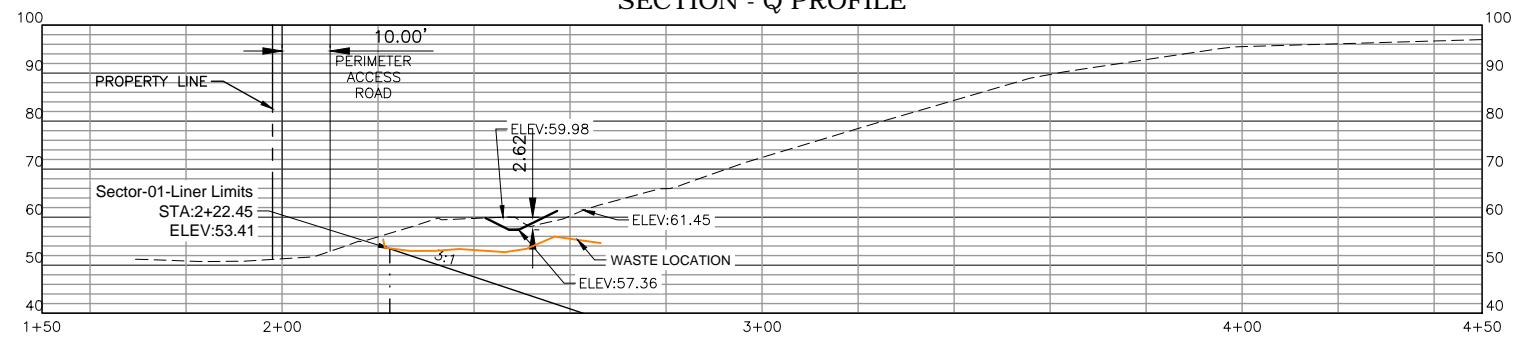
SECTION - O PROFILE



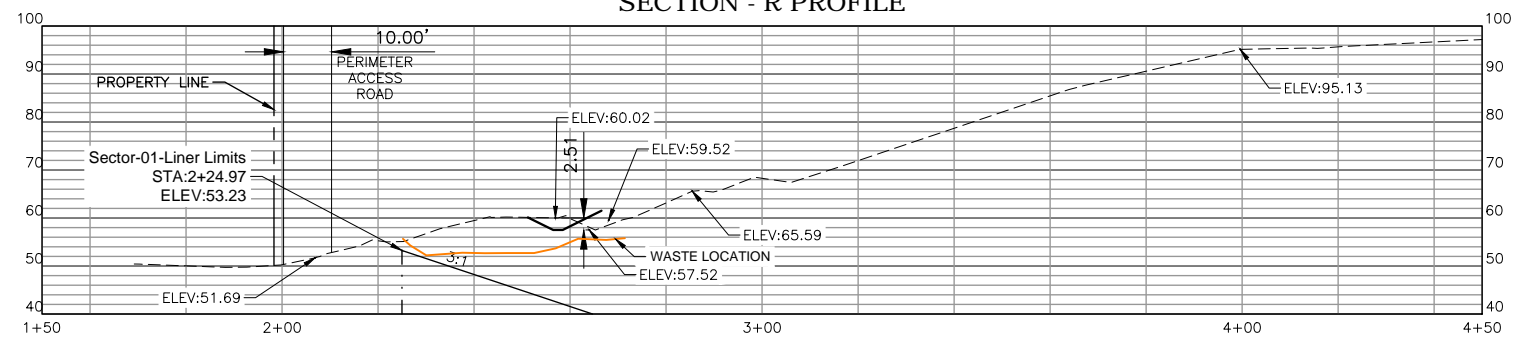
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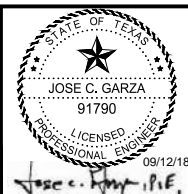
SECTION - Q PROFILE



SECTION - R PROFILE



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DRAWN	DT	09/12/2018
REVIEWED	JMR	09/12/2018

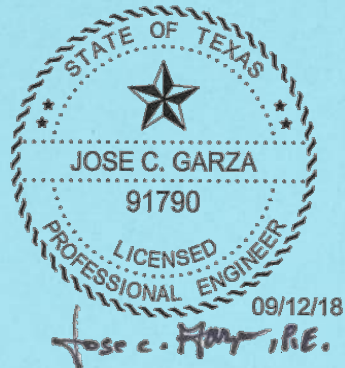
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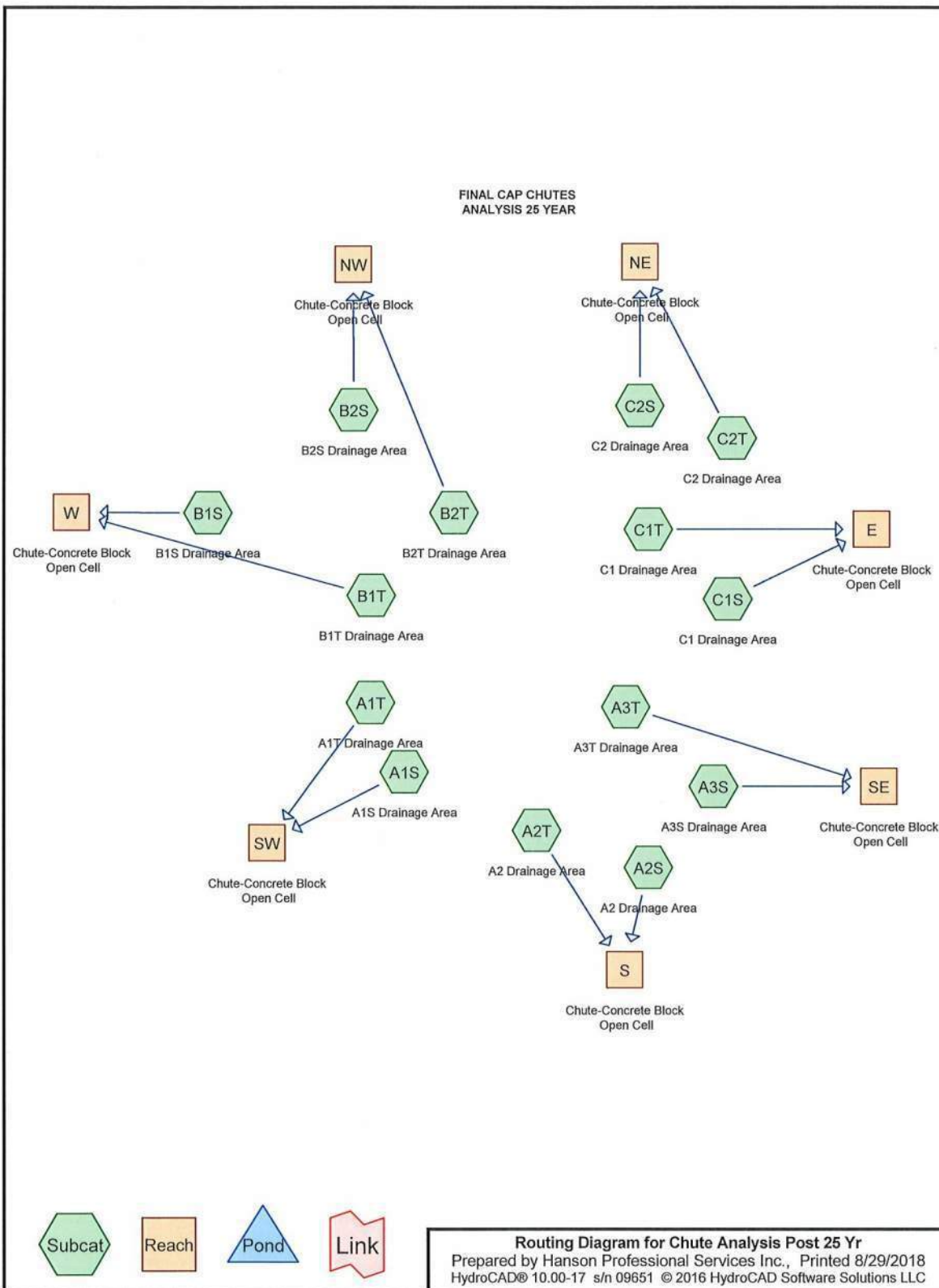
PART III, ATTACHMENT 6, APPENDIX 6B.11.2  
**CROSS SECTIONS**  
**CITY OF KINGSVILLE LANDFILL**  
 MSW PERMIT No. 235-C  
 KINGSVILLE, TEXAS  
 KLEBERG COUNTY, TEXAS

**FIGURE:**  
**III.6-6B.11.2**

APPENDIX 6B.12  
HYDROCAD MODEL 25 YEAR POST DEVELOPMENT CHUTES







**Chute Analysis Post 25 Yr**

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Page 2

**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
119.627	79	50-75% Grass cover, Fair, HSG C (A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1T, C2S, C2T)
<b>119.627</b>	<b>79</b>	<b>TOTAL AREA</b>

**Chute Analysis Post 25 Yr**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
119.627	HSG C	A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1T, C2S, C2T
0.000	HSG D	
0.000	Other	
<b>119.627</b>		<b>TOTAL AREA</b>

**Chute Analysis Post 25 Yr**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	119.627	0.000	0.000	119.627	50-75% Grass cover, Fair	A1S, A1T, A2S, A2T, A3S, A3T, B1S, B1T, B2S, B2T, C1S, C1T, C2S, C2T
<b>0.000</b>	<b>0.000</b>	<b>119.627</b>	<b>0.000</b>	<b>0.000</b>	<b>119.627</b>	<b>TOTAL AREA</b>	

**Chute Analysis Post 25 Yr**

*Type III 24-hr 25-Year Rainfall=8.70"*

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Page 5

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment A1S: A1S Drainage Area</b>	Runoff Area=8.009 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=49.80 cfs 4.113 af
<b>Subcatchment A1T: A1T Drainage Area</b>	Runoff Area=7.425 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=46.16 cfs 3.813 af
<b>Subcatchment A2S: A2 Drainage Area</b>	Runoff Area=12.241 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=76.11 cfs 6.287 af
<b>Subcatchment A2T: A2 Drainage Area</b>	Runoff Area=5.120 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=31.83 cfs 2.629 af
<b>Subcatchment A3S: A3S Drainage Area</b>	Runoff Area=10.760 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=66.90 cfs 5.526 af
<b>Subcatchment A3T: A3T Drainage Area</b>	Runoff Area=7.489 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=1,050' Tc=16.7 min CN=79 Runoff=38.81 cfs 3.846 af
<b>Subcatchment B1S: B1S Drainage Area</b>	Runoff Area=14.884 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=92.54 cfs 7.644 af
<b>Subcatchment B1T: B1T Drainage Area</b>	Runoff Area=7.499 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=950' Tc=16.0 min CN=79 Runoff=39.52 cfs 3.851 af
<b>Subcatchment B2S: B2S Drainage Area</b>	Runoff Area=8.806 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=54.75 cfs 4.522 af
<b>Subcatchment B2T: B2T Drainage Area</b>	Runoff Area=4.309 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=850' Tc=13.7 min CN=79 Runoff=24.07 cfs 2.213 af
<b>Subcatchment C1S: C1 Drainage Area</b>	Runoff Area=11.506 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=71.54 cfs 5.909 af
<b>Subcatchment C1T: C1 Drainage Area</b>	Runoff Area=6.292 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=800' Tc=12.5 min CN=79 Runoff=36.29 cfs 3.231 af
<b>Subcatchment C2S: C2 Drainage Area</b>	Runoff Area=10.038 ac 0.00% Impervious Runoff Depth=6.16" Tc=10.0 min CN=79 Runoff=62.41 cfs 5.155 af
<b>Subcatchment C2T: C2 Drainage Area</b>	Runoff Area=5.249 ac 0.00% Impervious Runoff Depth=6.16" Flow Length=800' Tc=12.5 min CN=79 Runoff=30.27 cfs 2.696 af
<b>Reach E: Chute-Concrete Block</b>	Avg. Flow Depth=0.71' Max Vel=19.08 fps Inflow=106.93 cfs 9.140 af n=0.025 L=456.0' S=0.2500 ' /' Capacity=877.30 cfs Outflow=106.72 cfs 9.140 af
<b>Reach NE: Chute-Concrete Block</b>	Avg. Flow Depth=0.66' Max Vel=18.27 fps Inflow=91.93 cfs 7.851 af n=0.025 L=456.0' S=0.2500 ' /' Capacity=877.30 cfs Outflow=91.74 cfs 7.851 af

**Chute Analysis Post 25 Yr**

*Type III 24-hr 25-Year Rainfall=8.70"*

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**Reach NW: Chute-Concrete Block** Avg. Flow Depth=0.60' Max Vel=17.38 fps Inflow=77.52 cfs 6.735 af  
n=0.025 L=456.0' S=0.2500 '/' Capacity=877.30 cfs Outflow=77.39 cfs 6.735 af

**Reach S: Chute-Concrete Block** Avg. Flow Depth=0.72' Max Vel=19.13 fps Inflow=107.94 cfs 8.916 af  
n=0.025 L=451.0' S=0.2500 '/' Capacity=877.30 cfs Outflow=107.71 cfs 8.916 af

**Reach SE: Chute-Concrete Block** Avg. Flow Depth=0.69' Max Vel=18.76 fps Inflow=100.71 cfs 9.372 af  
n=0.025 L=441.7' S=0.2500 '/' Capacity=877.36 cfs Outflow=100.58 cfs 9.372 af

**Reach SW: Chute-Concrete Block** Avg. Flow Depth=0.67' Max Vel=18.50 fps Inflow=95.96 cfs 7.926 af  
n=0.025 L=406.0' S=0.2500 '/' Capacity=877.30 cfs Outflow=95.76 cfs 7.926 af

**Reach W: Chute-Concrete Block** Avg. Flow Depth=0.78' Max Vel=20.06 fps Inflow=127.46 cfs 11.495 af  
n=0.025 L=456.0' S=0.2500 '/' Capacity=877.30 cfs Outflow=127.28 cfs 11.495 af

**Total Runoff Area = 119.627 ac Runoff Volume = 61.436 af Average Runoff Depth = 6.16"**  
**100.00% Pervious = 119.627 ac 0.00% Impervious = 0.000 ac**

**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A1S: A1S Drainage Area**

Use Conservative Value of Tc=10 min.

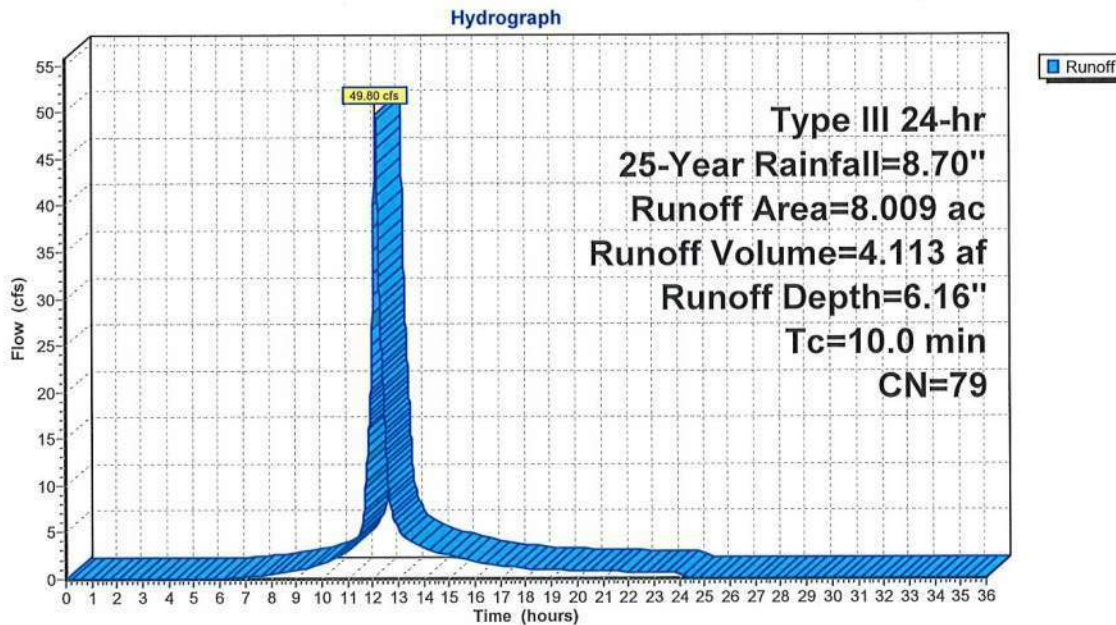
Runoff = 49.80 cfs @ 12.14 hrs, Volume= 4.113 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
8.009	79	50-75% Grass cover, Fair, HSG C
8.009		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1S-Chute Flow Evaluation

**Subcatchment A1S: A1S Drainage Area**



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A1T: A1T Drainage Area**

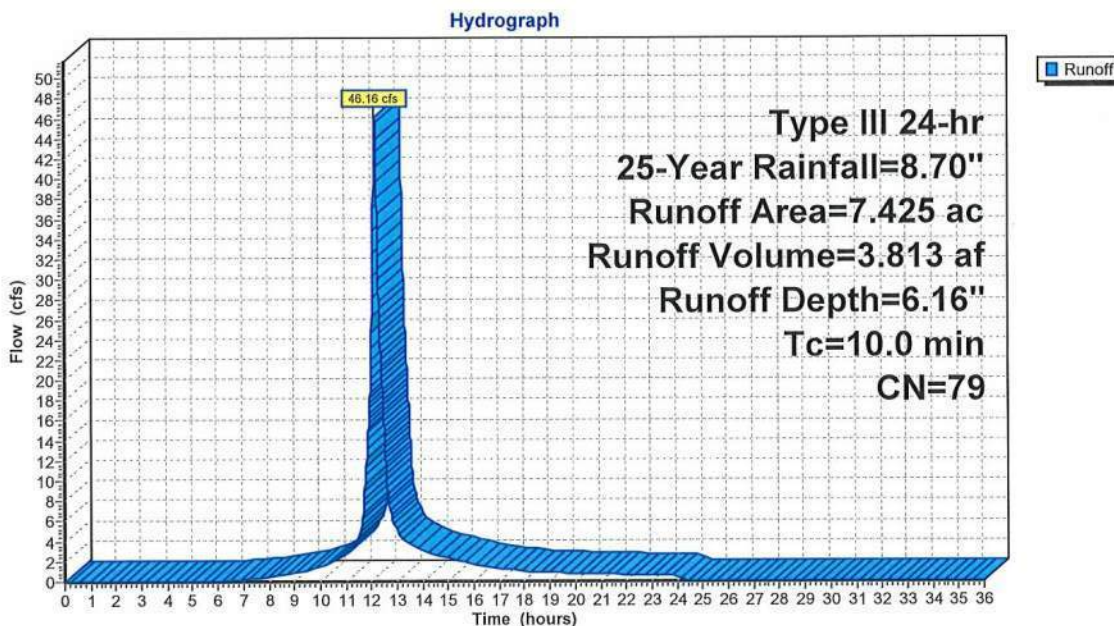
Runoff = 46.16 cfs @ 12.14 hrs, Volume= 3.813 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
7.425	79	50-75% Grass cover, Fair, HSG C
7.425		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A1T-Chute Flow Evaluation

**Subcatchment A1T: A1T Drainage Area**





**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A2S: A2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 76.11 cfs @ 12.14 hrs, Volume= 6.287 af, Depth= 6.16"

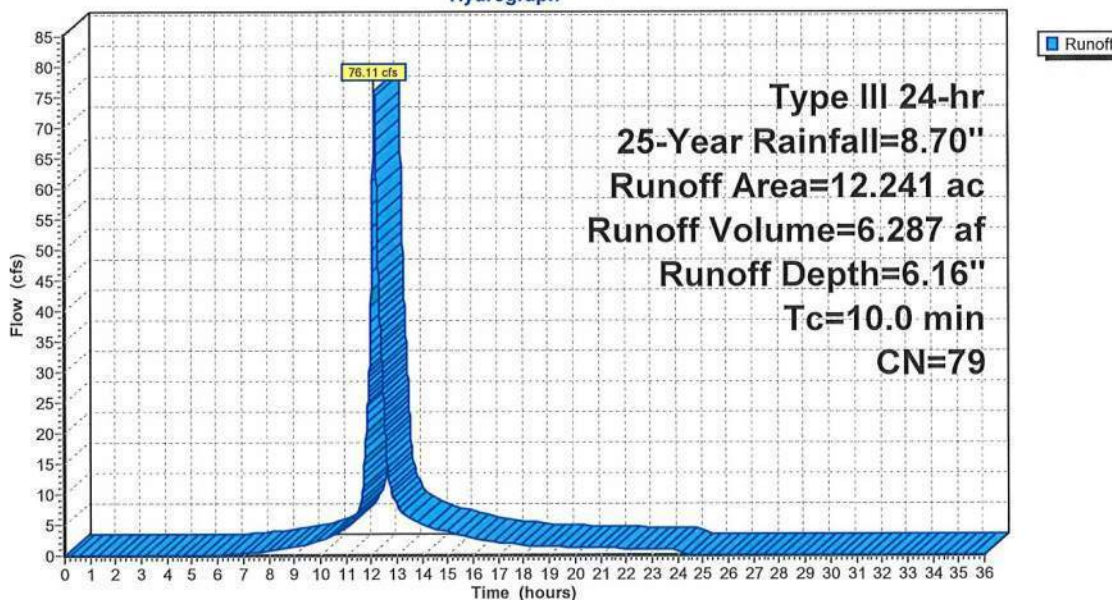
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
12.241	79	50-75% Grass cover, Fair, HSG C
12.241		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2S: A2 Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A2T: A2 Drainage Area**

Runoff = 31.83 cfs @ 12.14 hrs, Volume= 2.629 af, Depth= 6.16"

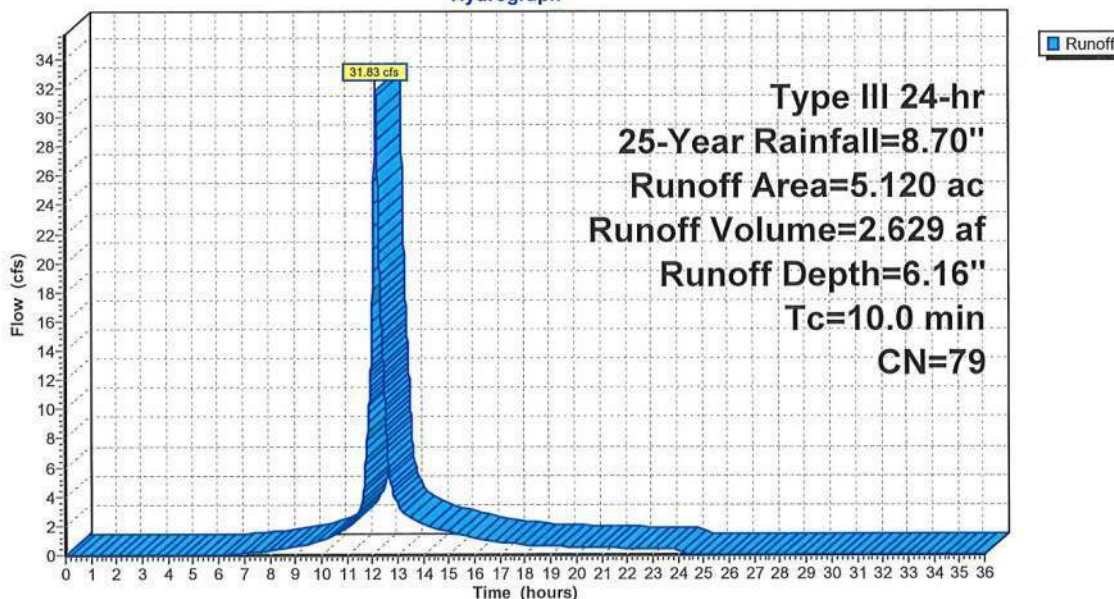
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
5.120	79	50-75% Grass cover, Fair, HSG C
5.120		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A2 Drainage Area

**Subcatchment A2T: A2 Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A3S: A3S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 66.90 cfs @ 12.14 hrs, Volume= 5.526 af, Depth= 6.16"

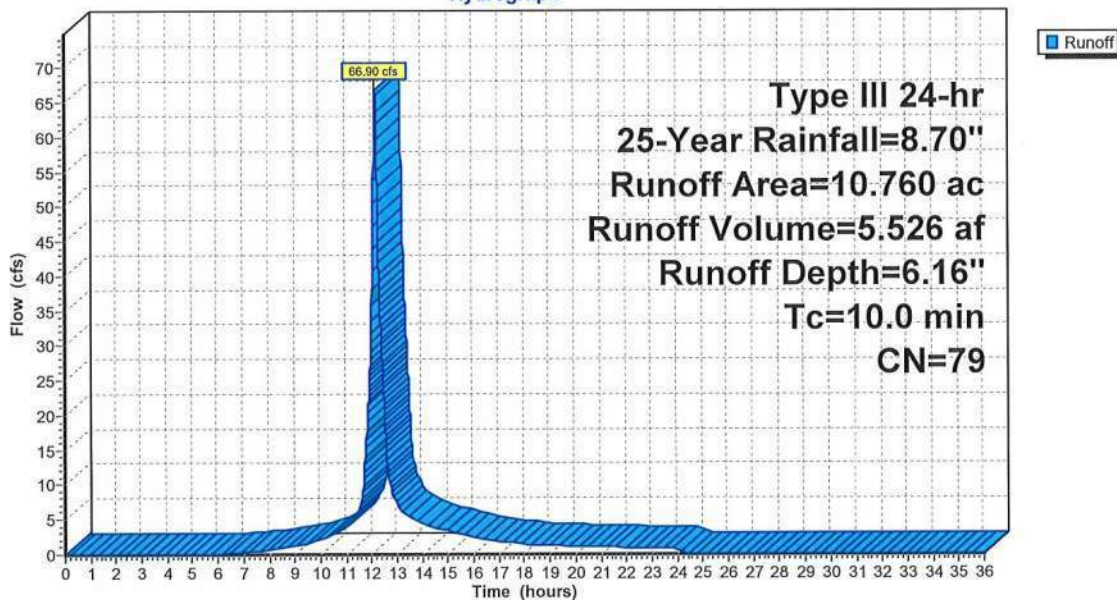
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
10.760	79	50-75% Grass cover, Fair, HSG C
10.760		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, A3S-Chute Flow Evaluation

**Subcatchment A3S: A3S Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment A3T: A3T Drainage Area**

Runoff = 38.81 cfs @ 12.23 hrs, Volume= 3.846 af, Depth= 6.16"

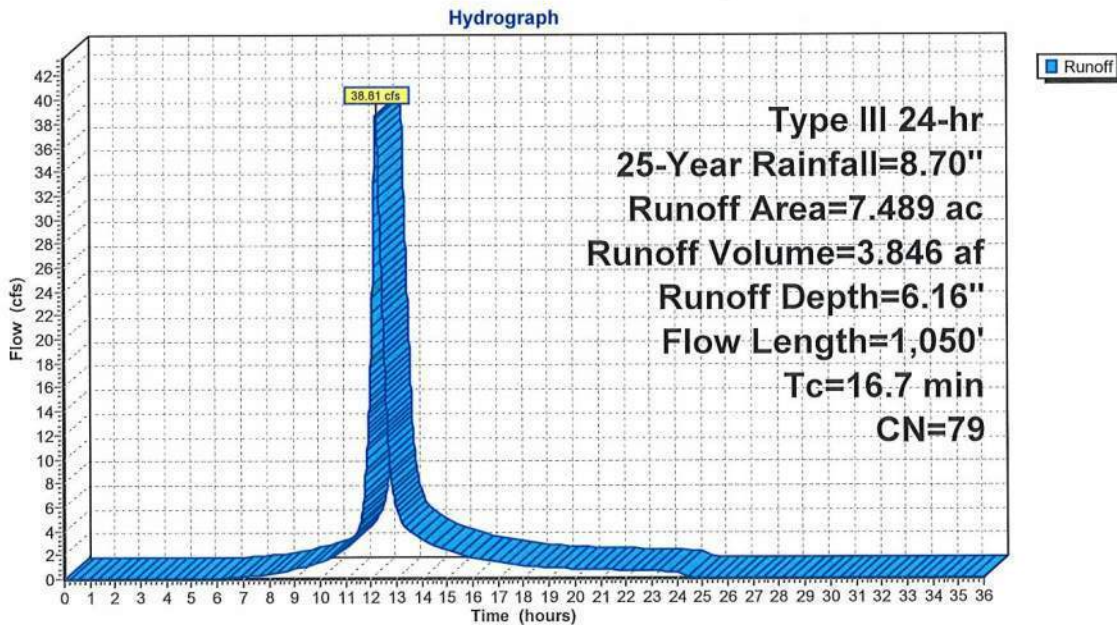
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
7.489	79	50-75% Grass cover, Fair, HSG C
7.489		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.6	750		1.30		Direct Entry, A3T-Chute Flow Evaluation
7.1	300		0.70		Direct Entry,
16.7	1,050				Total

**Subcatchment A3T: A3T Drainage Area**



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B1S: B1S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 92.54 cfs @ 12.14 hrs, Volume= 7.644 af, Depth= 6.16"

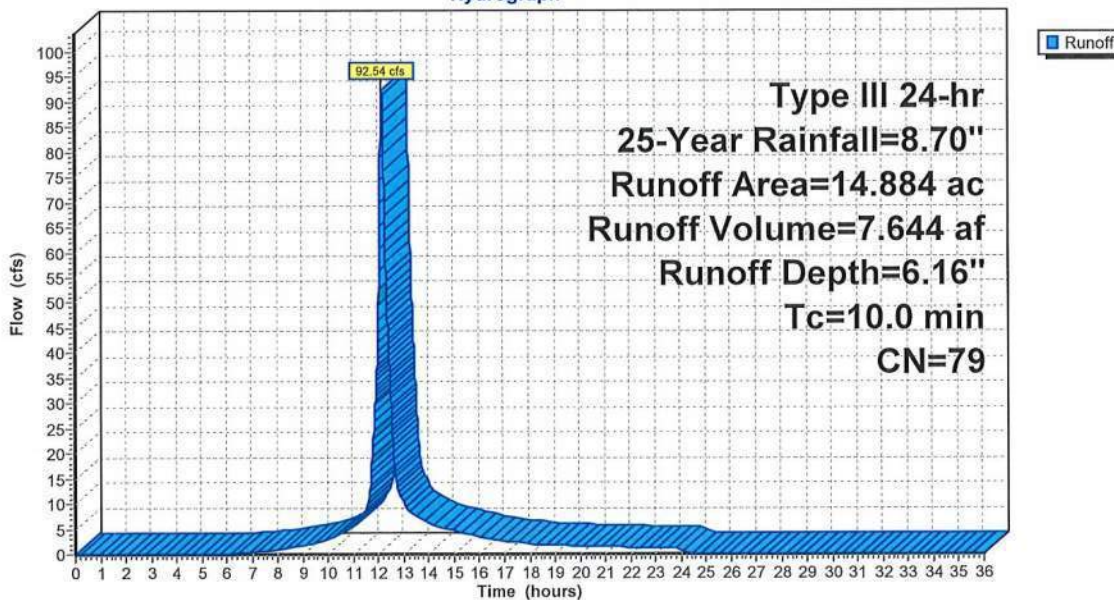
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
14.884	79	50-75% Grass cover, Fair, HSG C
14.884		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B1S-Chute Flow Evaluation

**Subcatchment B1S: B1S Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B1T: B1T Drainage Area**

Runoff = 39.52 cfs @ 12.21 hrs, Volume= 3.851 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

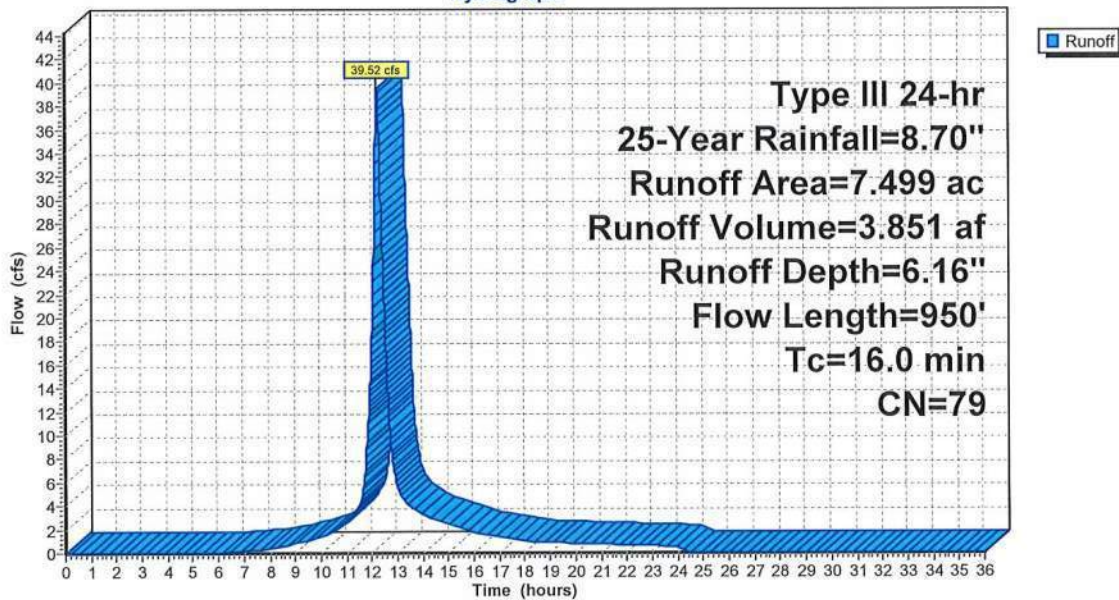
Area (ac)	CN	Description
7.499	79	50-75% Grass cover, Fair, HSG C
7.499		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B1T-Chute Flow Evaluation
8.3	350		0.70		Direct Entry,
16.0	950				Total

**Subcatchment B1T: B1T Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B2S: B2S Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 54.75 cfs @ 12.14 hrs, Volume= 4.522 af, Depth= 6.16"

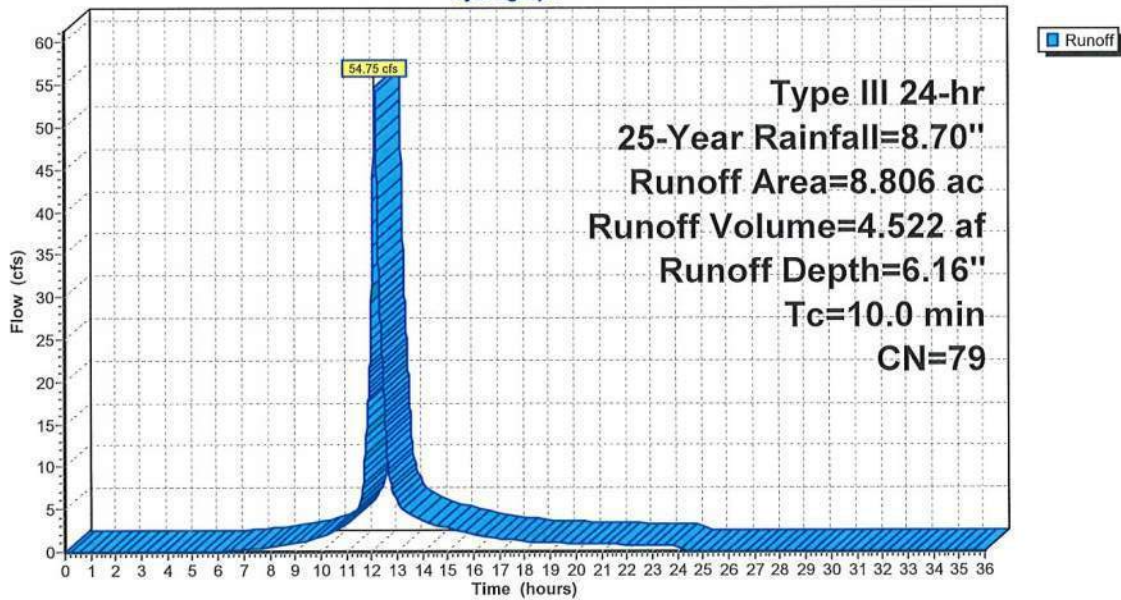
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
8.806	79	50-75% Grass cover, Fair, HSG C
8.806		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, B2S-Chute Flow Evaluation

**Subcatchment B2S: B2S Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment B2T: B2T Drainage Area**

Runoff = 24.07 cfs @ 12.19 hrs, Volume= 2.213 af, Depth= 6.16"

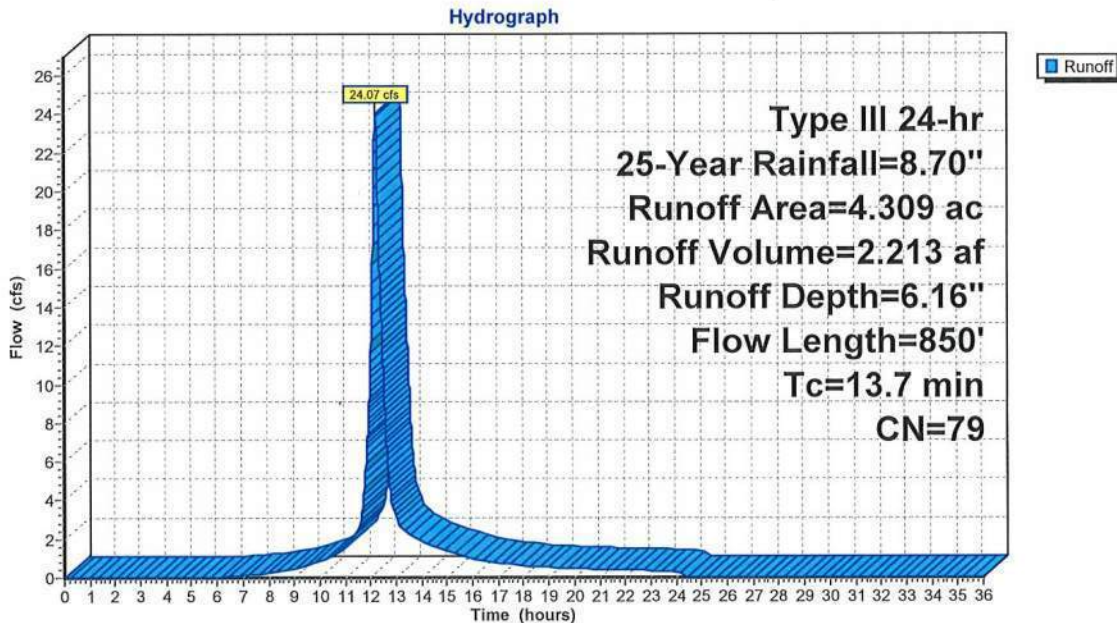
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
4.309	79	50-75% Grass cover, Fair, HSG C
4.309		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, B2T-Chute Flow Evaluation
6.0	250		0.70		Direct Entry,
13.7	850				Total

**Subcatchment B2T: B2T Drainage Area**





**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1S: C1 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 71.54 cfs @ 12.14 hrs, Volume= 5.909 af, Depth= 6.16"

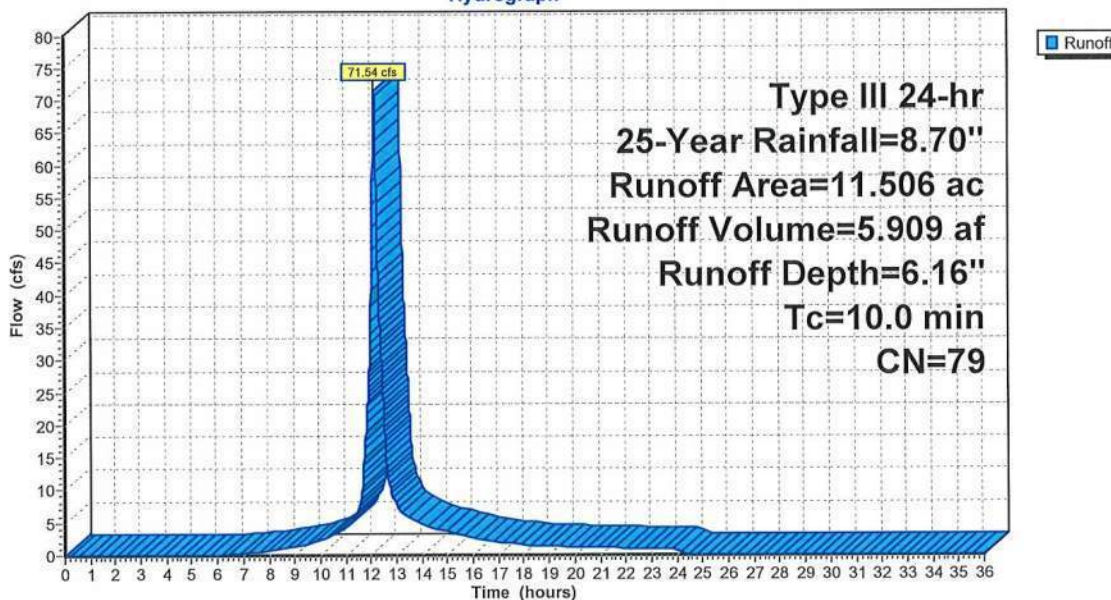
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
11.506	79	50-75% Grass cover, Fair, HSG C
11.506		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C1 Drainage Area

**Subcatchment C1S: C1 Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C1T: C1 Drainage Area**

Runoff = 36.29 cfs @ 12.17 hrs, Volume= 3.231 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

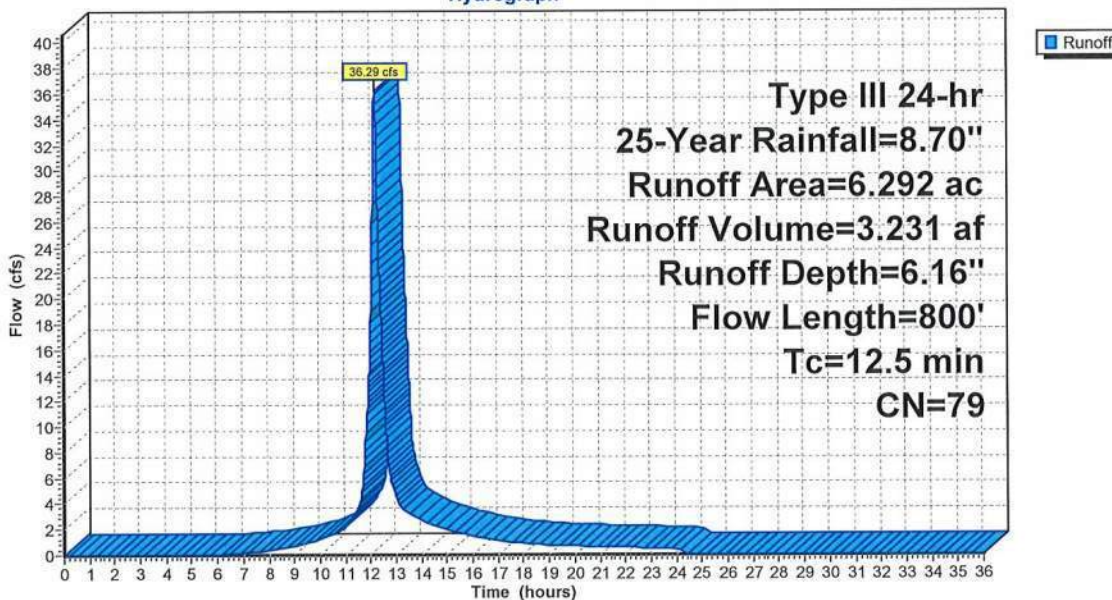
Area (ac)	CN	Description
6.292	79	50-75% Grass cover, Fair, HSG C
6.292		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C1 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800				Total

**Subcatchment C1T: C1 Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C2S: C2 Drainage Area**

Use Conservative Value of Tc=10 min.

Runoff = 62.41 cfs @ 12.14 hrs, Volume= 5.155 af, Depth= 6.16"

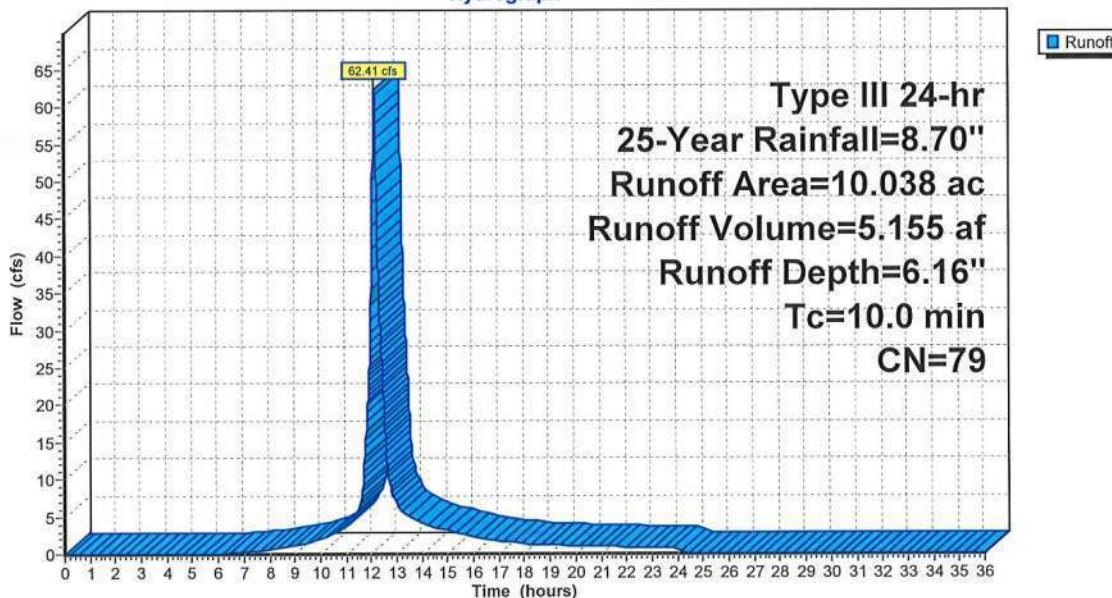
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
10.038	79	50-75% Grass cover, Fair, HSG C
10.038		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry, C2 Drainage Area

**Subcatchment C2S: C2 Drainage Area**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Subcatchment C2T: C2 Drainage Area**

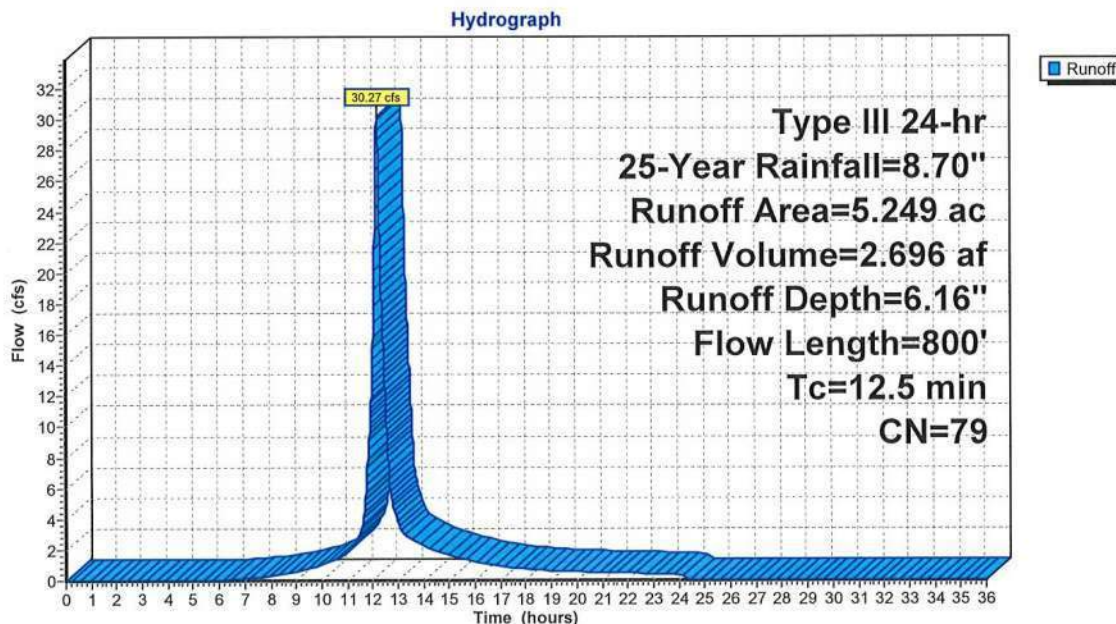
Runoff = 30.27 cfs @ 12.17 hrs, Volume= 2.696 af, Depth= 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 25-Year Rainfall=8.70"

Area (ac)	CN	Description
5.249	79	50-75% Grass cover, Fair, HSG C
5.249		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	600		1.30		Direct Entry, C2 Drainage Area
4.8	200		0.70		Direct Entry,
12.5	800				Total

**Subcatchment C2T: C2 Drainage Area**



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach E: Chute-Concrete Block Open Cell**

Inflow Area = 17.798 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 106.93 cfs @ 12.15 hrs, Volume= 9.140 af  
 Outflow = 106.72 cfs @ 12.16 hrs, Volume= 9.140 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.08 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 5.95 fps, Avg. Travel Time= 1.3 min

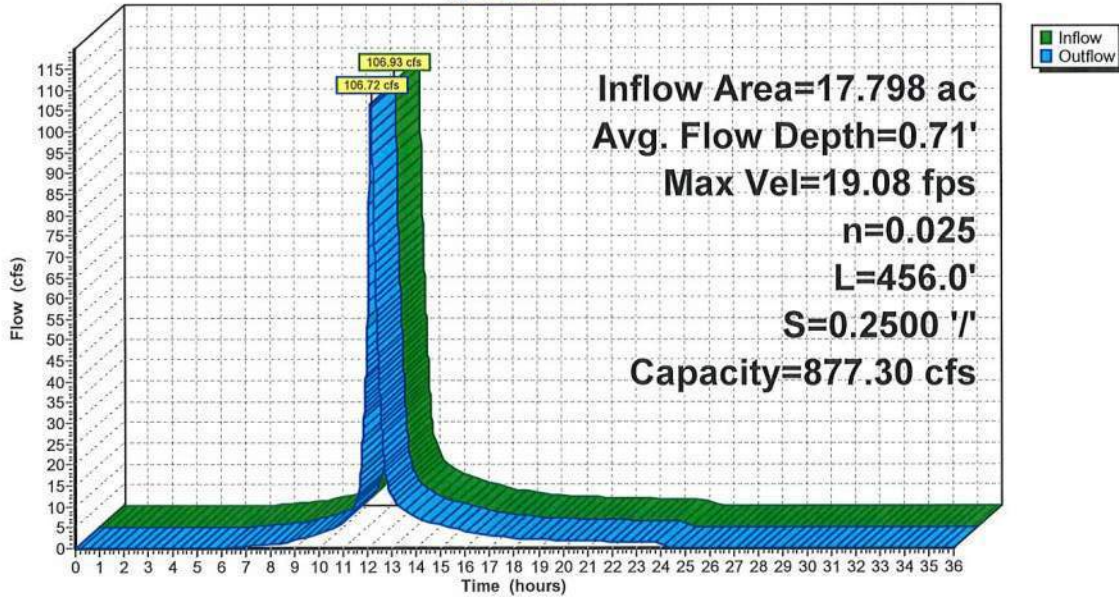
Peak Storage= 2,552 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.71'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 456.0' Slope= 0.2500 '/'  
 Inlet Invert= 172.00', Outlet Invert= 58.00'



**Reach E: Chute-Concrete Block Open Cell**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach NE: Chute-Concrete Block Open Cell**

Inflow Area = 15.287 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 91.93 cfs @ 12.15 hrs, Volume= 7.851 af  
 Outflow = 91.74 cfs @ 12.16 hrs, Volume= 7.851 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.27 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 5.65 fps, Avg. Travel Time= 1.3 min

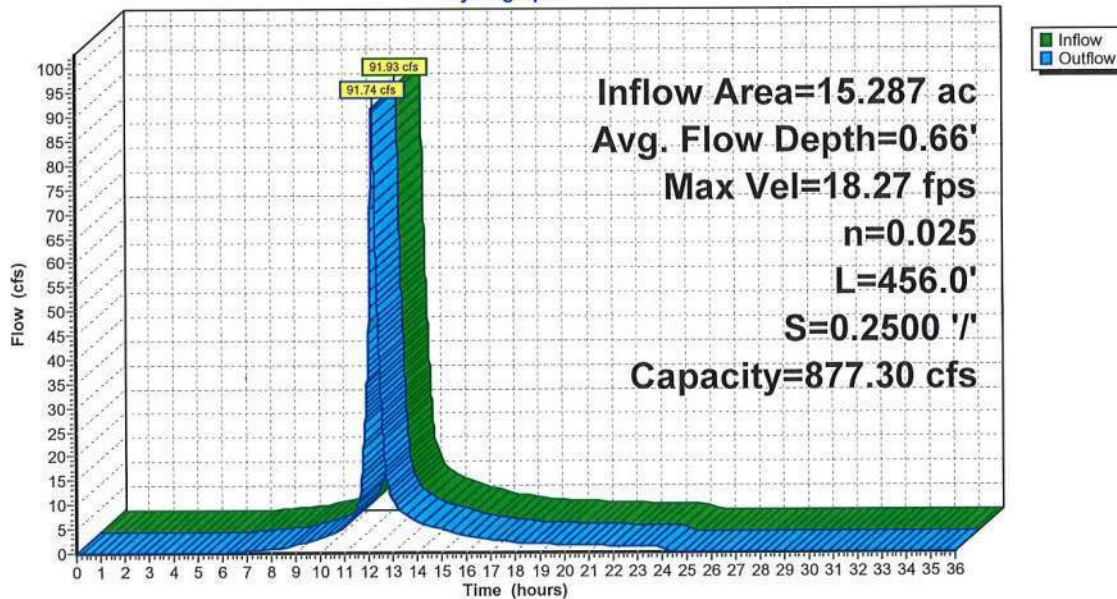
Peak Storage= 2,292 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.66'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 456.0' Slope= 0.2500 '/'  
 Inlet Invert= 172.00', Outlet Invert= 58.00'



**Reach NE: Chute-Concrete Block Open Cell**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach NW: Chute-Concrete Block Open Cell**

Inflow Area = 13.115 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 77.52 cfs @ 12.15 hrs, Volume= 6.735 af  
 Outflow = 77.39 cfs @ 12.16 hrs, Volume= 6.735 af, Atten= 0%, Lag= 0.8 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 17.38 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 5.36 fps, Avg. Travel Time= 1.4 min

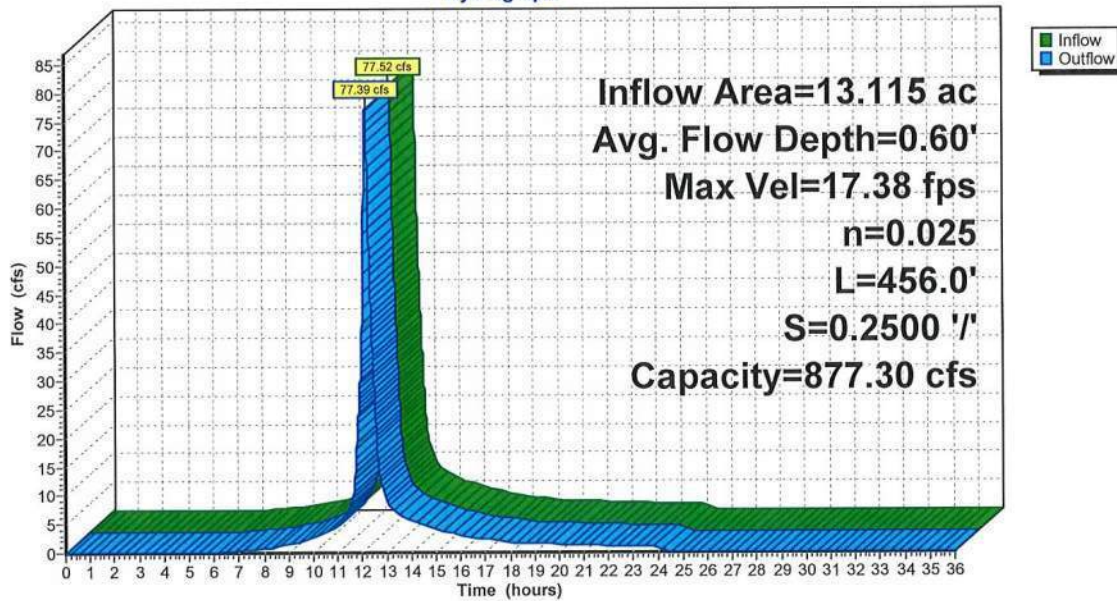
Peak Storage= 2,032 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.60'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '1' Top Width= 21.00'  
 Length= 456.0' Slope= 0.2500 '1'  
 Inlet Invert= 172.00', Outlet Invert= 58.00'



**Reach NW: Chute-Concrete Block Open Cell**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach S: Chute-Concrete Block Open Cell**

Inflow Area = 17.361 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 107.94 cfs @ 12.14 hrs, Volume= 8.916 af  
 Outflow = 107.71 cfs @ 12.15 hrs, Volume= 8.916 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 19.13 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 5.91 fps, Avg. Travel Time= 1.3 min

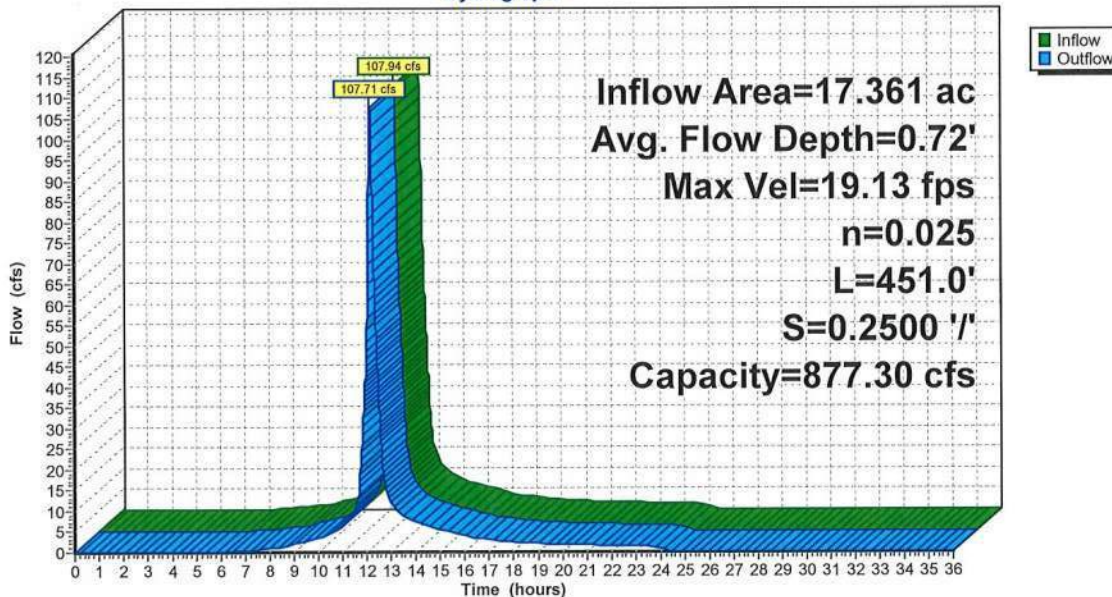
Peak Storage= 2,541 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.72'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '/' Top Width= 21.00'  
 Length= 451.0' Slope= 0.2500 '/'  
 Inlet Invert= 172.00', Outlet Invert= 59.25'



**Reach S: Chute-Concrete Block Open Cell**

Hydrograph





**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SE: Chute-Concrete Block Open Cell**

Inflow Area = 18.249 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 100.71 cfs @ 12.16 hrs, Volume= 9.372 af  
 Outflow = 100.58 cfs @ 12.17 hrs, Volume= 9.372 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.76 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.97 fps, Avg. Travel Time= 1.2 min

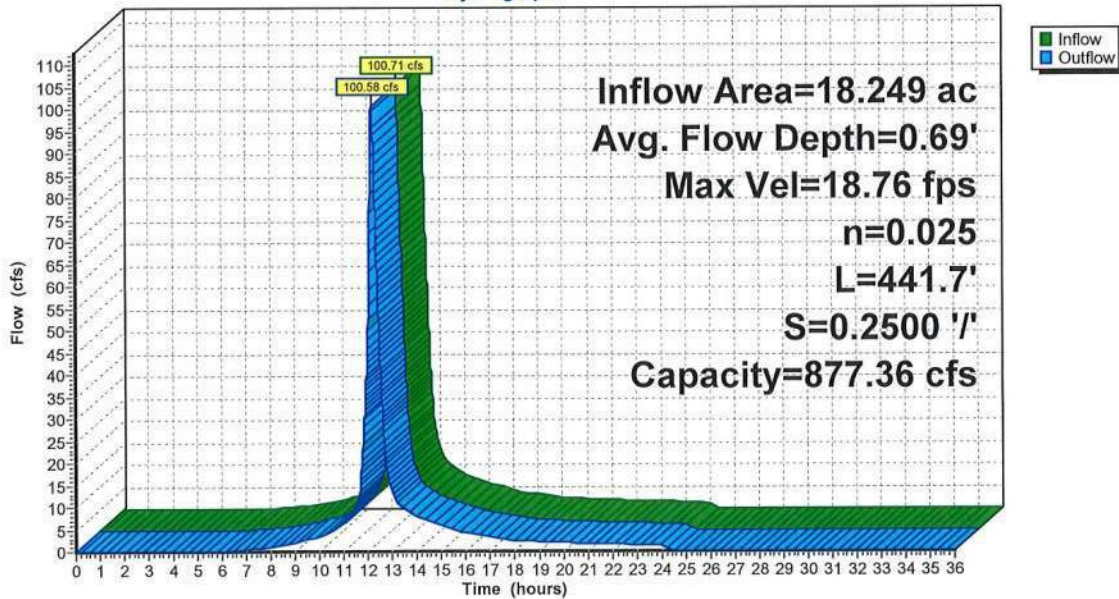
Peak Storage= 2,370 cf @ 12.16 hrs  
 Average Depth at Peak Storage= 0.69'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.36 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 441.7' Slope= 0.2500 ' / '  
 Inlet Invert= 172.00', Outlet Invert= 61.56'



**Reach SE: Chute-Concrete Block Open Cell**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach SW: Chute-Concrete Block Open Cell**

Inflow Area = 15.434 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 95.96 cfs @ 12.14 hrs, Volume= 7.926 af  
 Outflow = 95.76 cfs @ 12.15 hrs, Volume= 7.926 af, Atten= 0%, Lag= 0.6 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 18.50 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 5.68 fps, Avg. Travel Time= 1.2 min

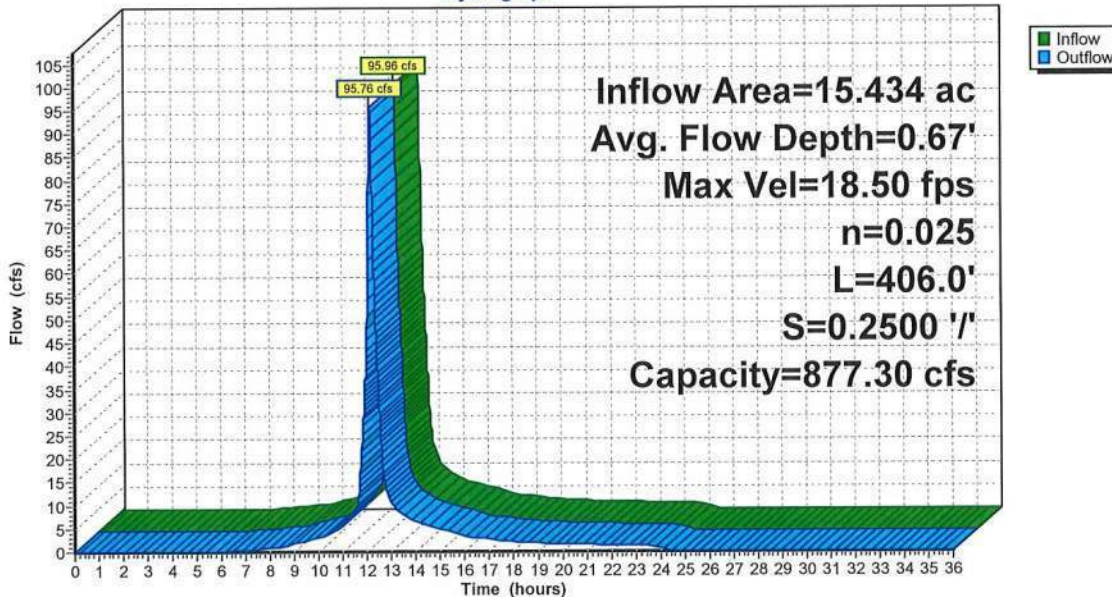
Peak Storage= 2,104 cf @ 12.14 hrs  
 Average Depth at Peak Storage= 0.67'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 ' / ' Top Width= 21.00'  
 Length= 406.0' Slope= 0.2500 ' / '  
 Inlet Invert= 172.00', Outlet Invert= 70.50'



**Reach SW: Chute-Concrete Block Open Cell**

Hydrograph



**Chute Analysis Post 25 Yr**

Type III 24-hr 25-Year Rainfall=8.70"

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**Summary for Reach W: Chute-Concrete Block Open Cell**

Inflow Area = 22.383 ac, 0.00% Impervious, Inflow Depth = 6.16" for 25-Year event  
 Inflow = 127.46 cfs @ 12.15 hrs, Volume= 11.495 af  
 Outflow = 127.28 cfs @ 12.16 hrs, Volume= 11.495 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 20.06 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity= 6.41 fps, Avg. Travel Time= 1.2 min

Peak Storage= 2,895 cf @ 12.15 hrs  
 Average Depth at Peak Storage= 0.78'  
 Bank-Full Depth= 2.00' Flow Area= 26.0 sf, Capacity= 877.30 cfs

5.00' x 2.00' deep channel, n= 0.025 Rubble masonry, cemented  
 Side Slope Z-value= 4.0 '1' Top Width= 21.00'  
 Length= 456.0' Slope= 0.2500 '1'  
 Inlet Invert= 172.00', Outlet Invert= 58.00'



**Reach W: Chute-Concrete Block Open Cell**

Hydrograph

